The Third Spectrum of Praseodymium (Pr III) in the Vacuum Ultraviolet

Jack Sugar

Institute for Basic Standards, National Bureau of Standards, Washington, D.C. 20234

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Measurements of the spectrum of doubly ionized praseodymium from 821 to 2103 Å are given. One hundred fifty-three energy levels deduced from these wavelengths and an earlier line-list of longer wavelengths are presented. These levels are identified with the configurations 4f26s, 4f27s, 4f28s, 4f²6p, 4f²6d, 4f²5f, 5d²4f, and 4f⁵d6s and are given term designations. Radial energy integrals belonging to these configurations are parametrically deduced from the known levels.

A value of 21.625 eV (174420 cm⁻¹) for the ionization energy of Pr III, with an estimated uncertainty

of 0.016 eV (130 cm⁻¹), is derived from the $4f^2ns$ series (n = 6, 7, 8).

Key words: Energy levels; interaction parameters; praseodymium; third spectrum; vacuum ultraviolet; wavelengths.

1. Introduction

The analysis of PrIII in the wavelength range from 2025 to 10716 Å [1,2] revealed nearly completely the energy level structure of the four low-lying configurations $4f^3$, $4f^25d$, $4f^26s$, and $4f^26p$, and some levels of $5d^24f$ and $4f^26d$. I have extended the observations to shorter wavelengths and measured 2948 lines in the range from 821 to 2103 Å. These new data have led to a considerable increase in the number of known levels of the $5d^{2}4f$ configuration and to the discovery of levels belonging to the 4f5d6s, $4f^25f$, and $4f^28s$ configurations. In addition, a reexamination of the old line-list yielded more levels of the configurations $4f^26s$, $4f^26d$, and $4f^27s$. In all, 153 energy levels of Pr III have been newly established.

The configurations to which they belong were treated theoretically for the purpose of determining parametrically the radial energy integrals and of calculating the level positions and eigenvectors. These calculations helped to confirm the experimental results and to locate unknown levels, as well as to provide an interpretation of the configurations in the most ap-

propriate coupling schemes.

Of particular interest are the mutually interacting odd configurations $4f^26p$, $5d^24f$, and 4f5d6s, which were treated as one complex. Many levels are strongly perturbed and were found to contain large percentages of terms of several configurations. In the $5d^24f$ configuration the addition of an "effective" two-body configuration interaction parameter for nonequivalent electrons decreased the rms error of the calculation by 25 percent.

The ionization energy of PrIII was calculated in ref. 2 by means of tentatively identified $4f^26d$ levels to form a $4f^2(^3H)nd$ (n=5,6) series. The new analysis provides the $4 f^2(^3H)ns$ series (n = 6, 7, 8) with which to determine a more reliable value.

Three levels given in reference 2 which were found to be poorly substantiated and have now been discarded are listed below:

Rejected levels	J	Config.	New levels
$45848.37~\mathrm{cm^{-1}}$ $68676.55~\mathrm{cm^{-1}}$	$\frac{2\frac{1}{2}}{2\frac{1}{2}}$	$4f^{2}6s$ $4f^{2}6p$	$45807.16~{\rm cm^{-1}}$
79378.43 cm ⁻¹	$\frac{2_{2}}{2_{2}^{1}}$	$4f^{2}6p$	$79366.69~{\rm cm^{-1}}$

2. Observations

For the most part, the procedure outlined in reference 2 for obtaining the spectrum PrIII has been followed. The sliding spark was operated at peak currents of 50 and 500 A to enhance the third and fourth spectra selectively. I departed from the earlier method of producing the second spectrum by means of an arc. Instead a 6 A sliding spark was used which gave a more clear-cut distinction between second and third spectra when compared with the 50 A spark, as well as sharper lines. This technique has already been used in the classification of Ce III [3].

The new extension of the observations of Pr III to shorter wavelengths was made with a 10.3 m Eagle vacuum spectrograph, utilizing a grating of 1200

¹ Figures in brackets indicate the literature references at the end of this paper.

grooves/mm blazed at 1200 Å. The first order of diffraction was photographed, giving a reciprocal dispersion of 0.78 Å/mm. One half to 2 hr exposures were required to record the spectrum of the spark, operating at a repetition rate of 15 sparks per second. Calibration spectra of C, N. O, Ar, Si, Ge, and Cu [4, 5, 6, 7, 8] were obtained from pulsed rf-excited electrodeless lamps and hollow cathode discharges.

Two to five measurements of the lines in the 50 A spark were made, the number depending on the recurrence of a line on progressively weaker exposures. From the variation of wavelengths obtained with different exposures the accuracy of the final values is estimated to be ± 0.004 Å. Systematic shifts between the various sets of measurements were removed by standardizing on wavelengths of internal impurities of C. N. O. and Si.

The new measurements overlap the previous list [1] in the region from 2000 to 2103 Å and considerably augment it, thus indicating that stronger exposures may be needed beyond this overlap. Lines of intensity designated as 1 in the old list are usually assigned 200 in the new list, and the other common lines are correspondingly stronger.

A complete tabulation of the newly observed lines appears in table X. The wavelengths given in the first column are the values in vacuum. Following this are the visually estimated intensities with the following descriptive notations:

cl = measurement affected by a close neighboring line, bl = a blend of two or more lines,

h = hazy,

w =wide.

Under "classification" appear the two energy levels from which the line originates, followed by a subscript *J*-value, and where appropriate a superscript degree mark representing odd parity. Double classifications of lines are given without repeating the wavelength.

In table I, newly classified lines from the longer wavelength list of reference 1 are given. Among these are lines having hfs, for which the following additional notations in the intensity column appear:

*r = strongest component of flag pattern shaded to red,
*v = strongest component of flag pattern shaded to
violet,

Table I. Newly classified lines of Pr III, $\lambda > 2103 \text{\AA}$

				TABLE 1. Newly classifie				
λ _ε Ā	air L	Intensity	σ (cm ⁻¹)	Classification	λ _{air} Å	Intensity	σ (cm ⁻¹)	Classification
4650	.609	9* v	21496.54	13887° _{7/2} - 35384 _{5/2}	3011.282	20 * v	33198.77	$50227_{5/2} - 83426^{\circ}_{5/2}$
4334	.697	9w	23063.18	$11761^{\circ}_{9/2} - 34825_{7/2}$	3006.469	60 * r	33251.92	$38726_{7/2} - 71978^{\circ}_{7/2}$
3607	.068	4 * r	27715.46	$52026_{3/2} - 79742^{\circ}_{1/2}$	3004.002	10 * r	33279.22	$52026_{3/2} - 85306^{\circ}_{5/2}$
3577	.336	8 * v	27945.80	$33659_{5/2} - 61605^{\circ}_{7/2}$	3002.106	2	33300.24	$38694_{5/2} - 71994^{\circ}_{5/2}$
3567	.897	1bl	28019.71	$50869_{1/2} - 78889^{\circ}_{3/2}$	2982.236	9* r	33522.11	$45844_{3/2} - 79366^{\circ}_{5/2}$
3565	.845	9 * v	28035.78	50658 _{13/2} - 78694° _{11/2}	2980.583	5 * r	33540.70	$50869_{1/2} - 84409^{\circ}_{3/2}$
3564	.405	30 * r	28047.13	50647 _{11/2} - 78694° _{11/2}	2978.907	9 * v	33559.57	$45807_{5/2} - 79366^{\circ}_{5/2}$
3510	.532	20 * v	28477.56	$50658_{13/2} - 79136^{\circ}_{13/2}$	2976.347	40 * v	33588.43	$45807_{5/2} - 79395^{\circ}_{7/2}$
3509	.142	3 * r	28488.86	50647 _{11/2} — 79136° _{13/2}	2963.032	2	33739.36	$36642_{13/2} - 70381^{\circ}_{13/2}$
3462	.700	1 * r	28870.93	$52026_{3/2} - 80897^{\circ}_{3/2}$		* 1		
3462	.432	1 * r	28873.16	$50869_{1/2} - 79742^{\circ}_{1/2}$	2940.896	7 * v	33993.30	$51312_{5/2} - 85306^{\circ}_{5/2}$
3412	.607	7 * r	29294.71	$50869_{1/2} - 80164^{\circ}_{3/2}$	2933.827	1	34075.21	$37919_{7/2} - 71994^{\circ}_{5/2}$
3402	.969	50 * r	29377.68	$52026_{3/2} - 81404^{\circ}_{5/2}$	2930.192	50 * v	34117.48	$35291_{9/2} - 69408^{\circ}_{11/2}$
3379	.131	50 * v	29584.91	$51312_{5/2} - 80897^{\circ}_{3/2}$	2924.661	2 * v	34181.99	$50227_{3/2} - 84409^{\circ}_{3/2}$
3377	.141	100 * v	29602.34	$45807_{5/2} - 75409^{\circ}_{3/2}$	2910.612	70 * v	34346.98	$28885_{\ 9/2}-\ 63232^{\circ}_{\ 7/2}$
3367	.350	200 * v	29688.42	$35291_{9/2} - 64979^{\circ}_{7/2}$	2890.842	2	34581.86	$39024_{9/2} - 73606^{\circ}_{9/2}$
3359	.973	3 * v	29753.59	$45807_{5/2} - 75560^{\circ}_{5/2}$	2885.001	6* r	34651.87	$38726_{7/2} - 73378^{\circ}_{7/2}$
3358	.083	30 * r	29770.34	$45844_{3/2} - 75614^{\circ}_{5/2}$	2876.229	1	34757.55	$69138^{\circ}_{9/2} - 103895_{7/2}$
3353	.866	50 * v	29807.77	$45807_{5/2} - 75614^{\circ}_{5/2}$	2857.700	4	34982.90	$37011_{5/2} - 71994^{\circ}_{5/2}$
3322	.203	6 * v	30091.85	$51312_{5/2} - 81404^{\circ}_{5/2}$	2851.486	6* r	35059.13	$33466_{11/2} - 68525^{\circ}_{11/2}$
3161	.330	7* r	31623.10	$50869_{1/2} - 82492^{\circ}_{3/2}$	2838.461	7 * r	35220.00	$35801_{7/2} - 71021^{\circ}_{9/2}$
3147	.878	9 * v	31758.23	$35291_{9/2} - 67049^{\circ}_{9/2}$	2827.668	3	35354.43	$36640_{7/2} - 71994^{\circ}_{5/2}$
3122	.646	7 * v	32014.84	$45807_{5/2} - 77821^{\circ}_{5/2}$	2819.342	2	35458.83	$37919_{7/2} - 73378^{\circ}_{7/2}$
3108	.884	7 * r	32156.56	$50869_{1/2} - 83025^{\circ}_{3/2}$	2812.509	9 * v	35544.98	$32760_{13/2} - 68305^{\circ}_{15/2}$
3098	.474	3 * v	32264.59	$50227_{3/2} -\ 82492^{\circ}_{3/2}$	2803.090	3	35664.41	$48745_{5/2} - 84409^{\circ}_{3/2}$
3087	.175	1 * r	32382.56	$52026_{3/2} -\ 84409^{\circ}_{3/2}$	2797.924	1bl	35730.25	$65935^{\circ}_{7/2} - 101665_{5/2}$
3061	.277	9 * v	32656.61	$45807_{5/2} - 78463^{\circ}_{7/2}$	2784.154	1	35906.96	$39732_{11/2} - 75640^{\circ}_{11/2}$
3039	.680	7	32888.63	$45805_{9/2} - 78694^{\circ}_{11/2}$	2776.318	4	36008.30	$48401_{3/2} - 84409^{\circ}_{3/2}$
3036	.913	8	32918.59	$44903_{5/2} - 77822^{\circ}_{5/2}$	2774.708	4	36029.19	$39732_{11/2} - 75762^{\circ}_{9/2}$
3018	.701	20 * v	33117.19	$51312_{5/2} - 84430^{\circ}_{7/2}$	2766.880	3	36131.12	$35863_{3/2} - 71994^{\circ}_{5/2}$

Table I. Newly classified lines of Pr III, $\lambda > 2103 \text{\AA}$ – Continued

$\overset{\boldsymbol{\lambda_{air}}}{\mathring{\mathbf{A}}}$	Intensity	σ (cm^{-1})	Classification	$\overset{\boldsymbol{\lambda_{air}}}{\mathring{\mathbf{A}}}$	Intensity	σ (cm ⁻¹)	Classification
2741.262	1	36468.76	66148° _{13/2} —102617 _{11/2}	2564.509	4	38982.14	65922° _{11/2} —104904 _{11/2}
2734.368	8	36560.70	$48745_{5/2} - 85306^{\circ}_{5/2}$	2563.474	6	38997.87	$36642_{13/2} - 75640^{\circ}_{11/2}$
2732.952	1	36579.64		2561.773	_		
			68987° _{7/2} -105566 _{9/2}		6	39023.77	$63593^{\circ}_{9/2} - 102617_{11/2}$
$2720.409 \\ 2712.384$	$\frac{1}{2}$	36748.29 36857.01	$66735^{\circ}_{13/2}$ — $103484_{15/2}$ $35137_{3/2}$ — $71994^{\circ}_{5/2}$	2559.865 2559.277	$\frac{1}{2}$	39052.85 39061.82	$68801^{\circ}_{7/2}$ $-107854_{9/2}$
						39001.02	$63768^{\circ}_{7/2}$ $-102830_{9/2}$
2707.422	2	36924.56	68525° _{11/2} —105450 _{11/2}	2558.675	5	39071.01	$61717^{\circ}_{5/2} -100788_{7/2}$
2706.611	5	36935.62	$36670_{11/2} - 73606^{\circ}_{9/2}$	2558.537	4	39073.12	$61357^{\circ}_{9/2} - 100430_{9/2}$
2704.403	1	36965.78	$36640_{7/2} - 73606^{\circ}_{9/2}$	2557.323	3	39091.67	$36670_{11/2} - 75762^{\circ}_{9/2}$
2699.300	5 * r	37035.65	$38726_{7/2} - 75762^{\circ}_{9/2}$	2556.813	4	39099.46	$64235^{\circ}_{9/2}$ $-103335_{9/2}$
2687.981	6 * v	37191.60	$38448_{9/2} - 75640^{\circ}_{11/2}$	2555.353	7	39121.80	$62558^{\circ}_{11/2}$ — $101680_{13/2}$
2687.506	1	37198.17	$63232^{\circ}_{7/2}$ $-100430_{9/2}$	2554.979	1	39127.53	$38694_{5/2} - 77822^{\circ}_{5/2}$
2686.455	3	37212.73	$63576^{\circ}_{5/2}$ $-100788_{7/2}$	2549.531	1	39211.13	$67870^{\circ}_{9/2}$ $-107081_{9/2}$
2673.055	5	37399.26	$65909^{\circ}_{5/2} - 103308_{7/2}$	2545.790	9	39268.75	$64215^{\circ}_{13/2}$ $-103484_{15/2}$
2666.218	2	37495.16	$63576^{\circ}_{5/2} -101071_{5/2}$	2543.644	1	39301.88	$66148^{\circ}_{13/2}$ $-105450_{11/2}$
2663.415	3	37534.62	$65295^{\circ}_{7/2}$ $-102830_{9/2}$	2541.080	8	39341.53	$61605^{\circ}_{7/2}$ $-100947_{9/2}$
2650.675	1	37715.01	$63232^{\circ}_{7/2}$ $-100947_{9/2}$	2540.311	7	39353.44	$61717^{\circ}_{5/2}$ $-101071_{5/2}$
2647.019	1	37767.10	$68978^{\circ}_{5/2} - 106745_{5/2}$	2539.759	5	39361.99	$68492^{\circ}_{7/2} - 107854_{9/2}$
					$\frac{3}{2}$		
2640.290	4	37863.35	68801° _{7/2} -106665 _{7/2}	2537.099		39403.26	$39732_{11/2}$ $79136^{\circ}_{13/2}$
2634.707 2629.918	5 1	37943.58 38012.66	$69138^{\circ}_{9/2}$ $-107081_{9/2}$ $65295^{\circ}_{7/2}$ $-103308_{7/2}$	2536.648 2534.759	7 9	39410.26 39439.63	$39725_{15/2}$ — $79136^{\circ}_{13/2}$ $62240^{\circ}_{11/2}$ — $101680_{13/2}$
					_		
2626.210	2	38066.33	$62558^{\circ}_{11/2}$ — $100625_{11/2}$	2531.925	7	39483.77	$66148^{\circ}_{13/2}$ – $105632_{13/2}$
2626.016	1	38069.14	$68676^{\circ}_{5/2}$ $-106745_{5/2}$	2530.464	9	39506.57	$44903_{5/2}-84409^{\circ}_{3/2}$
2624.624	1	38089.33	$63576^{\circ}_{5/2}$ $-101665_{5/2}$	2529.726	4	39518.09	$63816^{\circ}_{11/2}$ – $103335_{9/2}$
2622.448	5	38120.94	$68544^{\circ}_{9/2}$ $-106665_{7/2}$	2529.430	2	39522.72	$68331^{\circ}_{7/2}$ $-107854_{9/2}$
2619.706	3	38160.83	$69138^{\circ}_{9/2}$ $-107299_{7/2}$	2529.110	9	39527.72	$65922^{\circ}_{11/2}$ — $105450_{11/2}$
2619.162	1	38168.76	$66735^{\circ}_{13/2} - 104904_{11/2}$	2528.330	2	39539.91	63768° _{7/2} —103308 _{7/2}
2618.891	2	38172.71	$68492^{\circ}_{7/2} - 106665_{7/2}$	2526.636	1	39566.42	$63768^{\circ}_{7/2}$ $-103335_{9/2}$
2617.740	3	38189.49	$62240^{\circ}_{11/2} - 100430_{9/2}$	2525.123	8	39590.12	$61357^{\circ}_{9/2} - 100947^{\circ}_{9/2}$
2616.047	1	38214.21	$63232^{\circ}_{7/2} - 101446_{7/2}$	2521.677	1	39644.22	$65922^{\circ}_{11/2}$ $-105566_{9/2}$
2010.011			$62535^{\circ}_{9/2} - 100788_{7/2}$	2521.021	7	39654.54	$64150^{\circ}_{11/2}$ $-103805_{13/2}$
2613.377	3	38253.24	$68492^{\circ}_{7/2} - 106745_{5/2}$				
2611 525		20200 04		2520.662	2	39660.18	$64235^{\circ}_{~9/2}$ $-103895_{~7/2}$
2611.527	1	38280.34	$68801^{\circ}_{7/2}$ $-107081_{9/2}$	2517.515	8	39709.76	$65922^{\circ}_{11/2}$ — $105632_{13/2}$
2610.351	8	38297.59	$66301^{\circ}_{15/2}$ – $104598_{13/2}$	2516.337	1	39728.35	$61717^{\circ}_{5/2}$ $-101446_{7/2}$
2606.515	5	38353.95	$35024_{7/2} - 73378^{\circ}_{7/2}$	2515.487	7	39741.77	$63593^{\circ}_{9/2} - 103335_{9/2}$
2604.457	3	38384.25	$62240^{\circ}_{11/2}$ — $100625_{11/2}$	2509.243	7	39840.66	$61605^{\circ}_{7/2} - 101446_{7/2}$
2603.320	2	38401.01	67049° _{9/2} —105450 _{11/2}	2505.358	1	39902.44	$37919_{7/2} - 77822^{\circ}_{5/2}$
2603.263	1	38401.86	$64215^{\circ}_{13/2}$ – $102617_{11/2}$	2503.391	5	39933.78	$35828_{9/2} - 75762^{\circ}_{9/2}$
2602.446	2	38413.91	$68331^{\circ}_{7/2} - 106745_{5/2}$	2502.526	5	39947.59	$61717^{\circ}_{5/2}$ $-101665_{5/2}$
2602.224	1	38417.19	$37197_{3/2} - 75614^{\circ}_{5/2}$	2499.968	10	39988.46	$63816^{\circ}_{11/2}$ $-103805_{13/2}$
2599.960	1	38450.64	$66148^{\circ}_{13/2}$ – $104598_{13/2}$	2499.686	6	39992.97	$38701_{13/2}$ — $78694^{\circ}_{11/2}$
2595.448	1	38517.48	$67049^{\circ}_{9/2} - 105566_{9/2}$	2498.297	1	40015.20	$68544^{\circ}_{9/2} - 108559_{11/2}$
2592.832	5	38556.34	$68525^{\circ}_{11/2}$ $-107081_{9/2}$	2497.143	2	40033.69	$68525^{\circ}_{11/2} - 108559_{11/2}$
2592.424	2	38562.40	$62062^{\circ}_{9/2} - 100625_{11/2}$	2495.584	2	40058.70	$67240^{\circ}_{7/2} - 107299_{7/2}$
2590.248	3	38594.80	64235° _{9/2} -102830 _{9/2}	2495.508	10	40059.92	$61605^{\circ}_{7/2} - 101665_{5/2}$
2589.900	4	38599.98	$65295^{\circ}_{7/2}$ $-103895_{7/2}$	2493.685	6	40089.20	$61357^{\circ}_{9/2} - 101446_{7/2}$
2584.766	3	38676.65	65922° _{11/2} —104598 _{13/2}	2491.326	6	40127.16	63768° _{7/2} —103895 _{7/2}
2582.712	1	38707.40	$68374^{\circ}_{9/2} -107081_{9/2}$	2487.750	6	40184.84	$68374^{\circ}_{9/2}$ $-108559_{11/2}$
2577.866	2	38780.16	$67965^{\circ}_{3/2} - 106745_{5/2}$	2482.577	1	40268.57	$60520^{\circ}_{7/2}$ $-100788_{7/2}$
2576.922	3	38794.37	$67870^{\circ}_{9/2} - 106665_{7/2}$	2480.487	9	40302.49	$63593^{\circ}_{9/2}$ $-103895_{7/2}$
2576.109	1	38806.61	68492° _{7/2} —107299 _{7/2}	2475.946	1	40376.40	$62240^{\circ}_{11/2} - 102617_{11/2}$
2574.917	7	38824.58	$61605^{\circ}_{7/2}$ $-100430_{9/2}$	2474.320	1	40402.94	$44903_{5/2} - 85306^{\circ}_{5/2}$
2572.074	i	38867.49	$68987^{\circ}_{7/2} - 107854_{9/2}$	2472.376	5	40434.70	$38701_{13/2} - 79136^{\circ}_{13/2}$
2572.074	4	38896.28	$66735^{\circ}_{13/2}$ $-107634_{9/2}$ $-105632_{13/2}$	2469.796	1	40476.94	$35137_{3/2} - 75614^{\circ}_{5/2}$
	1						
2565.796 2565.346	1 1	38962.58	$36652_{5/2} - 75614^{\circ}_{5/2}$	2465.272	2	40551.21	$60520^{\circ}_{7/2} - 101071_{5/2}$
		38969.42	$36670_{11/2} - 75640^{\circ}_{11/2}$	2462.895	10	40590.35	$35024_{7/2} - 75614^{\circ}_{5/2}$

TABLE I. Newly classified lines of Pr III, $\lambda > 2103 \text{Å}$ —Continued

$egin{array}{c} \lambda_{air} \ \mathring{A} \end{array}$	Intensity	σ (cm ⁻¹)	Classification	Å Å	Intensity	σ (cm ⁻¹)	Classification
2460.719	10	40626.24	$44679_{7/2} - 85306^{\circ}_{5/2}$	2320.906	2	43073.39	62558° _{11/2} —105632 ₁₃
2451.381	2	40780.98	$60166^{\circ}_{9/2} - 100947_{9/2}$	2317.199	9	43142.29	$60166^{\circ}_{9/2} - 103308_{7/2}$
2449.908	4	40805.50	$62678^{\circ}_{13/2} - 103484_{15/2}$	2315.774	2	43168.84	$60166^{\circ}_{9/2} - 103335_{9/2}$
2449.636	1	40810.03	$37011_{5/2} - 77822^{\circ}_{5/2}$	2310.248	3	43272.09	$58174^{\circ}_{9/2} - 101446_{7/3}$
2442.697	1	40925.95	$60520^{\circ}_{7/2}$ $-101446_{7/2}$	2309.386	1	43288.24	58158° _{7/2} —101446 _{7/}
2432.678	7	41094.49	$34520_{5/2} - 75614^{\circ}_{5/2}$	2308.670	5	43301.66	$34520_{5/2} - 77822^{\circ}_{5/2}$
2431.260	8	41118.46	29263 _{13/2} — 70381° _{13/2}	2307.384	6	43325.79	62240° _{11/2} —105566 _{9/}
2423.700	3	41246.71	$62558^{\circ}_{11/2}$ – $103805_{13/2}$	2307.277	2	43327.80	$40098_{5/2} - 83426^{\circ}_{5/2}$
2422.883	6	41260.61	$60419^{\circ}_{11/2}$ – $101680_{13/2}$	2304.201	6	43385.64	$60419^{\circ}_{11/2}$ – 103805_{13}
2416.527	1	41369.13	65295° _{7/2} —106665 _{7/2}	2303.121	7	43405.98	$41023_{7/2} - 84430^{\circ}_{7/2}$
2384.757	5	41920.21	$62678^{\circ}_{13/2} - 104598_{13/2}$	2296.541	2	43530.34	63768° _{7/2} —107299 _{7/}
2382.979	3	41951.49	$61357^{\circ}_{9/2} -103308_{7/2}$	2295.856	4	43543.32	$29835_{9/2} - 73378^{\circ}_{7/2}$
2382.588	6	41958.37	$35863_{3/2} - 77822^{\circ}_{5/2}$	2287.502	2	43702.33	64857° _{9/2} -108559 ₁₁
2380.051	4	42003.09	$65295^{\circ}_{7/2}$ $-107299_{7/2}$	2261.530	6	44204.17	$40205_{3/2} - 84409^{\circ}_{3/2}$
2378.867	6	42024.00	$36670_{11/2} - 78694^{\circ}_{11/2}$	2257.546	4	44282.17	$41023_{7/2} - 85306^{\circ}_{5/2}$
2369.081	10	42197.57	60419° _{11/2} —102617 _{11/2}	2257.342	5w	44286.18	26095 _{11/2} — 70381° ₁₃
2367.497	3	42225.80	$62678^{\circ}_{13/2}$ $-104904_{11/2}$	2251.445	8	44402.16	25979 _{15/2} — 70381° ₁₃
2365.796	8	42256.16	$58174^{\circ}_{9/2} -100430_{9/2}$	2243.485	1w	44559.69	$39870_{9/2} - 84430^{\circ}_{7/2}$
2360.786	5	42345.83	$62558^{\circ}_{11/2} - 104904_{11/2}$	2238.560	6	44657.71	$28720_{9/2} - 73378^{\circ}_{7/2}$
2357.627	3	42402.56	$41023_{7/2} - 83426^{\circ}_{5/2}$	2227.201	3	44885.45	$28720_{9/2} - 73606^{\circ}_{9/2}$
2357.176	3	42410.67	$60419^{\circ}_{11/2} - 102830_{9/2}$	2211.332	1	45207.52	$40098_{5/2}-85306^{\circ}_{5/2}$
2354.942	6	42450.90	$58174^{\circ}_{9/2} - 100625_{11/2}$	2208.939	6	45256.49	$30505_{11/2}$ $- 75762^{\circ}_{9/2}$
2354.128	2	42465.58	$36670_{11/2} - 79136^{\circ}_{13/2}$	2201.678	7w	45405.73	$39024_{9/2} -\ 84430^{\circ}_{7/2}$
2353.942	6	42450.90	$60166^{\circ}_{9/2}$ $-102617_{11/2}$	2196.775	7	45507.06	$37919_{7/2} - 83426^{\circ}_{5/2}$
2345.001	4	42630.85	$58158^{\circ}_{7/2} -100788_{7/2}$	2176.676	3	45927.22	$29835_{9/2} - 75762^{\circ}_{9/2}$
2337.295	2	42771.39	$62678^{\circ}_{13/2} - 105450_{11/2}$	2162.611	2	46225.88	27380 _{11/2} — 73606° ₉
2335.873	6	42797.43	$35024_{7/2} - 77822^{\circ}_{5/2}$	2155.562	5	46377.03	29263 _{13/2} — 75640° ₁
2332.129	1	42866.12	$35828_{9/2}-78694^{\circ}_{11/2}$	2148.203	1	46535.89	23442 _{11/2} — 69978° ₁
2330.393	6	42898.06	$64401^{\circ}_{5/2}$ $-107299_{7/2}$	2135.942	2	46802.99	23175 _{13/2} — 69978° ₁
2329.568	7	42913.25	$58158^{\circ}_{7/2}$ $-101071_{5/2}$				
2329.456	2	42915.31	$60419^{\circ}_{11/2}$ – $103335_{9/2}$				
2325.016	2	42997.26	$64857^{\circ}_{9/2} - 107854_{9/2}$				
2324.807	1	43001.12	$27380_{11/2} - 70381^{\circ}_{13/2}$				
2324.438	7	43007.95	$62558^{\circ}_{11/2} - 105566_{9/2}$				
2321.717	5	43058.35	$28936_{3/2} - 71994^{\circ}_{5/2}$				

3. New Energy Levels

The techniques for using electronic computers in the search for energy levels are now well-known. The method [9] by which the line-list is added to (or subtracted from) the known levels to obtain statistically significant numbers of repeating sums (or differences) was used here. The selection of real levels is based on the probability of the occurrence of a chain of repeating sums of a particular length and tolerance as well as the line intensity distribution in the chain. This method yields many energy levels, but there always remain a certain number which make few combinations (particularly levels of high *J*-value) and which must be sought by intensity criteria alone

according to the appropriate selection rules, and predicted positions.

Most of the observed lines of Pr III with moderate to strong intensity in the vacuum ultraviolet range are due to transitions to the $4f^25d$ configuration. The highest density of lines occurs between 1000 and 1200 Å, the main region of the $4f^25d-4f^25f$ transition array. This is analogous to Ce III where the same region contained the 4f5d-4f5f array [3]. In both cases, the array is well isolated and easily accessible, so that a thorough description of it can be obtained. With these lines 74 levels of the $4f^25f$ configuration were found.

Designations in LS-coupling were assigned to these levels on the basis of relative line intensities. Although final designations are given in the J_1l scheme in

Table II. New energy levels of Pr III

table II, the experimentally derived LS names were important in relating the theoretical calculation of this configuration to the observed levels. The calculated LS composition, while showing less purity than J_1l , gave single designations for many levels exceeding 50 percent. The largest LS component for each level has been included in table VI.

A second region of high line-density appears from the beginning of table X to about 1800 Å. This is the short wavelength end of the $4f^25d$ — $(4f^26p+5d^24f)$ transition array, which extends to about 2700 Å. Many of these lines were classified with the previously known levels. The tail of this array reaches to much shorter wavelengths due to the high-lying levels of $5d^24f$.

An extension of the high-level structure of even parity was made by using the longer wavelength linelist of reference 1. By combining these lines with the $4f^26p$ levels, more levels in the region of the previously identified $4f^26d$ group were found. Calculations of the structure of the configurations $4f^26d$ and $4f^27s$ provided the means to distinguish the latter configuration from among these levels.

Several low levels of the $4f^28s$ configuration were found by adding the vacuum ultraviolet lines to the $4f^26p$ levels. They were identified by their predicted location (compared with Ce III, 4f8s), by their strong combinations with particular core terms of $4f^26p$, and by reasonable fitted values of the parameters $G^3(fs)$, $\zeta(4f)$ and $E^3(f^2)$.

A detailed investigation of the hfs of the $4f^26s$ configuration has been carried out by J. Reader and J. Sugar [10]. A by-product of this work was the discovery of the pair of levels based on the $4f^2(^3P_2)$ parent and the replacement of the level $\langle 4f^2(^1D_2), 6s, 5/2 \rangle$.

The newly derived energy levels of PrIII are given in table II. Their designations result from calculations of the configurations in the purest coupling schemes, with radial parameters obtained by least squares fitting of linear energy formulas to the observed energy levels [11]. The results of these calculations are given in the sections which follow.

Designations of levels of the $4f^25f$, $5d^24f$, and 4f5d6s configurations in the LS-coupling scheme were made on the basis of relative strengths of the combinations with the $4f^25d$ terms. Later calculations of energy levels in this coupling scheme substantiated these assignments where the purity of the eigenvectors indicated a major LS component for a level. The successful correlation of observed and calculated energy levels was largely due to these experimental LS assignments.

The $4f^26d$, $4f^27s$, and $4f^28s$ levels were designated in J_{ij} -coupling according to the intensities of combinations with levels of $4f^26p$. In these transition arrays the selection rules $\Delta L_1 = 0$, $\Delta S_1 = 0$, and $\Delta J_1 = 0$ on parent levels are strongly obeyed. The J_{ij} -coupling designations given in table II for these configurations and for $4f^26s$ and $4f^26p$ contain the $4f^2$ core level and the j-value of the outer electron.

Configuration	Designation	J	Energy/hc (cm ⁻¹)
4f26s	$(^{7}D_{2})1/2$ $(^{3}P_{1})1/2$ $(^{3}P_{2})1/2$ $(^{3}P_{2})1/2$	$ \begin{array}{c} 2\frac{1}{2} \\ 0\frac{1}{2} \\ 2\frac{1}{2} \\ 1\frac{1}{2} \end{array} $	^a 45807.1 50869.3 51312.8 52026.9
$5d^24f$	(3P ₂)1/2 (3F) ² I° (3F) ³ I° (1D) ³ H° (3P) ⁴ G° (3F) ³ G° (3F) ³ G° (3P) ² G° (3P) ² G° (3P) ² D° (1D) ² D° (1G) ² H° (1D) ² G° (3P) ³ G°	$egin{array}{c} 1rac{1}{2} \\ 5rac{1}{2} \\ 7rac{1}{2} \\ 5rac{1}{2} \\ 2rac{1}{2} \\ 5rac{1}{2} \\ 6rac{1}{2} \\ 4rac{1}{2} \\ 3rac{1}{2} \\ 4rac{1}{2} \\ 3rac{1}{2} \\ 4rac{1}{2} \\ 5rac{1}{2} \\ 5rac{1}{2} \\ 5rac{1}{2} \\ 5racc{1}{2} \\ 5racccccccccccccccccccccccccccccccccccc$	52026.9 68238.12 68305.1 69408.51 69681.6 69978.08 70381.48 71021.1 71385.6 71501.0 71994.81 73029.9 73378.42 73606.17 73609.1
	(3P)4P° (3P)4F° (3P)4F°	$\begin{array}{c} 2\frac{1}{2} \\ 1\frac{1}{2} \\ 3\frac{1}{2} \end{array}$	74105.2 74463.7 75294.0
$4f^26p$	$(^{1}D_{2})1/2^{\circ}$	$2\frac{1}{2}$	75614.81
$5d^24f$	(3F)2H° (1G)2G° (1G)2F° (1G)2F° (1G)2I° (1G)2I°	$egin{array}{c} 5rac{1}{2} \ 4rac{1}{2} \ 1rac{1}{2} \ 2rac{1}{2} \ 3rac{1}{2} \ 5rac{1}{2} \ 6rac{1}{2} \ \end{array}$	75640.00 75762.23 76892.4 77822.00 78463.6 78694.57 79136.23
$4f^26p$	$(^{1}D_{2})3/2^{\circ}$	$2\frac{1}{2}$	79366.65
$5d^24f$	$(^1\mathrm{G})^2\mathrm{D}^\circ$	$1\frac{1}{2}$	82492.4
$4f^26p$	$\begin{array}{c} (^{3}P_{1})3/2^{\circ} \\ (^{3}P_{1})3/2^{\circ} \\ (^{3}P_{2})3/2^{\circ} \\ (^{3}P_{2})3/2^{\circ} \end{array}$	$\begin{array}{c} 2\frac{1}{2} \\ 1\frac{1}{2} \\ 3\frac{1}{2} \\ 2\frac{1}{2} \end{array}$	83426.55 84409.93 84430.98 85306.10
4f5d6s	(3G)4G° (3H)4F° (3G)4G° (3G)5G°	$3\frac{1}{2}$ $4\frac{1}{2}$ $4\frac{1}{2}$ $5\frac{1}{2}$ $4\frac{1}{2}$ $3\frac{1}{2}$	87511.6 88220.2 88948.6 90119.8 90629.2 92441.7
$5d^24f$	$(^{1}\mathrm{S})^{2}\mathrm{F}^{\circ}$	$2\frac{1}{2}$	92554.8
4f5d6s	$(^3\mathrm{H})^2\mathrm{H}^\circ$	$5\frac{1}{2}$	93296.5
$5d^24f$	$(^{1}\mathrm{S})^{2}\mathrm{F}^{\circ}$	$3\frac{1}{2}$	93967.4
4f5d6s	(3G) ² G° (1F) ² F°	$\frac{4\frac{1}{2}}{3\frac{1}{2}}$	95147.9 96830.5
$4f^26d$	(3H ₄)3/2 (3H ₄)3/2 (3H ₄)3/2 (3H ₄)5/2 (3H ₄)5/2 (3H ₄)5/2 (3H ₄)5/2 (3H ₅)3/2 (3H ₅)3/2 (3H ₅)3/2 (3H ₅)3/2 (3H ₅)5/2	$4\frac{1}{2}$ $5\frac{1}{2}$ $3\frac{1}{2}$ $4\frac{1}{2}$ $2\frac{1}{2}$ $2\frac{1}{2}$ $2\frac{1}{2}$ $2\frac{1}{2}$ $4\frac{1}{2}$ $4\frac{1}{2}$ $3\frac{1}{2}$ $4\frac{1}{2}$ $4\frac{1}{2}$ $4\frac{1}{2}$	100430.29 100625.04 100788.95 100947.18 101071.43 101446.27 101665.58 101680.38 102617.24 102830.43 103308.53 103335.06
	$(^{3}H_{5})5/2$ $(^{3}H_{5})5/2$ $(^{3}H_{5})5/2$	$ \begin{array}{c} 7\frac{1}{2} \\ 6\frac{1}{2} \\ 3\frac{1}{2} \end{array} $	103484.19 103805.38 103895.83

Configuration	Designation	J	Energy/hc (cm ⁻¹)
$4f^{2}7s$	$(^{3}H_{6})1/2$	$6\frac{1}{2}$	104598.99
$4f^26d$	$ \begin{array}{l} (^{3}H_{6})3/2 \\ (^{3}H_{6})5/2 \\ (^{3}H_{6})3/2 \\ (^{3}H_{6})5/2 \end{array} $	$5\frac{1}{2}$ $5\frac{1}{2}$ $4\frac{1}{2}$ $6\frac{1}{2}$	104904.55 105450.18 105566.62 105632.16
$4f^27s$	${3F_3}1/2$ ${3F_3}1/2$ ${3F_4}1/2$	$\begin{array}{c} 3\frac{1}{2} \\ 2\frac{1}{2} \\ 4\frac{1}{2} \end{array}$	106665.07 106745.65 107081.94
$4f^26d$	${(^{3}F_{3})3/2} \over {(^{3}F_{4})3/2} \over {(^{3}F_{4})5/2}$	$3\frac{1}{2}$ $4\frac{1}{2}$ $5\frac{1}{2}$	107299.07 107854.46 108559.40
4f25f	(3H ₄)[6]° [4]° [5]° [4]° [6]° [2]° [7]° [3]° [5]° [7]° [7]° [8]° [4]° [4]° [3]° [6]°	$\begin{array}{c} 5_{1\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}} \\ 5_{1\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}} \\ 5_{1\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}} \\ 4_{1\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}} \\ 4_{1\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}} \\ 6_{1\frac{1}{2}$	110295.1 110333.5 110530.9 110881.1 110922.5 111110.3 111268.7 111335.1 111342.8 111494.8 111993.0 112643.2 112769.7 112896.3 113023.5 113158.8 113291.8 113556.8 113600.3
	$\begin{bmatrix} 3 \\ 6 \\ 9 \\ 4 \\ 9 \\ 2 \\ 8 \\ 9 \\ 2 \\ 9 \\ 6 \\ 6 \\ 9 \\ 6 \\ 9 \\ 6 \\ 9 \\ 6 \\ 9 \\ 9$	$\begin{array}{c} 3\frac{1}{2}\frac{1}{12}\frac{1}{12}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\\ 4\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\\ \frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\\ \frac{1}{2}\frac{1}{2$	113630.9 113664.3 113780.5 113825.5 113833.9 113914.1 114725.6 114797.2 114970.7 115324.3 115403.3 115408.4
		$egin{array}{c} 3 & 4 & 3 & 7 & 1 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 1 & 2 & 2$	115420.8 115499.8 115670.0 115672.2 115800.0 115933.2 116021.8 116238.8 116309.2 116453.2 116489.8 116727.1 117044.6 117248.2 117333.1 117540.5 117574.5
	[4]° [3]° [3F ₄][6]° [7]° [3F ₃][4]° [2]° [3F ₄][5]° [3F ₃][3]° [3H ₄][5]°	$\begin{array}{c} 3\frac{1}{2} \\ 3\frac{1}{2} \\ 2\frac{1}{2} \\ 6\frac{1}{2} \\ 7\frac{1}{2} \\ 4\frac{1}{2} \\ 1\frac{1}{2} \\ 5\frac{1}{2} \\ 3\frac{1}{2} \\ 4\frac{1}{2} \\ \end{array}$	117647.2 117686.4 117775.3 118063.0 118081.1 118201.4 118271.6 118318.6 118468.8

Configuration	Designation	J	Energy/hc (cm ⁻¹)
	[7]°	$6\frac{1}{2}$	118610.9
	Ī5ΰ	$5\frac{1}{2}$	118879.3
	$({}^{1}G_{4})[6]^{\circ}$	$6\frac{1}{2}$	120498.7
	°[5]°	$5\frac{1}{2}$	121095.2
	Ī7ΰ	$7\frac{1}{2}$	121 1 19.2
	Ī5ΰ	$4\frac{1}{2}$	121382.6
	Ī7ΰ	$6\frac{1}{2}$	121431.2
	ľ6ľ°	$5\frac{1}{2}$	121532.5
1 1	$({}^{\scriptscriptstyle 1}\mathrm{D}_2)[[1]]^\circ$	$1\frac{1}{2}$	128214.2
	[5]°	$4\frac{1}{2}$	128352.8
	[5]°	$5\frac{1}{2}$	128381.6
	[4]°	$3\frac{1}{2}$	128453.2
	ӷ҇41๋°	$4\frac{1}{2}$	128568.6
	$({}^{1}I_{6})[9]^{\circ}$	$8\frac{1}{2}$	133194.3
	°[6]	$9\frac{1}{2}$	133242.3
	°[8]	$7\frac{1}{2}$	133352.2
	[8]°	$\begin{array}{c} 6^{\frac{1}{2}}_{1^{\frac{1}{2}}} \frac{1}{2} \frac{1}{2} \frac{1}{2} \\ 5 \frac{1}{2} \\ 5 \frac{1}{2} \frac{1}{$	133373.0
$4f^{2}8s$	$(^{3}H_{4})1/2$	$4\frac{1}{2}$	129106.1
	$(^{3}H_{5})1/2$	$5\frac{1}{2}$	131200.3
	$(^{3}H_{5})1/2$	$4\frac{1}{2}$	131226.3
	$(^{3}H_{6})1/2$	$6\frac{1}{2}$	133393.2
-	$(^{3}H_{6})1/2$	$egin{array}{c} 4rac{1}{2} \\ 5rac{1}{2} \\ 4rac{1}{2} \\ 6rac{1}{2} \\ 5rac{1}{2} \\ 3rac{1}{2} \\ 4rac{1}{2} \end{array}$	133503.9
	$(^{3}F_{3})1/2$	$3\frac{1}{2}$	135445.2
	$({}^{3}F_{4})1/2$	$4\frac{1}{2}$	135868.8

^a Level values are given to two decimal places when derived from wavelengths > 2100 Å having no hfs.

4. Theoretical Interpretation of the Observed Configurations

For the calculation and diagonalization of energy matrices, computer programs written by Y. Bordarier and A. Carlier at Laboratoire Aimé Cotton, Orsay, France, were used. These programs evaluate the energy formulas given in terms of *nj*-coefficients, and compiled the output in the form of *J*-matrices which may then be diagonalized. The large library of matrices assembled at Hebrew University by G. Racah and his co-workers was made available to us by Z. Goldschmit, and is compatible with the above-mentioned programs.

The matrix library tape contains the configurations f^2p and $f(d+s)^2$. For the present work they were combined with configuration interaction (utilizing the formulas for three-electron matrix elements calculated by Fano, Pratts, and Goldschmidt [12]) to study the configuration complex $4f^26p + 5d^24f + 4f5d6s$. The matrices of $f^2(d+s)$ are also on the library tape, and were used in the study of $4f^26d$, $4f^27s$, and $4f^28s$. The matrices of f^2f' were calculated manually by means of the Racah formalism [13] prior to the acquisition of these programs.

In the present paper, unreduced values for the Slater parameters are used. The convention of multiplying the coefficient martices by arbitrary factors to simplify denominators is unnecessary for computer calculations.

The notations for the parameters in tables III, V, VII, and IX have the following meaning: "A" is an additive constant common to all levels of the configuration; $F^k(l, l')$ and $G^k(l, l')$ are the Slater radial integrals arising from the electrostatic interaction between the electrons l and l'; ζ_l is the parameter of the spin-orbit

Table III. Fitted parameter values and associated standard errors for the 4f²6p + 5d²4f + 4f²6ds configurations of Pr III and corresponding parameters of Ce III and Pr IV in units of cm⁻¹

Parameters	Pr III	Се ІІІ	Prıv
	$4f^26p$	4f6p	$4f^2$
$\frac{\Gamma^1(f^2)}{\Gamma^2}$	$\begin{array}{ccccc} 67903 & \pm & 90 \\ 4984 & \pm & 25 \\ 23.1 \pm & 0.2 \\ 486 & \pm & 2 \\ 28 & \pm & 2 \\ -50 & \pm & 9 \end{array}$	52001 ± 62	$\begin{array}{c} 5011 & \pm 17 \\ 23.1 \pm & 0. \\ 488 & \pm & 1 \\ 24 & \pm & 1 \\ -49 & \pm & 6 \end{array}$
72 (fp)	$\begin{array}{rrr} 6075 & \pm 225 \\ 1785 & \pm 140 \\ 1531 & \pm 302 \\ 2338 & \pm 24 \\ 751 & \pm 10 \end{array}$	5400 ± 450 2450 ± 875 945 ± 284 2155 ± 33 644 ± 10	760 ± 6
	$5d^24f$	$5d^2$	
A = G = G = G = G = G = G = G = G = G =	73137 ± 48 406 ± 5 2021 ± 21 21000 ± 284 15385 ± 431 10080 ± 96	$46027 \pm 67 \\ 442 \pm 3 \\ 2006 \pm 111$	
73 75 .d 	13954 ±665 10825 ±611 946 ± 23 838 ± 19 483 ± 55	837± 14	
	4f5d6s	5 <i>d</i> 6 <i>s</i>	
4 F ² (fd) G ¹ G ³ G ⁵ G ² (ds) G ³ (fs) G ³ (fs)	$\begin{array}{c} 92316 & \pm \ 156 \\ 20790 & \pm \ 1050 \\ 15177 \ \text{Fixed} \ F^2/F^4 \\ 9905 & \pm \ 476 \\ 13167 \ \text{Fixed} \ G^1/G^3 \\ 10825 \ \text{Fixed} \ G^1/G^5 \\ 10125 & \pm \ 410 \\ 2100 \ \text{Fixed} \\ 1035 & \pm \ 66 \\ 838 \ \text{Fixed} \\ \end{array}$	66388 ± 96 11125 ± 705 927 ± 28	
Configuration interaction $R^1(fp, d^2)$ $R^3(fp, d^2)$ $R^3(fp, sd)$ $R^3(fp, sd)$ $R^2(dd, ds)$ $R^2(fd, fs)$ $R^3(fd, sf)$	-1583 ± 122 1655 ± 308 6590 ± 341 0 Fixed 16940 ± 621 0 Fixed 0 Fixed	3115 ± 105 0 Fixed 5355 ± 730 0 Fixed 15820 ± 1295	
rms error in calculated levels	$89~{ m cm}^{-1}$	47 cm ⁻¹	

interaction for the electron $l; E^1, E^2$, and E^3 are linear combinations of the Slater radial integrals defined by Racah [14] which arise from the electrostatic interaction within an f^n shell; B and C are linear combinations of Slater integrals defined by Racah [13] for the d^n shell; α and γ are two-body effective interaction parameters acting within the f^n shell which have the coefficients L(L+1) and 12g(U), respectively, where L refers to the orbital angular momentum in the f^n shell and

g(U) are the eigenvalues of the Casimir operator $G(G_2)$ tabulated by Racah [14]; E_s is the two-body effective interaction parameter for nonequivalent electrons proposed by Sack [20] and is used here for the $5d^24f$ configuration; R^k are the radial integrals arising from configuration interaction.

4.1. The $4f^26p + 5d^24f + 4f5d6s$ Complex

These three configurations are analogous to the Ce III group 4f6p, $5d^2$, and 5d6s treated theoretically by Z. Goldschmidt [15]. She found strong mutual perturbations in Ce III, reporting large mixutres of terms of two configurations in several levels. This accounts for the poor results of Spector's calculation of 4f6p alone [16]. The rms error in his calculated levels is 394 cm^{-1} , while that obtained in reference 15 for the mixture of the three configurations is 47 cm^{-1} .

Following the results in Ce III, I have treated the mixed complex of configurations $4f^26p$, $5d^24f$, and 4f5d6s in Pr III. Initial parameters for the first diagonalization of the energy matrices were obtained from the following sources for the $5d^24f$ and 4f5d6s configurations:

Interaction	Source	Reference
d-d	Ce III 5d2	15
d-s f-s	Ce III 5 <i>d</i> 6 <i>s</i> Pr III 4 <i>f</i> 26 <i>s</i>	15 19
d-f	Pr III $4f^25d$	17
$\zeta_d(5d^2)$ $\zeta_d(5d)$	Ce III 5 <i>d</i> ² Ce III 5 <i>d</i> 6s	15 15
ζ_f	Pr IV 4f6s	18

The matrices for these configurations were diagonalized without configuration interaction to determine the correspondence with the observed levels. This was accomplished by means of the experimentally identified LS composition of many of the levels. The parameters were then improved by least squares adjustment to fit the observed levels and further improved by several repetitions of these steps. Because of the small number of known levels of 4f5d6s, fixed ratios were assumed for F^2/F^4 , G^1/G^3 , and G^1/G^5 of the f-d interaction as well as fixed values of $G^3(f,s)$ and ζ_f . The refined parameter values then served as initial parameters for the first diagonalization with configuration interaction.

Spector has treated the $4f^26p$ configuration of Pr III theoretically [19] and obtained an rms error of 198 cm⁻¹ for his calculated levels. His results served here for initial parameters of this configuration.

Initial values for the configuration interaction parameters $R^1(fp,d^2)$ between $4f^26p$ and $5d^24f$, $R^1(fp,ds)$ between $4f^26p$ and 4f5d6s, and $R^2(d^2,ds)$ between $5d^24f$ and 4f5d6s were taken from the Ce III results [15]. All other configuration interaction parameters were initially set equal to zero.

Several sequences of diagonalization and adjustment of the parameters were carried out to obtain convergence before attempting to evaluate the less sensitive interaction parameters. Then the parameters $R^2(fd,fs)$ and $R^3(fd,sf)$ which act between the $5d^24f$ and 4f5d6s configurations, and $G^3(fs)$ of the latter configuration were added. These were found to be undefinable in the least squares calculations (their standard errors exceeded their values) because too few levels of 4f5d6s are known. They were therefore fixed at the following values:

$$R^2(fd, fs) = R^3(fd, sf) = 0$$

 $G^3(fs) = 2100 \text{ cm}^{-1}.$

Finally, values for $R^3(fp, d^2)$ and $R^3(fp,sd)$ were sought. The latter was undefinable and was therefore fixed at zero. The iterative fitting procedure was again brought to convergence, with an rms error of 119 cm⁻¹ for the calculated levels.

Goldschmidt's success in utilizing the Sack [20] effective two-body interaction operators $E_1L(L+1)$ and $E_sS(S+1)$ acting on the final L and S of the levels of 4f5d in Ce III [15] suggested their use for the $4f^26p$ and $5d^24f$ configurations of Pr III. For these configurations, following Sack, the operators are $E_l[L(L+1)-L_c(L_c+1)]$ and $E_s[S(S+1)-S_c(S_c+1)]$, where L_c and S_c refer to the $4f^2$ or $5d^2$ core terms. A well defined value was obtained only for E_s of $5d^24f$. The addition of this parameter reduced the rms error to its final value of $89~\rm cm^{-1}$.

In table III the final values for the parameters derived from the mixing of the three configurations are given. In all least squares calculations the ratios F^2/F^4 . G^1/G^3 , and G^1/G^5 of the 4f5d6s configuration were fixed at the values taken by the corresponding parameters of $5d^24f$ in the preceding calculation. Also the parameter ζ_f of 4f5d6s was required to be equal to ζ_f in $5d^24f$. The remaining free parameters common to these two configurations, namely F^2 ,

 G^1 , and ζ_d , took nearly equal values in both configurations. It is interesting to note that they are nearly equal to the corresponding parameters of the 4f5d configuration [18] of Pr IV.

Included in table III are the corresponding parameters of Ce III evaluated by Goldschmidt [15] and the parameters of the $4f^2$ configuration of Pr IV [21] included for comparison with $4f^26p$ core interactions.

Table IV contains all the calculated levels of the three configurations, all the experimental levels assigned to these configurations, and the squares of the components of the eigenvectors of the calculated levels (their percentage composition). A maximum of three components is given for each level, but less are shown when the sum represents 90 percent or more of the composition. Where a level contains 20 percent or more of the eigenvectors of two configurations, both are indicated in the column labeled "configuration" by means of an "X".

The highest purity of eigenvectors for $4f^26p$ is of course obtained in J_{ij} -coupling because of the large value of ζ_p and the small electrostatic interaction between the f and p electrons. The designation of the energy levels in this scheme gives the $4f^2$ core level in parentheses followed by the j of the 6p electron (1/2 or 3/2).

The coupling is much less pure in $5d^24f$. Here the electrostatic interactions within the $5d^2$ shell and between 5d and 4f are both strong. Therefore, no preferred order of coupling of electrons occurs. The basis states are calculated in an LS scheme in which the d electrons are first coupled and the f electron is then added. In table IV the $5d^2$ core term is given in parentheses followed by the final LS term. The large values of $\zeta(5d)$ and $\zeta(4f)$ give rise to intermediate coupling. I transformed the eigenvectors to the $(d^2)J_1(f)j$ scheme and found higher purity for a few levels, but the average purity for the configuration is lower than in the LS scheme.

Table IV. Calculated energy levels and compositions of the mixed 4f²6p, 5d²4f, and 4f5d6s configurations of Pr III.

The $4f^26p$ levels are designated in f_{1j} -coupling. The levels of $5d^24f$ and 4f5d6s are designated in LS-coupling, with those of 4f5d6s distinguished by the symbol *. Levels attributed to two configurations contain 20 percent or more of each

	Levels	Levels	Obs.	Obs. Configuration								
<i>J</i>	calculated (cm ⁻¹)	observed (cm ⁻¹)	minus calc.	4f26p	$5d^24f$	4f5d6s			Composition			
$0\frac{1}{2}$	63030 64988 66481 68973 70262 72188 74970 78311 79409 79703	66325 78313 79742	-156 2 39	X X X X	X X X X X X		(3F)2S (3F)2S (3F)2S (3F)3/2 (1D)2P (3F)4P (3F)4D (3F)2P (1D ₂)3/2 (3P ₀)1/2 (3P ₁)1/2	31%, 41%, 81%, 31%, 74%, 62%, 37%, 68%, 72%,	(3F)4D (3F)4D (3F)2S (3F)2P (3F)2S (3F)2P (1D)2P (3P ₂)3/2 (1D ₂)3/2 (3P ₀)1/2	23%, 30%, 4%, 24%, 19%, 13%, 30%, 11%, 16%	$^{(3}F)^{2}P$ $^{(3}F_{2})3/2$ $^{(3}F)^{4}D$ $^{(3}F)^{4}D$ $^{(3}F)^{4}D$ $^{(3}P)^{4}D$ $^{(3}P_{0})1/2$	19% 11% 3% 23% 12% 18% 9%
	83375 84984 87650 89556 92742 97264 101423 111001		Ů,	X	X	X X X X	(3P ₁)3/2 (3P ₂)3/2 (1G) ² P *(3D) ⁴ D *(3P) ⁴ P *(3P) ² P *(1P) ² P (1S ₀)1/2	51%, 47%, 91% 91% 90% 90% 89%, 94%	$(^{3}P_{2})^{3/2}$ $(^{3}P_{1})^{3/2}$ $(^{3}P_{1})^{3/2}$	35%, 37%, 5%	*(3P)4P (1G)2P	6% 6%

Table IV. Calculated energy levels and compositions of the mixed $4f^26p$, $5d^24f$, and 4f5d6s configurations of Pr III.—Continued The $4f^26p$ levels are designated in J_i -coupling. The levels of $5d^24f$ and 4f5d6s are designated in LS-coupling, with those of 4/5d6s distinguished by the symbol *. Levels attributed to two configurations contain 20 percent or more of each

,	Levels	Levels	Obs.		Configuratio	n			Commencial		
J	calculated (cm ⁻¹)	observed (cm ⁻¹)	minus calc.	$4f^26p$	$5d^24f$	4f5d6s			Composition		
11/2	63142 65166 65639 66828 67916 68942 69488 70631 71456 71988 73947 74066 74509 75415 76826 78963 80190 80878 82573 82926 84003 84494 85279 87031 89214 90681 92797 95092 96994 103051	63221 66867 67965 71501 74464 75410 76892 78889 80164 80898 82492 83026 84410	79 39 49 45 -45 -5 66 -74 -26 20 -81 100 -84	X X X X X X X X X	X X X X X X X X X X X X X X X X X X X	X X X X X X	(3F ₂)1/2 (3F)4D (3F)4F (3F ₂)3/2 (3F ₃)3/2 (3F) ² P (3F) ² P (3P) ² D (3P) ⁴ F (3P) ⁴ F (3P) ⁴ F (1D ₂)1/2 (3F) ³ D (1D ₂)3/2 (3P ₁)1/2 (3P ₁)3/2 (3P ₁)3/2 (3P ₁)3/2 (3P ₁)3/2 (3P ₁)3/2 (3P ₁)3/2 (3P ₂)3/2 (1G) ² P *(3D) ⁴ D *(3D) ⁴ D *(3D) ⁴ D *(3P) ⁴ P *(3D) ⁴ D *(3P) ⁴ P *(3P) ⁴ P	91%, 76%, 76%, 76%, 91% 41%, 82%, 35%, 31%, 20%, 76%, 88%, 75%, 44%, 43%, 31%, 62%, 65%, 66%, 76%, 76%, 76%, 76%, 76%, 76%, 76	(3P)4D 13%, (3F)3/2 10%, (3F)4F 7%, (1D)2P 13%, (3F)4S 5%, (3F)4S 16%, (3F)4S 25%, (3P)4D 17%, (3P)4D 27%, (3P)4D 27%, (3P)2D 18%, (3F)2D 26%, (3P)2D 38%, (1D)2P 27%, (3P)2D 38%, (1D)2)1/2 8%, (1D)2)1/2 5%, (1D)2)1/2 7%, (1D)2)1/2 7%, (1D)2)1/2 5%, (3P)3/2 11%, (1G)2P 6%, (3P)3/2 11%, (1G)2P 6%, (3P)3/2 11%, (1G)2P 16%, (3P)3/2 15%, *(3P)3/2 15%, *(3P)3/2 15%, *(3P)3/2 15%, *(3P)3/2 15%, *(3P)3/2 15%, *(3P)3/2 15%, *(3P)3/2 15%, *(3P)3/2 15%, *(3P)3/2 16%, *(3P)3/2 16%, *(3P	(3F) ² P (3F) ⁴ F (3F) ⁴ D (3F) ⁴ D (3F) ² P (1D) ² P (3P) ⁴ D (1D) ² D (3F) ² D (3F) ² P (3F) ² P (3F) ² P (3F) ² P (1G) ² P (1G) ² P (1G) ² D (1G) ² D	109 59 59 109 149 149 159 79 49 59 159 49 129 139 79 49 49 59 59 59 59 59 59 49 49 59 59 49 49 149 159 59 49 49 159 59 59 59 59 59 59 59 59 59 59 59 59 5
$2\frac{1}{2}$	61698 63544 64396 64817 66014 66571 66994 67361 68288 68991 69359 69572 70369 71504 72007 74168 74744 75354 75782 76491 77944 79360 81472 83359 84317 84710 84986 85323 85904 88297 90038 91295 92422 94069	61718 63576 64401 64818 65909 66681 66943 67395 68979 69682 71536 71995 74105 75561 75615 77822 79367 81405 83427	$\begin{array}{c} 20 \\ 32 \\ 5 \\ 1 \\ -105 \\ 110 \\ -51 \\ 34 \\ -12 \\ 110 \\ \\ 32 \\ -12 \\ -63 \\ \\ 207 \\ -167 \\ -122 \\ -67 \\ 68 \\ \\ -17 \\ \end{array}$	X X X X X X X X X X X X X X X X X X X	X X X X X X X X X X X X	X X X X X X	("S ₀)3/2 ("H ₄)3/2 ("F ₂)1/2 ("F ₃)1/2 ("F ₃)1/2 ("F ₃)3/2 ("F ₃)3/2 ("F ₃)3/2 ("F ₃)3/2 ("F ₃)3/2 ("F ₃)3/2 ("P ₃)3/2 ("P ₃)3/2 ("P ₃)3/2 ("P ₃)2 ("O ₂)1/2 ("P ₂)1/2 ("P ₂)3/2 ("P ₁)3/2 ("G)2P ("P ₂)3/2 ("P ₁)3/2 ("G)2P ("P ₂)3/2 ("P ₁)3/2 ("G)2P ("P ₁)3/2 ("S ₁)3/2 ("O ₂)4C ("S ₁)3/2 ("S ₁)3/2	72%, 75%, 75%, 31%, 47%, 524%, 44%, 38%, 41%, 36%, 27%, 62%, 35%, 60%, 27%, 70%, 79%, 83%, 79%, 43%, 52%, 52%, 84%, 52%, 54%, 66%, 52%, 60%, 60%, 60%, 60%, 60%, 60%, 60%, 60	(3F ₂)1/2 18% (3H ₄)3/2 20% (3F) ⁴ D 7%, (3F) ⁴ G 27%, (3F) ⁴ G 27%, (3F) ⁴ G 27%, (3F) ⁴ F 14%, (3F) ³ /2 14%, (3F) ³ /4 22%, (3F ₄)3/2 35%, (3F) ² D 22%, (3F) ⁴ P 35%, (3F) ⁴ P 35%, (3F) ⁴ P 23%, (3P) ⁴ P 23%, (3P) ⁴ D 12%, (1D) ² D 10%, (1D) ² D 10%, (1D) ² F 19%, (3F) ² F 5%, (3F) ² F 5%, (3F) ² F 13%, (3F) ² F 13%, (3F) ² F 19%, (3F) ² F 18%, *(3F) ⁴ F 19%, *(3F) ⁴ F 1	(\$F) ² F (\$F3)3/2 (\$D) ² F (\$F3)3/2 (\$F) ² F (\$F3)3/2 (\$F) ² F (\$F) ⁴ D (\$F) ⁴ D (\$F) ⁴ D (\$P2)1/2 (\$F) ⁴ P (\$D) ² F (\$D) ² F (\$D) ² D (\$P2)1/2 (\$P3)1/2 (\$P3)1/2 (\$P3)1/2 (\$P3)1/2 (\$P3)1/2 (\$P4)1/2 (\$P3)1/2 (\$P4)1/2 (\$P4)1/2 (\$P5)1/2 (\$P	69 169 9% 59% 119 1149 169 109 139 59 77 22 46% 149 169 199 79 99 109 119 39 99 119 119 119 119 119 119 119

Table IV. Calculated energy levels and compositions of the mixed 4f²6p, 5d²4f, and 4f5d6s configurations of Pr III.—Continued
The 4f²6p levels are designated in J₀-coupling. The levels of 5d²5f and 4f5d6s are designated in LS-coupling, with those of 4f5d6s distinguished by the symbol *. Levels attributed to two configurations contain 20 percent or more of each

	Levels	Levels	Obs.		Configuration	n					
J	calculated (cm ⁻¹)	observed (cm ⁻¹)	minus calc.	4f26p	$5d^{2}4f$	4f5d6s			Composition		
$3\frac{1}{2}$	58164 60524 61560 63260 63807 64992 65265 65932 66949 67280 67624 68221 68511 68789 69184 69492 71450 72005 73316 74550 75309 76550 78374 79226 81357 84135 84418 85860 86122 86381 87602 90636 92022 92476 94002 96948	58158 60520 61605 63232 63769 64980 65296 65935 66853 67240 67679 68332 68492 68802 68987 69431 71386 71979 73378 75294 78463 79396 84431	-6 -4 45 -28 -38 -12 31 3 -96 -40 55 111 -19 13 -197 -61 -64 -26 62 -15 89 170 13 -90 -34 -35 -118	X X X X X X X X X X X X X	X X X X X X X X X X X X X X X X X X X	X X X X X X X	(3H ₄)1/2 (3F) ⁴ H (3H ₄)3/2 (3F) ⁴ H (3H ₅)3/2 (3F ₄)1/2 (3F ₃)1/2 (3F ₃)1/2 (3F) ⁴ F (3F) ⁴ G (3F) ⁴ F (3F) ⁴ H (3F) ⁴ H (3F) ⁴ H (3F) ⁴ H (1D) ² F (1D) ² F (1D) ² F (1D) ² F (1D) ² S (3F) ⁴ H (3P) ² G (3F) ⁴ H (3P) ² G (3F) ⁴ H (3P) ² G (3F) ⁴ F (1D) ² F (1D) ² F (1D) ² F (1D) ² S (3F) ² F (3F) ² G (3F) ⁴ F (3F) ² G (3F) ⁴ F (3F) ² F (3F) ² F (3F) ⁴ F (3F) ² F (3F) ² F (3F) ⁴ F (3F) ² F	82%, 43%, 43%, 42%, 47%, 46%, 45%, 22%, 47%, 58%, 32%, 22%, 37%, 29%, 19%, 18%, 58%, 65%, 65%, 66%, 74%, 46%, 73%, 85%, 57%, 32%, 32%,	(\P)^4\therefore 6%, (\P)^2\Green 33%, (\P)^2\Green 7%, (\P)^2\Green 20%, (\P)^2\Green 20%, (\P)^2\Green 20%, (\P)^4\Green 12%, (\P)^4\Green 12%, (\P)^4\Green 12%, (\P)^4\Green 15%, (\P)^4\Green 11%, (\P)^2\Green 12%, (\P)^2\Gre	(3H ₄)3/2 (3H ₄)1/2 (1G ⁴)3/2 (3F) ² F (3F) ⁴ G (3F) ² G (3F) ⁴ D (3F)3/2 (3F ₄)1/2 (3F ₂)3/2 (1D) ² G (1D) ² G (1D) ² G (1D) ² F (3F) ² F	44 104 27 77 44 88 66 99 77 77 49 100 55 77 99 100 222 44 115 100 48 88
$4\frac{1}{2}$	58244 60160 61332 61971 62508 63560 64271 64929 66953 67412 67815 68349 68683 69181 69529 70999 71641 73119 73690 74675 75636 77169 81428 84446 85028 86442 88134 89017 90557 95075 99782	58174 60166 61357 62063 62536 63593 64236 64857 67049 67399 67871 68375 68544 69138 69686 71021 71592 73030 73606 75762 84411	770 6 25 92 28 33 -35 -72 96 -13 56 26 -139 -43 157 22 -49 -89 -84 126 -35	X X X X X X X X X X	X X X X X X X X X X	X X X X X X X	(3H ₄)1/2 (3H ₄)3/2 (3H ₅)1/2 (3F) ⁴ I (3F) ² G (3H ₅)3/2 (3F) ⁴ H (3F ₄)1/2 (3H ₆)3/2 (1D) ² H (3F ₃)3/2 (1G ₄)1/2 (3F) ⁴ G (3F) ⁴ G (1G ₄)3/2 (3F) ⁴ G (1G) ² G (3F) ⁴ G (1G) ² G (3F) ² H (1G) ² G (3F) ² H (1G) ² G (3F) ⁴ H (3G) ⁴ G *(3F) ⁴ F *(3F) ⁴ F	95%, 79%, 53%, 44%, 33%, 67%, 46%, 57%, 36%, 42%, 51%, 38%, 85%, 46%, 78%, 35%, 54%, 57%, 39%, 79%, 79%, 77%, 85%,	(3H ₄)3/2 7%, (3F) ⁴ 1 19%, (3H ₄)3/2 32%, (3F) ⁴ H 27%, (3F) ⁴ H 11%, (3H ₅)3/2 24%, (1G ₄)1/2 12%, (3F) ² H 20%, (3F) ² H 20%, (3F) ⁴ G 26%, (3F) ⁴ G 27, (3F) ⁴ G 28%, (3F) ⁴ G 17%, (3F) ⁴ H 25%, (1G) ² H 21%, (3F) ⁴ H 21%, (3F) ⁴ H 21%, (3F) ⁴ H 21%, (3F) ⁴ H 34%, (4G) ² G 28%, *(4H) ² H 34%, *(3F) ⁴ H 34%, *(4G) ² G 24%, *(3F) ⁴ H 35%, *(1G) ² G 35%, (1D) ² H 5%, (1D) ² H 5%, (1D) ² H 5%, (1D) ² G 8%, (1G) ² G 8%, (1G) ² G 8%,	(3F) ⁴ H (3H ₅)1/2 (3F) ² G (3F) ⁴ I (3F) ² G (3F) ² G (3H ₆)3/2 (1D) ² H (3H ₆)3/2 (3F ₄)3/2 (3F ₄)3/2 (3F ₃)3/2 (3P) ⁴ G (1D) ² G (1D) ² G (1D) ² H (1D) ² H (1D) ² H (1D) ² G *(3H) ⁴ H (1I ₆)3/2 *(3F) ⁴ F *(1G) ² G *(1G) ² G *(1G) ² G	7 12 9 27 11

TABLE IV. Calculated energy levels and compositions of the mixed 4f²6p, 5d²4f, and 4f5d6s configurations of Pr III. — Continued
The 4f²6p levels are designated in Jy-coupling. The levels of 5d²4f and 4f5d6s are designated in LS-coupling, with those of 4f5d6s distinguished by the symbol *. Levels attributed to
two configurations contain 20 percent or more of each

	Levels	Levels	Obs.		Configuratio	n					
J	calculated (cm ⁻¹)	observed (cm ⁻¹)	minus calc.	4f26p	$5d^24f$	1/5d6s			Composition		
$5\frac{1}{2}$	60465	60420	-45	X			(3H ₅)1/2	94%			
	62243 62569	62241 62559	$-2 \\ -10$	XX			(3H ₄)3/2 (3H ₆)1/2	40%, 55%,	(³ H ₆)1/2 35%, (³ H ₄)3/2 37%	$(^{3}H_{5})3/2$	15%
	63811	63817	6	X	X		(3F)4I	50%,	$(^{3}H_{5})3/2 24\%$	$(^{3}H_{4})3/2$	15%
	64074	64151	77	X	X		(3F)4I	42%,	$(^{3}H_{5})3/2$ 39%,	(3F)4H	6%
	64951	64865	-86		X		(3F)4H	73%,	$(^{3}H_{5})3/2$ 15%		
	65912	65922	10	X			$(^{3}H_{6})3/2$	88%,	$(^{3}F)^{4}H$ 4%		
	68184	68238	54		X		(3F)2I	51%,	$({}^{1}G){}^{2}I$ 36%,	(3F)4H	6%
	68514	68526	12	X			$(^{3}F_{4})3/2$	53%,	$({}^{1}G_{4})3/2 20\%,$	(3F)4G	14%
	69455	69409	-46		X		(3F)2H	37%,	$(^{1}D)^{2}H$ 25%,	(3F)4G	11%
	69924	69978	54		X		(3F)4G	62%,	$(^{1}D)^{2}H$ 11%,	(3P)4G	8%
	71714	71736	22	X	37		$({}^{1}G_{4})3/2$	65%,	$({}^{3}F_{4})3/2 29\%$	(1C)9II	001
	73535	73609	74		X		(3P)4G (3F)2H	76%,	(3F) ² H 9%, (¹ D) ² H 18%,	(¹G)²H (¹G)²I	8% 16%
	75641	75640	-1		X		(³ F) ² H (¹ G) ² H	32%,	(¹ D) ² H 18%, (¹ D) ² H 27%,	(³ P) ⁴ G	9%
	76097	78695	- 174		X		(1G)2H (1G)2I	56%. 35%.	$(^{3}F)^{2}I$ 25%,	(3F)2H	12%
	78869 80312	80361	-174 49	X	Λ		$({}^{1}I_{6})1/2$	80%,	$({}^{3}F)^{2}I$ 25%, 6% ,	(1G)2I	6%
	83729	83607	-122	X			$({}^{1}I_{6})3/2$	87%,	$({}^{1}I_{\theta})1/2$ 7%	(0)1	0 / 0
	87519	05007	122	A		X	*(3H)4H	95%	(191/2 170		
	90049	90120	71			X	*(3G)4G	96%			
	93283	93296	13			X	*(3H)2H	80%,	*(1H)2H 9%.	*(3H)4H	5%
	99971	30230	10			X	*(1H)2H	82%,	*(3H)2H 10%		
$6\frac{1}{2}$	62725	62679	-46	X			(3H ₆)1/2	89%,	(3H ₆)3/2 6%		
	64218	64215	-3	X			$(^{3}H_{5})3/2$	86%,	$(^{3}\text{H}_{6})3/2$ 8%		
	65944	65967	23		X		(3F)4I	86%,	(3F)4H 5%	(011) 0 (0	1000
	66091	66148	57	X	X		$(^{3}\text{H}_{6})3/2$	51%,	(3F)4H 25%,	$(^{3}H_{5})3/2$	12%
	66872	66736	-136	X	X X X		(3F)4H	53%,	$(^{3}\text{H}_{6})3/2 32\%,$	(3F)4I (3F)4H	6% 12%
	70452	70381	-71		X	1 1 1 1 1 1 1	(3F)2I (1G)2K	53%, 96%	$({}^{1}G){}^{2}I$ 29%,	(aL).II	12%
	77201	70106	110		X		(¹G)²K (¹G)²I	96% 51%.	$(^{3}F)^{2}I$ 26%,	$({}^{1}I_{6})1/2$	17%
	79246 80743	79136 80989	$-110 \\ 246$	X	X		$({}^{1}I_{6})1/2$	51%, 70%,	$({}^{1}G){}^{2}I$ 26%, $({}^{1}G){}^{2}I$ 12%,	$({}^{3}F){}^{2}I$	9%
	83713	80989	-10	X	Λ		$\binom{1_6}{1_6} \frac{1}{2}$	87%,	$({}^{1}I_{6})1/2 11\%$	(-1-)-1	370
	89758	65705	-10	Α		X	*(3H)4H	100%	(16)1/2 11/0		
$7\frac{1}{2}$	66298	66301	3	X		1 5 3	(3H ₆)3/2	96%			
-	68285	68305	20		X		(3F)4I	95%			
	79787				X		(1G)2K	98%			
	84999	84992	-7	X			$({}^{1}I_{6})3/2$	98%			

The $5d^24f$ configuration is illustrated in figure 1. The observed levels are represented by solid lines and the calculated positions of unknown levels are given as dashed lines. The term designations represent the major components, although in many cases these are less than 50 percent. The identity of a unique major component in some cases is impossible. In spite of the intermediate coupling, the low-lying quartets exhibit a regularity in their structure characteristic of LS-coupling. This is also true of the equally complex $4f^25d$ configuration of the same ion [1]. Judd has shown that this structure arises from the near equality of $\zeta(4f)$ and $\zeta(5d)$, which results in nearly null nondiagonal matrix elements between terms of maximum multiplicity [22]. The structure of the (3F)4H0 term is distorted by the strong mixture with (3F)2G0.

The coupling in 4f5d6s is LS, but not very pure because of the large spin-orbit interactions. The basis states were constructed by first coupling the f and d electrons to form parent terms and then adding the s electron. If more levels had been found, it would probably have been possible to define parameters E_l and E_s for this configuration since they have been essential to other configurations of PrIII and CeIII containing both 4f and 5d electrons.

4.2. The $4f^25f$ Configuration

This is a well-isolated configuration which is quite amenable to individual treatment. The correspond-

Table V. Fitted parameter values and associated standard errors for the $4f^25f$ configuration of Pr III and corresponding parameters of Ce III in units of cm^{-1}

Parameters	Pr III	Се п		
	$4f^{2}5f$	4 <i>f</i> 5 <i>f</i>		
	118394 ± 16	101544 ± 12		
f ²)	$ \begin{array}{ccc} 4983 & 9 \\ 22.99 \pm & 0.05 \end{array} $			
	479 ± 1			
	22.7 ± 0.4			
	-56 Fixed			
ff')	3150 ± 53	3150 ± 90		
	1870 ± 160	1420 ± 220		
	490 ± 190	$736 \pm ?$		
	931 ± 9	1175 ± 14		
	1511 ± 71	1530 ± 110		
	1220 ± 170	870 ± 330		
	847 ± 140	$736 \pm ?$		
f^2)	760 ± 2	639 ± 7		
	22 ± 3	26 ± 8		
ms error in	28 cm^{-1}	39 cm^{-1}		

ing configuration 4/5 f of Ce III reported in reference 3 was treated theoretically by Spector [16], who obtained an rms error in the level predictions of 39 cm⁻¹.

As was found in the Ce III work, the highest purity of eigenvectors results from the use of the J_1l -coupling scheme. However, due to the large value of the exchange parameter $G^0(f')$, substantial LS-components are obtained when the calculation is carried out in the LS-scheme. Analogous to Ce III, this condition permitted the experimental assignment of many LS terms on the basis of line intensities due to transitions to the LS-coupled $4f^25d$ configuration. These LS designations were essential in establishing the correspondence between the observed and calculated levels.

Initial parameter values were obtained from the $4f^2$ configuration of Pr IV for the $4f^2$ core interactions and from Spector's results in Ce III for the f-f' interaction as well as for $\zeta(5f)$.

Because no levels based on $4f^2(^3P)$ or (^1S) are known only 4 electrostatic core parameters could be fit to the 5 observed core terms. Therefore the "effective" interaction parameter γ was fixed at -56 cm⁻¹, the value obtained by S. Feneuille and N. Pelletier-Allard [23] in a recent calculation of $4f^2(6s+5d)$ of PrIII. The free parameters did not change significantly from their initial values.

All observed levels of odd parity in this region were fitted to the $4f^25f$ configuration. The final rms error in the calculated level positions was 28 cm^{-1} . The resulting parameters are given in table V along with the corresponding ones of 4f5f of Ce III.

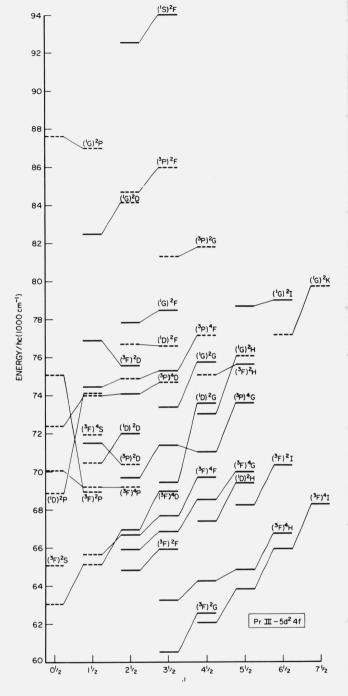


FIGURE 1. Energy levels of the 5d²4f configuration of Pr III. Levels not observed are represented by dashed lines at their calculated positions.

The calculated and observed energy levels and eigenvectors of $4f^25f$ in J_1l -coupling are given in table VI. The designations show the $4f^2$ core level followed by the quantum number $K = (J_1 + l)$ in square brackets. Because of the importance of the LS-coupling designations in the theoretical analysis they are included in a column containing the largest component in this scheme.

 $\label{eq:table_viscosity} TABLE~VI.~~\textit{Calculated energy levels and compositions of the 4f2f$ configuration of Pr III.}\\ Designations are in J_1l-coupling}$

J	Levels calculated (cm ⁻¹)	Levels observed (cm ⁻¹)	Obs. minus Calc.	Composition in J_1l -coupling	$Largest$ component in LS -coupling
$0\frac{1}{2}$	111748 115693 116909 117392 118943 120507 128370 134088			$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(3H) 4D 92% (3F) 2S 41% (3F) 4P 60% (3F) 4D 65% (3F) 2P 61% (1G) 2P 80% (1D) 2P 88% (3P) 4D 92%
$1\frac{1}{2}$	111267 111755 113803 115948 116812 117552 118154 118260 119010 121489 122588 128163 128942 132798 133895 134173	111269 113826 117540 118201	2 23 -12 47 51	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(3H) ⁴ F 80% (3H) ⁴ D 54% (3H) ² D 45% (3F) ⁴ P 70% (3F) ² P 37% (3F) ² P 24% (3F) ⁴ F 34% (3F) ⁴ F 62% (1G) ² P 43% (1G) ² P 43% (1D) ² P 83% (1D) ² P 83% (3F) ⁴ F 62% (3F) ⁴ F 62%
2½	111489 111928 113542 113902 115831 116471 116711 117609 117651 118612 118952 120686 121763 128590 128833 132127 132709 133044 133832 134221 136510 163236	111495 113557 113914 115800 116727 117686	6 15 12 -31 16 35	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(3H) ⁴ F 59% (3H) ⁴ G 52% (3H) ⁴ D 23% (3H) ² F 38% (3H) ² P 47% (3F) ⁴ F 50% (3F) ⁴ F 50% (3F) ⁴ F 42% (3F) ⁴ F 53% (1G) ² F 53% (1G) ² F 53% (1G) ² F 83% (1D) ² F 83% (1D) ² D 82% (3P) ⁴ G 64% (3P) ² D 37% (3P) ⁴ F 28% (11) ² F 41% (3P) ⁴ D 55% (3P) ⁴ D 55%
$3\frac{1}{2}$	110340 111381 113308 113639 115405 115672 116021 117029 117671 118143 118321 118967 121401 121599 128456 129012 132256 132760 132869	110334 111343 113292 113631 115421 115670 116022 117045 117647 118319	-6 -38 -16 -8 16 -2 1 16 -24 -2	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(3H) ⁴ H 81% (3H) ² G 40% (3H) ⁴ F 44% (3H) ⁴ G 51% (3H) ⁴ D 35% (3F) ⁴ H 82% (3H) ² F 42% (3F) ² F 21% (3F) ² F 33% (3F) ⁴ D 40% (3F) ² G 41% (3F) ² G 45% (1G) ² F 36% (1G) ² F 36% (1D) ² C 86% (1D) ² F 86% (3P) ⁴ G 41% (3P) ² G 37% (3P) ⁴ G 37%

	Designations are in Me-coupling									
J	Levels calculated (cm ⁻¹)	Levels observed (cm ⁻¹)	Obs. minus Calc.	Composition in $J_1 l$ -coupling	Largest component in LS-coupling					
	133585 134108 134896 136377 163249	1		$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(¹ I) ² F 42% (³ P) ⁴ F 54% (¹ I) ² G 48% (³ P) ² F 54% (¹ S) ² F 99%					
$4\frac{1}{2}$	110906 111915 113154 113783 115334 115519 115841 116456 117516 118076 118495 118911 121376 122121 128360 128584 132719 133285 133459 134030 135078	110922 111993 113159 113780 115324 115500 116453 118081 118469 121383 128353 128569	16 78 5 -3 -10 -19 -3 -26 7 -7 -15	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(3F)4H 70% (3F)2I *58% undefined (3H)2H 35% (3H)4F 35% (3H)4F 35% (3H)4H 71% (3P)4H 54% (3F)2G 36% (3F)2G 36% (3F)4G 36% (3F)4G 36% (3F)4G 36% (1G)2G 45% (1D)2H 77% (1D)2G 78% (3P)4G 48% (1D)2G 48% (1D)2G 43% (3P)4G 48% (3P)4G 48% (3P)4G 48% (3P)4G 48% (3P)4G 48% (3P)4G 56% (3P)4G 56% (3P)4G 56% (3P)4G 55% (3P)2G 54%					
5½	110308 110876 112636 113664 115402 115934 116276 117320 117577 118304 118926 121078 121546 128364 133162 133322 133955	110295 110881 112643 113664 115403 115933 116309 117323 117574 118272 118879 121095 121532 128382	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	(3H) 4K 74% (3H) 2I 41% (3H) 4H 61% (3H) 4I 67% (3H) 2H 34% (3H) 4G 41% (3F) 4I 31% (3F) 4H 28% (3F) 2I 48% (3F) 2I 48% (3F) 2H 40% (1G) 2H 40% (1G) 2I 31% (1D) 2H 88% (1I) 2I 83% (1I) 2H 76% (3P) 4G 83%					
$6\frac{1}{2}$	110535 111115 112756 113570 114792 115369 117263 117762 118629 120502 121437 132708 133181	110531 111110 112770 113600 114797 115408 117248 117775 118611 120499 121431	$ \begin{array}{r} -4 \\ -5 \\ 14 \\ 30 \\ 5 \\ 39 \\ -15 \\ 13 \\ -18 \\ -3 \\ -6 \end{array} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	(3H) ⁴ L 89% (3H) ⁴ K 59% (3H) ² I 39% (3H) ² K 43% (3H) ⁴ H 48% (3H) ⁴ I 60% (3F) ⁴ H 54% (3F) ⁴ I 61% (3F) ² I 55% (¹ G) ² I 56% (¹ G) ² K 44% (¹ I) ² K 100% (¹ I) ² I 99%					
$7\frac{1}{2}$	111339 112895 113832 115666 116196 118051 121087 132780 133421	111335 112896 113834 115672 116239 118063 121119	-4 1 2 6 43 12 32 -69	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(3H) ⁴ L 67% (3H) ⁴ K 72% (3H) ² L 76% (3H) ² K 57% (3H) ⁴ I 72% (3F) ⁴ I 65% (¹ G) ² K 67% (¹ I) ² K 98% (¹ I) ² L 98%					

Table VI. Calculated energy levels and compositions of the 4f25f configuration of Pr III.—Continued
Designations are in J₁l-coupling

J	Levels calculated (cm ⁻¹)	Levels observed (cm ⁻¹)	Obs. minus Calc.	Composition in $J_1 l$ -coupling	Largest component in LS-coupling
$8\frac{1}{2}$	113026 114733 116497 133120 133438	113024 114726 116490 133194 133373	-2 -7 -7 74 -65	$^{3}H_{5}[8] 94\%$ $^{3}H_{6}[8] 95\%$ $^{3}H_{6}[9] 89\%, \qquad ^{3}H_{5}[8] 6\%$ $^{1}I_{6}[9] 98\%$ $^{1}I_{6}[8] 97\%$	(³ H) ⁴ L 94% (³ H) ⁴ K 95% (³ H) ² L 89% (¹ I) ² M 98% (¹ I) ² L 97%
$9\frac{1}{2}$	114978 133191	114971 133242	-7 51	$^{3}\text{H}_{6}[9] \ 100\%$ $^{1}\text{I}_{6}[9] \ 100\%$	(³ H) ⁴ L 100% (¹ I) ² M 100%

The energy level structure of $4f^25f$ is shown in figure 2 in J_1l -coupling. Pairs of levels of equal J_1 and K are connected and the $4f^2$ core is indicated. The experimentally derived levels are drawn with solid lines, and those not found are drawn with dashed lines at their calculated positions. By comparing this structure with that of 4f5f of Ce III shown in figure 4 of reference 3, we note a decrease in the pair splittings in Pr III, indicating a trend with increasing Z to purer J_1l coupling. The electrostatic parameter $G^0(ff')$ has decreased by 20 percent from its value in Ce III while $F^2(ff')$ remains unchanged.

4.3. The $4f^26d$ and $4f^27s$ Configurations

Levels of both of these configurations were given in ref. 2, but were all designated as $4f^26d$. They were derived from transitions to $4f^26p$. No distinction between configurations was evident from relative line intensities.

The present analysis of this transition array revealed 26 more levels belonging to the upper two configurations. A clue as to the designation of these levels is the fact that nearly all observed transitions from a given upper level has the same $4f^2$ core level of $4f^26p$ in common. This arises from the condition that both the upper and lower configurations exhibit good J_1j -coupling.

The two configurations $4f^26d$ and $4f^27s$ were expected to overlap because of the arrangement of the corresponding Ce III configurations 4f6d and 4f7s. To unravel them, I calculated their energy levels using the parameters of Ce III for the f-d and f-s interactions, and compared the result with the known levels. It was then possible to recognize the level groupings in the two configurations.

For both configurations, levels based only on the two core levels ${}^{3}\text{H}$ and ${}^{3}\text{F}$ are known. Therefore, only one core electrostatic parameter, namely E^{3} , could be determined. The ratios E^{1}/E^{3} and E^{1}/E^{2} were fixed at the values 10.3 and 216, respectively. These ratios are nearly equal in the configurations [17, 23] $4f^{3}$, $4f^{2}(5d+6s)$, and $4f^{2}6p$ (table III of present work)

of Pr III, and $4f^2$ of Pr IV(see table III). The parameters α and γ of the $4f^2$ core were fixed at the values found in $4f^26s$ of Pr III [23].

The least squares adjustment of the 4f-6d and 4f-7s interaction parameters produced the well-defined values given in tables VII and IX. The corresponding parameters of 4f6d in Ce III are also given. A diagonalization with these final parameters provided the calculated levels and eigenvectors in J_1j -coupling shown in table VIII for the $4f^2(^3H,^3F)$ 6d levels. A complete listing of the calculated results is not given because of the small number of known levels. The eigenvectors were also calculated in the J_1l -coupling scheme. The overall purity of levels was found to be lower than in J_1j , as is the case in Ce III for 4f6d [16].

A diagram of the configurations $4f^2(^3H, ^3F)$ 6d and 7s is given in figure 3. As in figures 1 and 2, observed levels are given as solid lines while those not yet located are represented by dashed lines at their calculated positions. Levels are connected which are based on the same J_1 core level.

Table VII. Fitted parameter values and associated standard errors for the 44°6d configuration of PrIII and corresponding parameters of Ce III in units of cm⁻¹.

Parameters	Pr III	Ce III	
	$4f^26d$	4f6d	
A	108321 ± 20	91509 ± 36	
$E^1(f^2)$	4927 Fixed E^{1}/E^{3}		
\mathbb{E}^2	22.8 Fixed E^2/E^3		
E3	479 ± 2		
χ	23 Fixed		
/	-56 Fixed		
$F^2(fd)$	4070 ± 100	3260 ± 320	
74	2500 ± 190	1730 ± 690	
Ç1	1396 ± 60	1330 ± 180	
G ³	1500 ± 220	540 ± 690	
G ⁵	2590 ± 160	1980 ± 610	
f	766 ± 3	642 ± 20	
Sd	197 ± 7	239 ± 36	
rms error in calculated levels	31 cm ⁻¹	139 cm ⁻¹	

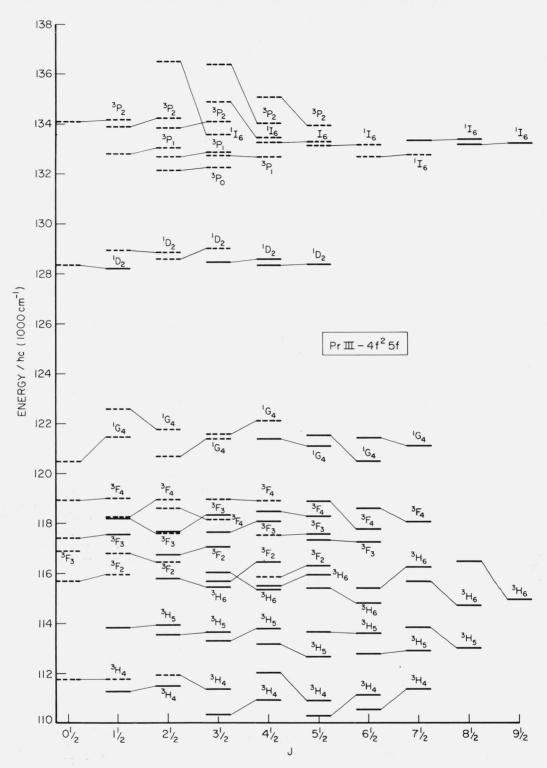


FIGURE 2. Energy levels of the $4f^25f$ configuration of Pr III. Pairs of levels of identical $4f^2$ core and quantum number K in the J_1l -coupling scheme are connected. Levels not observed are represented by dashed lines at their calculated positions.

Table VIII. Calculated energy levels and compositions of the 4f²6d configuration of Pr III. Designations are in J_1j -coupling. Only levels built primarily on $4f^2(^3H)$ and $4f^2(^3F)$ core levels are given.

J	Levels calculated (cm ⁻¹)	Levels observed (cm ⁻¹)	Obs. minus calc.	Composition in J_1j -coupling
01/2	105740 105973 107684			(3F ₂)3/2 92% (3F ₂)5/2 93% (3F ₃)5/2 99%
11/2	101658 106059 106154 107120 107844 108345	2041 2 TO 10		$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$2^{1/2}$	101071 101715 104106 105741 106369 107280 107600 107799 108809	101071 101666	0 - 49	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
31/2	100783 101477 103361 103955 105514 106433 106496 107328 107890 108173 108305	100789 101446 103309 103896	6 -31 -52 -59 -29	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
$4^{1}/2$	100415 100954 102853 103327 105519 106245 106346 107190 107819 107872 108600	100430 100947 102830 103335 105567	15 -7 -23 8 48 -18	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
51/2	100617 101165 102639 103336 104924 105458 107403 107720 108527	100625 101165 102617 103344 104905 105450	8 0 -22 8 -19 -8	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
61/2	101667 102988 103764 105020 105644 107979	101680 102982 103805 105019 105632	$ \begin{array}{c} 13 \\ -6 \\ 41 \\ -1 \\ -12 \end{array} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
71/2	103488 105080 106356	103484 105050	$-4 \\ -30$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
81/2	105513			(3H ₆)5/2 100%

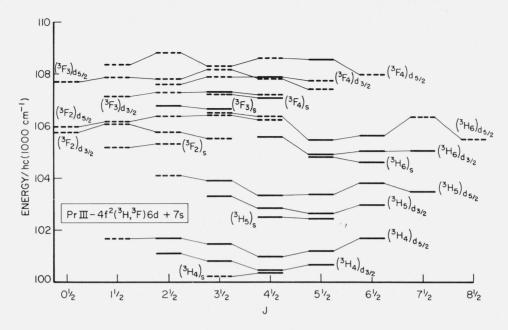


FIGURE 3. Energy levels of the $4f^26d$ and $4f^27s$ configurations of Pr III designated in J_{ij} -coupling. The $4f^2$ core levels are given in parentheses followed by subscript d or s for the 6d or 7s configurations.

Levels not observed are represented by dashed lines at their calculated positions.

4.4. The $4f^28s$ Configuration

Only a few high-lying levels were found by adding the vacuum ultraviolet lines of Pr III to the $4f^26p$ group. These were characterized by the strict adherence of the observed lines to core level selection rules in J_1j -coupling. They were therefore either $4f^27d$ or $4f^28s$ levels. Their pair structure suggested the latter configuration and I attempted to fit them accordingly.

Here again, only levels based on the ³H and ³F core levels were found. Therefore, the same fixed conditions on $4f^2$ core parameters were used as for $4f^26d$ and $4f^27s$. The results of least squares fitting of the remaining parameters are given in table IX. The free core parameters E^3 and ζ_{4f} are practically identical to those found for $4f^26d$ and $4f^27s$. Also, the parameter $G^3(fs)$ shows the same fractional increase from the Ce III value as does the same parameter of $4f^27s$ and $4f^26s$. These results strongly support the interpretation of these levels as $4f^28s$.

5. The Ionization Energy

The present extension of the analysis of Pr III provides a three member $4f^2ns$ series (n=6, 7, 8) which is suitable for a determination of the ionization energy of this ion.

Table IX. Fitted parameter values and associated standard errors for the 4f²7s and 4f²8s configurations of Pr III in units of cm⁻¹.

Parameters	Рг III	Pr III
	$4f^27s$	4f28s
A	$egin{array}{lll} 4950 & { m Fixed} \ E^1\!/E^3 \ 22.9 & { m Fixed} \ E^2\!/E^3 \ 482 & \pm 2 \ 23 & { m Fixed} \ -56 & { m Fixed} \ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
rms error in	27 0111	7 cm ⁻¹

The levels based on the $^3\mathrm{H}$ core term are available in the three configurations, and the purity of these levels is above 90 percent (in contrast to the $^3\mathrm{F}$ levels). Therefore, for the series terms I used the center of gravity of the levels built on the $^3\mathrm{H}$ core. For the missing level in $4f^2(^3\mathrm{H})7s$ and $4f^2(^3\mathrm{H})8s$ the calculated position was substituted. The centers of gravity of

4f²(³H)6s, 7s, and 8s and the fitted effective principal lating energy matrices written by Y. Bordarier and quantum numbers are:

Configuration	c.g. (cm ⁻¹)	n^*
4f ² (³ H)6s	31137	2.6045
$4f^{2}(^{3}\text{H})7s$	102738	3.6535
4f ² (3H)8s	131507	4.6732

The Ritz formula to which these values are fitted is:

$$T = -9R/(n-3.2959-6.8432 \times 10^{-7} T)^2$$
.

To reduce the limit of this series to the lowest limit corresponding to the ionization energy, the center of gravity of the ³H term of $4f^2$ observed in Pr IV [18] was subtracted. This gives the value of 174284 cm⁻¹ for the lowest series limit of Pr III.

The error resulting from the use of this three term series may be estimated from La III [24], where a four term ns series (n=6, 7, 8, 9) is known. The ionization energy derived from this series agrees with those obtained with nf and ng series to within 10 cm⁻¹. By using only the first three terms of the ns series in La III one obtains a value for the ionization energy differing from that given by the four term series by -115 cm^{-1} . I therefore added an equivalent fractional amount to the calculated ionization energy of Pr III obtained from the three term series and estimate the uncertainty to be equal to this quantity. This gives the ionization energy of Pr III as 21.625 eV (174420 cm⁻¹) with an estimated uncertainty of 0.016 eV (130 cm⁻¹).

This procedure for estimating the correction for the quadratic term in the quantum defect is valid if series of this kind generally exhibit the same behavior. It was noted in reference 10 that an examination of the curves of the quantum defect (σ) versus term energy (T) for the ns series of a large number of alkali-like atoms shows that their shapes are similar, and for the same period are practically identical (see table IV of ref. 10). Therefore, the use of the four-member series in La III to estimate the error in the ionization energy derived from a three-member series in PrIII is reasonable.

I am pleased to thank Prof. R. Chabbal, Director of Laboratoire Aimé Cotton, Orsay, France, for making available the excellent computer programs for calcu-

A. Carlier of his staff. My first experience with these programs was gained at his laboratory where part of the present theoretical analysis was carried out.

I also thank Mrs. Z. Goldschmidt for providing NBS with the library of energy matrices compiled at Hebrew University, Jerusalem, Israel, by Prof. G. Racah and his co-workers.

The assistance of Dr. R. Cowan of the Los Alamos Scientific Laboratory in checking for errors in the energy matrices by independently calculating them was extremely valuable.

Dr. V. Kaufman generously contributed the exposures of the Pr spark made with the Eagle vacuum spectrograph.

6. References

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Table X. Observed spectral lines of Pr III in the vacuum ultra violet region

${\stackrel{\lambda_{\rm vac}}{\mathring{A}}}$	Intensity	$\sigma \ (m cm^{-1})$	Classification ^a	$egin{array}{c} \lambda_{ m vac} \ \mathring{A} \end{array}$	Intensity	$\sigma \ (m cm^{-1})$	Classification ^a
9109 455	2	47540.9	22044 — 712059	2005 140	2	47958.2	
2103.455	3	47540.8	$23844_{9/2} - 71385\%_{/2}$	2085.148	2		
2102.907	20	47553.2		2084.954	10	47962.7	22522 515018
2102.492	3	47562.6		2084.699	3	47968.5	$23532_{5/2} - 71501^{\circ}_{3/2}$
2101.877	10	47576.5					$25409_{7/2} - 73378^{\circ}_{7/2}$
2101.778	100	47578.8	$23442_{11/2}$ $71021^{\circ}_{9/2}$	2084.344	60	47976.7	$14558_{9/2} - 62535^{\circ}_{9/2}$
2101.651	2	47581.6		2083.504	1	47996.1	$25033_{9/2} - 73029^{\circ}_{9/2}$
2099.948	5	47620.2	$25409_{7/2} - 73029^{\circ}_{9/2}$	2083.412	1	47998.2	$19872_{7/2} - 67870^{\circ}_{9/2}$
2099.757	50	47624.6		2083.123	400	48004.8	$13352_{11/2} - 61357^{\circ}_{9/2}$
2099.757	50	47624.6	$29267_{5/2} - 76892^{\circ}_{3/2}$	2082.879	2	48010.5	11/2
2099.402	200	47632.6	$16135_{7/2} - 63768^{\circ}_{7/2}$	2082.810	3	48012.1	$21418_{5/2} - 69431^{\circ}_{7/2}$
2098.974	3	47642.3		2082.653	3	48015.7	
2098.903	20	47643.9	$20848_{5/2} - 68492^{\circ}_{7/2}$	2081.788	$\frac{3}{2}$		27604 75640°
						48035.6	$27604_{9/2} - 75640^{\circ}_{11/2}$
2098.523	100	47652.6	$21755_{11/2} - 69408^{\circ}_{11/2}$	2080.866	1	48056.9	21611 606018
2098.275	5	47658.2	$26446_{7/2} - 74105^{\circ}_{5/2}$	2080.280	30	48070.4	$21611_{5/2} - 69681^{\circ}_{5/2}$
2097.806	100	47668.8	$17627_{9/2} - 65295^{\circ}_{7/2}$	2079.497	100	48088.6	$23647_{13/2} - 71736^{\circ}_{11/2}$
2097.601	1000	47673.5	$12846_{9/2} - 60520^{\circ}_{7/2}$	2079.441	300	48089.8	19308 _{11/2} — 67398° _{9/2}
2097.513	500	47675.5	$14859_{11/2}$ $-62535^{\circ}_{9/2}$	2079.020	1	48099.6	$16135_{7/2} - 64235_{9/2}^{\circ}$
2097.284	20	47680.7	$18241_{11/2}$ $- 65922^{\circ}_{11/2}$	2078.645	20	48108.3	$27452_{5/2} - 75560^{\circ}_{5/2}$
2097.234	100	47681.8	$14558_{9/2} - 62240^{\circ}_{11/2}$	2078.489	20	48111.9	$31254_{7/2} - 79366^{\circ}_{5/2}$
2097.160	40	47683.5	$21294_{7/2} - 68978^{\circ}_{5/2}$	2078.426	3	48113.3	1,2
2097.075	5	47685.5	$24309_{3/2} - 71994^{\circ}_{5/2}$	2077.544	60	48133.8	$23844_{9/2} - 71978^{\circ}_{7/2}$
2096.985	5	47687.5	21003 3/2 11331 3/2	2077.450	40	48135.9	$21294_{7/2} - 69431^{\circ}_{7/2}$
2096.890	5	47689.7	$27604_{9/2} - 75294^{\circ}_{7/2}$	2077.337	3	48138.6	
2096.832	200	47691.0	$18990_{7/2} - 66681^{\circ}_{5/2}$				$20848_{5/2} - 68987^{\circ}_{7/2}$
2096.787	6	47692.0	$\begin{array}{c} 18990_{7/2} - 60001_{5/2} \\ 21294_{7/2} - 68987_{7/2}^{\circ} \end{array}$	2076.841 2076.505	$\begin{bmatrix} 200 \\ 3 \end{bmatrix}$	48150.0 48157.8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2000.101		1.002.0	21271 1/2 00301 1/2	2010.303	5	40137.0	21004 9/2 - 13102 9/2
2096.496	400	47698.6	$14859_{11/2} - 62558^{\circ}_{11/2}$	2076.358	100	48161.2	$45805_{9/2} - 93967^{\circ}_{7/2}$
2094.953	20	47733.8	$23651_{7/2} - 71385^{\circ}_{7/2}$	2075.991	300	48169.8	$19700_{11/2} - 67870^{\circ}_{9/2}$
2094.676	400	47740.1	$19308_{11/2} - 67049^{\circ}_{9/2}$	2075.747	500	48175.4	$15045_{5/2} - 63221_{3/2}^{\circ}$
2094.155	4000	47752.0	$17113_{13/2} - 64865^{\circ}_{11/2}$	2074.851	5	48196.2	3/2
2093.909	5	47757.6		2073.739	20	48222.1	21755 _{11/2} — 69978° _{11/2}
2093.424	40	47768.6		2073.462	200	48228.5	$20315_{9/2} - 68544^{\circ}_{9/2}$
2092.509	10	47789.5		2073.215	3	48234.3	20313 9/2 00344 9/2
2091.826	30	47805.1	$20160_{3/2} - 67965^{\circ}_{3/2}$	2073.213	10		94799 72020°
2091.758	20	47806.7	$19872_{7/2} - 67679^{\circ}_{7/2}$			48241.9	$24788_{9/2} - 73029^{\circ}_{9/2}$
2091.411	4000	47814.6	$18921_{15/2} - 66735^{\circ}_{13/2}$	2072.580 2072.534	15 400	48249.0 48250.1	$18990_{7/2} - 67240^{\circ}_{7/2}$
2091.238	100	47818.6	$14859_{11/2} - 62678^{\circ}_{13/2}$	2071.991	80	48262.8	$21418_{5/2} - 69681^{\circ}_{5/2}$
2090.153	20	47843.4	$21294_{7/2} - 69138^{\circ}_{9/2}$	2071.533	5	48273.4	$22747_{9/2} - 71021^{\circ}_{9/2}$
2089.744	1	47852.7	$23532_{5/2} - 71385^{\circ}_{7/2}$	2070.768	50	48291.3	$15525_{11/2}$ — $63816^{\circ}_{11/2}$
2089.473	10	47859.0	$18063_{9/2} - 65922^{\circ}_{11/2}$	2070.649	200	48294.0	$23442_{11/2}$ $- 71736^{\circ}_{11/2}$
2089.306	5	47862.8	$18990_{7/2} - 66852^{\circ}_{7/2}$	2070.338	50	48301.3	$16516_{7/2} - 64817^{\circ}_{5/2}$
2088.848	2	47873.3	$21535_{9/2} - 69408^{\circ}_{11/2}$	2070.042	400	48308.2	$17627_{9/2} - 65935^{\circ}_{7/2}$
2088.769	10	47875.1	$32288_{3/2} - 80164^{\circ}_{3/2}$	2069.258	50	48326.5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2088.632	10	47878.2	3/2 00104 3/2	2068.559			
2088.346	400	47884.8	$16516_{7/2} - 64401^{\circ}_{5/2}$	The second secon	30	48342.8	$23651_{7/2} - 71994^{\circ}_{5/2}$
2088.042	5	47891.8	$\begin{array}{c} 10310_{7/2} - 04401_{5/2} \\ 23844_{9/2} - 71736_{11/2}^{\circ} \end{array}$	2068.261 2067.712	200 200	48349.8 48362.6	$39870_{9/2} - 88220^{\circ}_{9/2} 15454_{13/2} - 63816^{\circ}_{11/2}$
2007 207	4			2067.004			11/2
2087.387	4	47906.8	$18241_{11/2}$ — $66148^{\circ}_{13/2}$	2067.034	200	48378.5	
2087.300	4	47908.8		2066.270	10	48396.4	
2087.200	4	47911.1		2065.895	300	48405.2	$18990_{7/2} - 67395^{\circ}_{5/2}$
2086.712	10	47922.3	$20315_{9/2} - 68238^{\circ}_{11/2}$	2065.177	5	48422.0	$27138_{7/2} - 75560^{\circ}_{5/2}$
2085.246	30	47956.0	$28936_{3/2} - 76892^{\circ}_{3/2}$	2064.736	1000	48432.3	$17534_{15/2} - 65967^{\circ}_{13/2}$

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

${\stackrel{\lambda_{ m vac}}{{ m A}}}$	Intensity	σ (cm^{-1})	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{\mathring{A}}$	Intensity	σ (cm ⁻¹)	Classification ^a
2064 201		40.440.0	21505	2040 425	10	40010.0	
2064.291	2	48442.8	$21535_{9/2} - 69978^{\circ}_{11/2}$	2048.425	10	48818.0	$20160_{3/2} - 68978^{\circ}_{5/2}$
2064.176	10	48445.5	$23532_{5/2} - 71978^{\circ}_{7/2}$	2048.148	100	48824.6	$19700_{11/2} - 68525^{\circ}_{11/2}$
2063.966	5	48450.4	$23050_{3/2} - 71501^{\circ}_{3/2}$	2047.788	20	48833.2	$20848_{5/2} - 69681^{\circ}_{5/2}$
2063.765	2	48455.1		2047.369	80	48843.2	$19700_{11/2}$ $- 68544^{\circ}_{9/2}$
2063.592	1	48459.2	$19872_{7/2} - 68331^{\circ}_{7/2}$	2047.331	1	48844.1	
2063.478	3	48461.9	$23532_{5/2} - 71994^{\circ}_{5/2}$	2047.208	2	48847.0	$26446_{7/2} - 75294^{\circ}_{7/2}$
2063.161	4	48469.3	$18211_{5/2} - 66681^{\circ}_{5/2}$	2046.923	70	48853.8	$17113_{13/2} - 65967^{\circ}_{13/2}$
2062.870	200	48476.2	$27138_{7/2} - 75614^{\circ}_{5/2}$	2046.754	10	48857.8	$22527_{7/2} - 71385^{\circ}_{7/2}$
2062.457	200	48485.9	$20315_{9/2} - 68801^{\circ}_{7/2}$	2046.692	20	48859.3	$29835_{9/2} - 78694^{\circ}_{11/2}$
			$23050_{3/2} - 71536^{\circ}_{5/2}$	2046.390	10	48866.5	
2061.421	80	48510.2	$12846_{\ 9/2} -\ 61357^{\circ}_{\ 9/2}$	2045.914	10	48877.9	19360 _{13/2} — 68238° _{11/2}
2060.746	20	48526.1		2045.564	2	48886.3	
2060.636	10	48528.7	$25934_{5/2} - 74463^{\circ}_{3/2}$	2045.465	200	48888.6	$13352_{11/2}$ $- 62240^{\circ}_{11/2}$
2060.569	30	48530.3	$15045_{5/2} - 63576_{5/2}^{\circ}$	2044.686	10	48907.3	$24470_{7/2} - 73378^{\circ}_{7/2}$
2060.054	1	48542.4	5/2	2044.070	1	48922.0	
2059.891	10	48546.2		2043.773	500	48929.1	$19872_{7/2} - 68801^{\circ}_{7/2}$
2059.245	4000	48561.5	$19308_{11/2} - 67870^{\circ}_{9/2}$	2043.103	50	48945.2	$19360_{13/2} - 68305^{\circ}_{15/2}$
2058.796	60	48572.1	, 5/2	2042.616	400	48956.8	$14859_{11/2} - 63816^{\circ}_{11/2}$
2058.663	30	48575.2	$25033_{9/2} - 73609^{\circ}_{11/2}$	2041.925	2	48973.4	11/2
2058.371	10	48582.1	$35828_{9/2} - 84410^{\circ}_{9/2}$	2039.381	200	49034.5	$14558_{\ 9/2} - 63593^{\circ}_{\ 9/2}$
2058.090	5	48588.7		2038.682	1	49051.3	
2057.554	100	48601.4	$35828_{9/2} - 84430^{\circ}_{7/2}$	2038.366	î	49058.9	
2057.042	10	48613.5	$17534_{15/2} - 66148^{\circ}_{13/2}$	2037.578	3	49077.9	
2056.771	5	48619.9	$19872_{7/2} - 68492^{\circ}_{7/2}$	2036.415	20 c l	49105.9	$19872_{7/2} - 68978^{\circ}_{5/2}$
2056.545	30	48625.2	$15525_{11/2} - 64150^{\circ}_{11/2}$	2036.103	1	49113.4	1/2
2056.409	30	48628.4	$29835_{9/2}-78463^{\circ}_{7/2}$	2036.061	100	49114.4	$19872_{7/2} - 68987^{\circ}_{7/2}$
2056.326	100	48630.4	$30505_{11/2}$ $79136^{\circ}_{13/2}$	2035.210	10	49135.0	120.2 1/2 00201 1/2
2054.597	50	48671.4	$20315_{9/2} - 68987^{\circ}_{7/2}$	2034.894	100	49142.6	$21238_{13/2} - 70381^{\circ}_{13/2}$
2054.509	1000	48673.4	$14558_{9/2} - 63232^{\circ}_{7/2}$	2034.290	1	49157.2	$18241_{11/2} - 67398^{\circ}_{9/2}$
2054.168	200	48681.5	$16135_{7/2} - 64817^{\circ}_{5/2}$	2034.186	7	49159.7	$16135_{7/2} - 65295^{\circ}_{7/2}$
2053.815	10	48689.9	15525 _{11/2} — 64215° _{13/2}	2033.950	2000	49165.4	19360 _{13/2} — 68525° _{11/2}
2053.531	1000	48696.6	$15454_{13/2} - 64150^{\circ}_{11/2}$	2033.719	10	49171.0	17000 13/2 00020 11/2
2052.953	2000	48710.3	$13454_{13/2}$ $64150_{11/2}$ $13352_{11/2}$ $62062^{\circ}_{9/2}$	2033.478	40	49176.8	$18063_{9/2} - 67240^{\circ}_{7/2}$
2002.700	2000	40110.5	$15525_{11/2} - 64235^{\circ}_{9/2}$	2033.207	200	49183.4	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
2052.434	2	48722.6	$15045_{5/2} - 63768^{\circ}_{7/2}$	2033.201	200	47100.4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2052.198	3	48728.2		2033.129	50	49185.3	$23844_{9/2} - 73029^{\circ}_{9/2}$
2052.131	3	48729.8		2033.015	100	49188.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2052.131	10	48731.1	$18211_{5/2} - 66943^{\circ}_{5/2}$	2032.480	200	49201.0	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
2052.078	10	48731.9	10211 5/2 - 00940 5/2	2032.253	400	49206.5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2051.988	100	48733.2	$14859_{11/2} - 63593^{\circ}_{9/2}$	2032.233	1000	49209.8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2031.900	100	40133.2	14009 11/2 - 00090 9/2	2002.117	1000	47407.0	14000 9/2 - 00 (00 7/2
2051.736	200	48739.2	$21238_{\ 13/2} -\ 69978^{\circ}_{\ 11/2}$	2031.865	400	49215.9	$12846_{9/2} - 62062^{\circ}_{9/2}$
2050.969	20	48757.4	19046 (1605°	2031.558	1	49223.3	$22277_{3/2} - 71501^{\circ}_{3/2}$
2050.911	10	48758.8	$12846_{9/2} - 61605^{\circ}_{7/2}$	2031.455	400	49225.8	$17627_{9/2} - 66852^{\circ}_{7/2}$
2050.812 2050.587	400 200	48761.2 48766.5	$15454_{13/2}$ — $64215^{\circ}_{13/2}$ $17534_{15/2}$ — $66301^{\circ}_{15/2}$	2031.256 2030.131	10 100	49230.6 49257.9	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
						40961.5	
2050.036	20	48779.6	$16516_{7/2} - 65295^{\circ}_{7/2}$	2029.983	$\frac{2}{7}$	49261.5	10079 (0120°
2049.624	20	48789.4	$18063_{9/2} - 66852^{\circ}_{7/2}$	2029.814	7	49265.6	$19872_{7/2} - 69138^{\circ}_{9/2}$
2048.865	400	48807.5	$18241_{11/2} - 67049^{\circ}_{9/2}$	2029.694	2	49268.5	25127 04400°
2048.798 2048.630	100	48809.1	$17113_{13/2}$ — $65922^{\circ}_{11/2}$	2029.540	20	49272.2	$35137_{3/2} - 84409^{\circ}_{3/2}$
2048 630	1	48813.1		2029.192	300	49280.7	

^a For doubly-classified lines, the wavelength is entered only once.

TABLE X. Observed spectral lines of Pr III in the vacuum ultra violet region-Continued

$\overset{\boldsymbol{\lambda_{\mathrm{vac}}}}{\mathbf{A}}$	Intensity	$\sigma \atop (cm^{-1})$	Classification ^a	$egin{array}{c} \lambda_{ m yac} \ A \end{array}$	Intensity	σ (cm ⁻¹)	Classification ^a
2022 050	2	49286.4			1 2		$17627_{9/2} - 67398^{\circ}_{9/2}$
2028.959	2		44670 02067°	2000 107	40	49773.4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2028.926	5	49287.2	$44679_{7/2} - 93967^{\circ}_{7/2}$	2009.107	40		
2028.780	100	49290.7	$14859_{11/2} - 64150^{\circ}_{11/2}$	2008.066	10	49799.2	$16135_{7/2} - 65935^{\circ}_{7/2}$
2028.209	40	49304.6	$22080_{7/2} - 71385^{\circ}_{7/2}$	2007.738	20	49807.3	$18063_{9/2} - 67870^{\circ}_{9/2}$
2027.315	3	49326.3	$13352_{11/2} - 62678^{\circ}_{13/2}$	2006.763	1 1	49831.5	
2027.194	40	49329.3		2006.565	30	49836.4	21755 _{11/2} — 71592° _{9/2}
2027.102	300	49331.5	$15525_{11/2}$ — $64857^{\circ}_{9/2}$	2006.072	10	49848.7	
2026.948	10	49335.3	$18063_{9/2} - 67398^{\circ}_{9/2}$	2005.817	30	49855.0	$30505_{11/2}$ — $80360^{\circ}_{11/2}$
2026.694	10	49341.4	$18990_{7/2} - 68331^{\circ}_{7/2}$	2004.416	10	49889.8	$21611_{5/2} - 71501_{3/2}^{\circ}$
2026.007	30 c l	49358.2		2003.908	20	49902.5	
2025.296	30	49375.5	$14859_{11/2} - 64235^{\circ}_{9/2}$	2003.001	10	49925.1	$21611_{5/2} - 71536^{\circ}_{5/2}$
2024.954	100	49383.8	$18921_{15/2} - 68305^{\circ}_{15/2}$	2002.296	2	49942.7	3/2
2024.812	2	49387.3	10521 15/2 00505 15/2	2001.839	1	49954.1	
			$16516_{7/2} - 65909^{\circ}_{5/2}$	2001.548	10	49961.3	$23647_{13/2} - 73609^{\circ}_{11/2}$
2024.573 2024.540	20 c l 400	49393.1 49393.9	$10310_{7/2} - 03909_{5/2} $ $12846_{9/2} - 62240^{\circ}_{11/2}$	2001.348	40	49964.0	23047 13/2 73009 11/5
2024.340	100	47070.7	12010 9/2 02210 11/2	2001.111	10	12201.0	
2024.298	70	49399.8		2001.049	5	49973.8	$28720_{9/2} - 78694^{\circ}_{11/2}$
2023.848	10	49410.8	$15454_{13/2} - 64865^{\circ}_{11/2}$	2000.784	2	49980.4	$21755_{11/2}$ $- 71736^{\circ}_{11/2}$
2023.390	10	49422.0	$17627_{9/2} - 67049^{\circ}_{9/2}$	2000.587	200	49985.3	$19700_{11/2}$ — $69686^{\circ}_{9/2}$
2023.005	200	49431.4	$29263_{13/2} - 78694^{\circ}_{11/2}$	2000.462	20	49988.4	$18990_{7/2} - 68978^{\circ}_{5/2}$
2022.766	70	49437.3	$19700_{11/2} - 69138^{\circ}_{9/2}$	2000.116	400	49997.1	$14859_{11/2} - 64857^{\circ}_{9/2}$
2022.100	'	19101.0	15.00 11/2 05100 9/2		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		11/2
2022.370	3	49446.9					$18990_{7/2} - 68987^{\circ}_{7/2}$
2022.027	1	49455.3	$22080_{7/2} - 71536^{\circ}_{5/2}$	1999.902	30	50002.4	$24461_{5/2} - 74463^{\circ}_{3/2}$
2021.544	50	49467.1	$22527_{7/2} - 71994^{\circ}_{5/2}$	1999.795	100	50005.1	$14859_{11/2} - 64865^{\circ}_{11/2}$
2021.249	1	49474.4	1,2	1998.905	30	50027.4	
2020.778	10	49485.9	$21535_{~9/2}-~71021^{\circ}_{~9/2}$	1998.598	10	50035.1	
2018.512	1	49541.4		1998.301	1	50042.5	
2018.385	10	49544.6	$26095_{11/2} - 75640^{\circ}_{11/2}$	1998.064	400	50048.4	19360 _{13/2} — 69408° _{11/3}
2017.745	30		$29835_{9/2} - 79395^{\circ}_{7/2}$	1997.912	20	50052.2	$17627_{9/2} - 67679^{\circ}_{7/2}$
		49560.3	$29033 \frac{9}{2} - 79393 \frac{7}{2}$	1996.715	30	50082.3	$21418_{5/2} - 71501^{\circ}_{3/2}$
2016.711	100	49585.7	$23442_{11/2} - 73029^{\circ}_{9/2}$	1996.423	3	50082.5	21410 5/2 11301 3/2
2016.637	2	49587.5	23442 11/2 73029 9/2	1770.425		30007.0	
2016.463	1 ,	49591.8	$14558_{\ 9/2}-\ 64150^{\circ}_{\ 11/2}$	1996.023	5 c l	50099.6	19308 _{11/2} — 69408° _{11/2}
2015.591	100	49613.2	$17627_{9/2} - 67240^{\circ}_{7/2}$	1995.989	10	50100.5	
2015.488	200	49615.8	$18063_{9/2} - 67679^{\circ}_{7/2}$	1995.216	100	50119.9	$18211_{5/2} - 68331^{\circ}_{7/2}$
2015.267	20	49621.2	$29267_{5/2} - 78889^{\circ}_{3/2}$	1994.856	1	50128.9	
2015.214	100	49622.5	$17113_{13/2} - 66735^{\circ}_{13/2}$	1994.692	400	50133.0	$18241_{11/2}$ — $68374^{\circ}_{9/2}$
2014.946	100	49629.1	$18241_{\ 11/2} - 67870^{\circ}_{\ 9/2}$	1994.027	20	50149.8	$31254_{7/2} - 81404^{\circ}_{5/2}$
2014.405	2	49642.4		1993.422	300 c l	50165.0	$16516_{7/2} - 66681_{5/2}^{\circ}$
2013.897	5	49655.0		1993.346	100 c l	50166.9	$23442_{11/2}$ $73609^{\circ}_{11/2}$
2013.015		49676.7	14559 — 64925°	1991.983	10	50201.2	$21535_{9/2} - 71736^{\circ}_{11/2}$
2013.013	100	49679.7	$14558_{9/2} - 64235^{\circ}_{9/2} 25934_{5/2} - 75614^{\circ}_{5/2}$	1991.836	6	50204.9	$25409_{7/2} - 75614^{\circ}_{5/2}$
2012.070	50	15015.1	2000 + 5/2 1001 + 5/2	1551.000		50201.5	20103 1/2 10011 3/2
2011.593	100	49711.8	$12846_{9/2} - 62558^{\circ}_{11/2}$	1991.622	60	50210.3	
2011.388	3	49716.9	$22277_{3/2} - 71994^{\circ}_{5/2}$	1991.509	30	50213.2	$24250_{3/2} - 74463^{\circ}_{3/2}$
2011.008	1	49726.3	$21294_{7/2} - 71021^{\circ}_{9/2}$	1991.049	1	50224.8	
			$23651_{7/2} - 73378^{\circ}_{7/2}$	1990.959	3	50227.0	2.000
2010.696	20	49734.0		1989.646	50	50260.2	$25033_{9/2} - 75294^{\circ}_{7/2}$
2010.339	80	49742.8	$28720_{\ 9/2} -\ 78463^{\circ}_{\ 7/2}$	1989.319	300	50268.5	$18063_{9/2} - 68331^{\circ}_{7/2}$
2009.905	80	49753.6	$18211_{5/2} - 67965^{\circ}_{3/2}$	1988.770	6	50282.3	$22747_{9/2} - 73029_{9/2}^{\circ}$
2009.579	40	49761.7	3/2	1988.707	2	50283.9	$18241_{11/2} - 68525_{11/2}^{\circ}$
2009.379	5	49764.4	$23844_{9/2} - 73609^{\circ}_{11/2}$	1988.247	10	50295.6	102 11 11/2 00020 11/
2007.401	40	49771.6	$\frac{25044}{5/2} = \frac{75009}{11/2}$ $15045_{5/2} = 64817^{\circ}_{5/2}$	1988.139	300	50298.3	$14558_{9/2} - 64857^{\circ}_{9/2}$

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

1987.542 2 1985.995 5 1985.995 5 1985.023 1 1984.870 10 1984.698 20 1984.380 4 1984.348 2 1984.348 2 1983.311 10 1982.981 300 1982.785 2 1982.492 5 1982.492 5 1982.428 1 1981.580 100 1981.449 2 1981.449 2 1981.449 2 1980.287 200 1980.287 200 1979.692 20 1978.427 200 1975.820 2 1975.82 4 1975.582 200 1975.424 3 1973.367 10 1972.857 10 1972.857 10 1972.200 30 1971.913	Intensity	nsity σ (cm^{-1})	Classification ^a	$\overset{\boldsymbol{\lambda_{\mathrm{yac}}}}{\mathbf{A}}$	Intensity	$\sigma \atop (cm^{-1})$	Classification ^a
1987.542 2 1985.995 5 1985.995 5 1985.023 1 1984.698 20 1984.380 4 1984.381 1984.250 1983.311 10 1982.981 300 1982.785 2 1982.428 1 1981.580 100 1981.449 2 1981.449 2 1981.449 2 1980.287 200 1980.287 200 1979.692 20 1978.427 200 1975.850 2 1975.82 4 1975.82 2 1975.424 3 1973.367 10 1972.857 10 1972.200 30 1971.913 2 1971.287 4 1971.288 4 1971.287 4							
1985.995 5 1985.023 1 1984.870 10 1984.698 20 1984.380 4 1984.381 1984.250 1983.311 10 1982.981 300 1982.785 2 1982.428 1 1981.580 100 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1980.287 200 1979.692 20 1978.427 200 1975.850 2 1975.882 200 1975.882 200 1975.424 3 1973.367 10 1972.857 10 1972.200 1971.913 1971.63	40	50311.2	$18063_{9/2} - 68374_{9/2}^{\circ}$	1967.373	1	50829.2	
1985.995 5 1985.023 1 1984.870 10 1984.698 20 1984.380 4 1984.381 1984.250 1983.311 10 1982.981 300 1982.785 2 1982.428 1 1981.580 100 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1980.287 200 1979.745 5 1979.692 20 1978.427 200 1975.782 4 1975.880 2 1975.882 200 1975.424 3 1973.367 10 1972.857 10 1972.200 30 1971.913	2	50313.4		1967.233	1	50832.8	$24461_{5/2} - 75294^{\circ}_{7/2}$
1985.023	5		$21148_{3/2} - 71501^{\circ}_{3/2}$	1966.710	2	50846.3	$21148_{3/2} - 71994^{\circ}_{5/2}$
1984.870 1984.698 1984.380 1984.380 1984.348 1984.250 1983.311 1983.066 1982.981 1982.428 1982.428 1981.580 1981.449 1981.140 1980.950 1080.867 1980.287 1980.191 1979.745 1979.692 1978.427 1975.850 1975.782 1975.782 1975.582 1975.582 1975.424 1973.849 1973.849 1973.849 1973.849 1973.849 1973.857 1072.617 1972.200 1971.913 1971.730 1971.636 1971.248 1971.248 1970.573 1970.091			$25409_{7/2} - 75762_{9/2}^{\circ}$	1966.502	3	50851.7	$24788_{9/2} - 75640^{\circ}_{11/2}$
1984.698 20 1984.380 4 1984.381 4 1984.348 2 1983.311 10 1983.066 2 1982.785 2 1982.785 2 1982.492 5 1982.492 5 1982.492 100 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1980.287 200 1980.287 200 1979.745 3 1979.692 200 1978.427 200 1975.820 2 1975.82 4 1973.849 3 1973.367 10 1972.857 10 1972.857 10 1971.913 2 1971.730 15 1971.287 <t< td=""><td>1</td><td>50377.2</td><td>$19308_{11/2} - 69686^{\circ}_{9/2}$</td><td>1966.208</td><td>40</td><td>50859.3</td><td>$27604_{9/2} - 78463^{\circ}_{7/2}$</td></t<>	1	50377.2	$19308_{11/2} - 69686^{\circ}_{9/2}$	1966.208	40	50859.3	$27604_{9/2} - 78463^{\circ}_{7/2}$
1984.698 20 1984.380 4 1984.381 2 1984.348 2 1984.250 50 1983.311 10 1982.981 300 1982.885 2 1982.492 5 1982.492 5 1982.492 100 1981.580 100 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1980.867 2 1980.287 200 1979.745 3 1979.692 20 1978.427 20 1975.850 2 1975.782 4 1975.882 20 1975.894 3 1973.367 10 1972.857 10 1972.857 10 1971.913 2 1971.730 15 1971.287	10	50381.1					$36652_{5/2} - 87511^{\circ}_{7/2}$
1984.380 4 1984.348 2 1984.250 50 1983.311 10 1983.066 2 1982.981 300 1982.785 2 1982.492 5 1982.492 1 1982.492 1 1982.492 1 1982.492 1 1982.492 1 1981.580 100 1981.449 2 1981.449 2 1981.449 2 1981.449 2 1980.867 2 1980.287 200 1979.745 3 1979.692 200 1978.427 200 1975.782 4 1975.882 200 1975.882 200 1973.367 10 1972.857 10 1972.857 10 1972.200 30 1971.913 19 1971.287			$12846_{9/2} - 63232^{\circ}_{7/2}$	1065 070	00	50065 5	
1984.348 2 1984.250 50 1983.311 10 1983.066 2 1982.981 300 1982.785 2 1982.492 5 1982.492 1 1982.492 1 1982.492 1 1982.492 1 1982.492 1 1982.492 1 1981.580 100 1981.449 2 1981.449 2 1981.449 2 1980.287 200 1980.287 200 1979.692 20 1978.427 200 1975.850 2 1975.82 4 1975.82 2 1975.424 3 1973.367 10 1972.857 10 1972.200 30 1971.730 15 1971.287 4 1971.284 4 1970.573 10 1970.091 1			$12040_{9/2} - 03232_{7/2}$	1965.970	80	50865.5	$17627_{9/2} - 68492^{\circ}_{7/2}$
1984.250 50 1983.311 10 1983.066 2 1982.981 300 1982.785 1982.492 55 1982.428 1981.580 100 1981.449 2 1981.140 4 1980.950 10 1980.867 200 1980.87 100 1980.87 200 1978.427 1979.692 20 1978.427 1975.850 1975.782 4 1975.582 1975.424 3 1973.849 3 1973.849 3 1973.849 3 1973.367 10 1972.857 10 1972.857 10 1972.617 5 1972.617 5 1972.617 5 1971.636 1971.730 15 1971.636 1971.287 44 1971.248 44 1970.573 80				1965.346	1	50881.6	15605
1983.311 10 1983.066 2 1982.981 300 1982.785 2 1982.492 5 1982.492 10 1981.580 100 1981.449 2 1981.140 4 1980.950 10 1980.867 2 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.782 4 1975.582 200 1975.782 4 1975.582 200 1975.424 3 1973.849 3 1973.849 3 1973.849 3 1973.590 2 1978.427 10 1979.67 10 1979.	2 c l		15505	1963.974	2	50917.2	$17627_{9/2} - 68544^{\circ}_{9/2}$
1983.066 2 1982.981 300 1982.785 2 1982.492 5 1982.428 1 1981.580 100 1981.449 2 1981.449 2 1981.440 4 1980.950 10 1980.867 20 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.782 4 1975.582 20 1975.424 3 1973.367 10 1972.857 10 1972.857 10 1972.200 30 1971.913 2 1971.636 200 1971.287 4 4971.248 4 1970.091 1	50	50396.9	$15525_{11/2} - 65922^{\circ}_{11/2}$	1963.911	2	50918.8	
1982,981 300 1982,785 2 1982,492 5 1982,428 1 1981,580 100 1981,449 2 1981,449 4 1981,449 2 1980,867 2 1980,287 100 1979,745 5 1979,745 5 1975,850 2 1975,82 4 1975,82 2 1975,82 2 1975,82 2 1975,82 10 1973,849 3 1973,849 2 1973,849 3 1972,857 10 1972,857 10 1972,857 10 1971,913 2 1971,130 15 1971,287 4 4971,248 4 1970,091 1	10	50420.7	$14558_{9/2} - 64979^{\circ}_{7/2}$	1963.786	100 c l	50922.0	$12846_{9/2} - 63768^{\circ}_{7/2}$
1982.785 2 1982.428 1 1981.580 100 1981.449 2 1981.449 1 1981.449 2 1981.449 2 1981.449 2 1980.950 10 1980.867 2 1980.287 200 1979.745 5 1979.692 20 1978.427 200 1975.850 2 1975.782 4 1975.882 200 1975.782 4 1973.849 3 1973.849 3 1973.367 10 1972.857 10 1972.2617 5 1972.2617 5 1971.913 2 1971.287 4 1971.248 4 1970.573 80 1970.091 1	2	50427.0	$16516_{7/2} - 66943^{\circ}_{5/2}$	1963.731	20 c l	50923.5	$18063_{9/2} - 68987^{\circ}_{7/2}$
1982.785 2 1982.428 1 1981.580 100 1981.449 2 1981.449 2 1981.440 4 1980.950 10 1980.867 2 1980.287 200 1980.191 100 1979.745 5 1975.850 2 1975.782 4 1975.782 4 1975.782 4 1975.850 2 1975.851 200 1975.424 3 1973.849 3 1973.367 10 1972.857 10 1972.200 30 1971.913 2 1971.636 200 1971.287 4 4971.248 4 1970.091 1	300	50429.1	$18063_{9/2} - 68492^{\circ}_{7/2}$	1963.401	100	50932.0	3,2
1982.492 5 1982.428 1 1981.580 100 1981.449 2 1981.140 4 1980.950 10 1980.867 2 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.782 4 1975.782 4 1975.782 4 1975.424 3 1973.367 10 1972.857 10 1972.857 10 1972.200 30 1971.913 2 1971.730 15 1971.287 4 4971.248 4 1970.091 1	2		$23175_{13/2} - 73609^{\circ}_{11/2}$	1962.747	4	50949.0	$22080_{7/2} - 73029^{\circ}_{9/2}$
1981.580 100 1981.449 2 1981.140 4 1980.950 10 1980.867 20 1980.287 200 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.782 4 1975.582 200 1975.424 3 1973.367 10 1972.857 10 1972.200 30 1971.913 2 1971.730 15 1971.287 4 4971.248 4 1970.091 1	5		$15525_{11/2} - 65967^{\circ}_{13/2}$	1962.418	10	50957.5	$25934_{5/2} - 76892^{\circ}_{3/2}$
1981.580 100 1981.449 2 1981.140 4 1980.950 10 1980.867 2 1980.287 200 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.782 4 1975.582 200 1975.424 3 1973.367 10 1972.857 10 1972.857 10 1972.200 30 1971.913 2 1971.730 15 1971.287 4 4971.248 4 1970.091 1	1	50443.2	$21535_{9/2} - 71978^{\circ}_{7/2}$	1961.929	200	50970.2	19946 62916°
1981.449 2 1981.140 4 1980.950 10 1980.867 2 1980.287 200 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.782 4 1975.582 20 1975.424 3 1973.849 3 1973.867 10 1972.857 10 1972.617 5 1971.913 2 1971.636 200 1971.287 4 1971.248 4 1970.091 1							$12846_{9/2} - 63816^{\circ}_{11}$
1981.140 4 1980.867 2 1980.287 200 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.850 2 1975.782 4 1975.582 20 1975.424 3 1973.849 3 1973.367 10 1972.857 10 1972.617 5 1971.913 2 1971.730 15 1971.287 4 1971.248 4 1970.091 1			$13352_{11/2} - 63816^{\circ}_{11/2}$	1961.265	3	50987.5	
1980.950 10 1980.867 2 1980.287 200 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.850 2 1975.782 4 1975.582 20 1975.424 3 1973.849 3 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.636 200 1971.287 4 1971.248 4 1970.091 1			$15454_{13/2}$ — $65922^{\circ}_{11/2}$	1960.735	10	51001.3	10050
1980.867 1980.287 1980.287 1980.191 1979.745 1979.692 20 1978.427 1975.850 1975.782 1975.582 1975.424 1973.849 1973.590 1973.367 1972.857 1972.617 1972.200 1971.913 1971.730 1971.636 1971.287 1971.248 1971.248 1971.248 1971.248 1971.248 1970.091	4			1959.961	30	51021.4	$19360_{13/2}$ $- 70381^{\circ}_{13/2}$
1980.287 200 1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.850 2 1975.782 4 1975.582 200 1975.424 3 1973.849 3 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.636 200 1971.287 4 1971.248 4 1970.573 80 1970.091 1	10	50480.8	$18063_{9/2} - 68544^{\circ}_{9/2}$	1959.874	10bl	51023.7	$45807_{5/2} - 96830^{\circ}_{7/2}$
1980.191 100 1979.745 5 1979.692 20 1978.427 200 1975.850 2 1975.782 4 1975.582 200 1975.424 3 1973.849 3 1973.367 10 1972.857 10 1972.200 30 1971.913 2 1971.730 15 1971.287 4 1971.287 4 1971.248 4 1970.091 1	2	50483.0	$30505_{11/2} - 80988^{\circ}_{13/2}$	1958.687	2	51054.6	$23050_{3/2} - 74105^{\circ}_{5/3}$
1979.745 5 1979.692 20 1978.427 20 1975.850 2 1975.782 4 1975.582 20 1975.424 3 1973.849 3 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.730 15 1971.287 4 1971.248 4 1970.573 80 1970.091 1	200	50497.7		1958.387	100	51062.4	14859 _{11/2} — 65922° ₁₁
1979.745 5 1979.692 20 1978.427 200 1975.850 2 1975.782 4 1975.582 200 1975.424 3 1973.849 3 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.730 15 1971.287 4 1971.248 4 1970.573 80 1970.091 1	100 h	0 <i>h</i> 50500.2	$38448_{~9/2} - 88948_{~9/2}^{\circ}$	1958.053	2	51071.1	11/2
1979.692 20 1978.427 200 1975.850 2 1975.782 4 1975.582 200 1975.424 3 1973.849 3 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.730 15 1971.287 4 1971.248 4 1970.573 80 1970.091 1	5 b l			1958.001	1	51072.5	19308 _{11/2} - 70381° ₁₃
1975.850 1975.782 1975.782 1975.582 1975.424 200 1973.849 1973.367 1972.857 1972.617 1972.200 1971.913 1971.730 1971.636 1971.287 1971.248 1971.248 1970.573 1970.091	20		$15454_{13/2} - 65967^{\circ}_{13/2}$	1957.908	3	51074.9	$18063_{9/2} - 69138^{\circ}_{9/2}$
1975.850 1975.782 1975.782 1975.582 1975.424 200 1973.849 1973.367 1972.857 1972.617 1972.200 1971.913 1971.730 1971.636 1971.287 1971.248 1971.248 1970.573 1970.091	200	50545.2	$16135_{7/2} - 66681^{\circ}_{5/2}$	1957.338	1	51089.8	$24470_{7/2} - 75560^{\circ}_{5/3}$
1975.782 4 1975.582 200 1975.424 3 1973.849 3 1973.590 2 1973.367 10 1972.857 10 1972.201 30 1971.913 2 1971.730 15 1971.287 4 1971.248 4 1970.573 80 1970.091 1			$17627_{9/2} - 68238_{11/2}^{\circ}$	1957.073	6	51096.7	24410 7/2 15500 5/2
1975.582 200 1975.424 3 1973.849 3 1973.590 2 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.636 200 1971.287 4 1971.248 4 1970.573 80 1970.091 1			17027 9/2 00230 11/2				20262 20260°
1975.424 3 1973.849 3 1973.590 2 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.730 15 1971.636 200 1971.287 4 1971.248 4 1970.573 80 1970.091 1			10260 60079°	1957.039	3	51097.6	$29263_{13/2} - 80360^{\circ}_{11/2}$
1973.849 3 1973.590 2 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.730 15 1971.636 200 1971.287 4 1971.248 4 1970.573 80 1970.091 1			$19360_{13/2}$ — $69978^{\circ}_{11/2}$	1956.957	5	51099.7	$24461_{5/2} - 75560^{\circ}_{5/2}$
1973.590 2 1973.367 10 1972.857 10 1972.617 5 1972.200 30 1971.913 2 1971.730 15 1971.636 200 1971.287 4 1971.248 4 1970.573 80 1970.091 1	3	30022.0		1956.672	3	51107.2	14859 _{11/2} — 65967° _{13/2}
1973.367 1972.857 1972.617 1972.200 1971.913 1971.730 1971.636 1971.287 1971.248 1971.248 1970.573 1970.091	3			1955.992	15	51124.9	17113 _{13/2} — 68238° ₁₁
1972.857 1972.617 1972.200 1971.913 1971.730 1971.636 1971.287 1971.248 1970.573 1970.091	2	50669.1	$19308_{11/2} - 69978^{\circ}_{11/2}$	1955.521	3	51137.3	
1972.617 5 1972.200 30 1971.913 2 1971.730 15 1971.636 200 1971.287 4 1971.248 4 1970.573 80 1970.091 1	10	50674.8	$28720_{9/2} - 79395^{\circ}_{7/2}$	1955.268	3	51143.9	$24470_{7/2} - 75614^{\circ}_{5/2}$
1972.200 30 1971.913 2 1971.730 15 1971.636 200 1971.287 4 1971.248 4 1970.573 80 1970.091 1	10	50687.9	$20848_{5/2} - 71536^{\circ}_{5/2}$	1954.535	10	51163.1	$16516_{7/2} - 67679^{\circ}_{7/2}$
1971.913 1971.730 1971.636 1971.287 200 1971.287 4 1971.248 1970.573 1970.091	5	50694.1	$15454_{13/2} - 66148^{\circ}_{13/2}$	1954.455	60w	51165.2	
1971.913 1971.730 1971.636 1971.287 200 1971.287 4 1971.248 1970.573 1970.091	30	50704.8	$17627_{9/2} - 68331^{\circ}_{7/2}$	1954.386	20	51167.0	18241 69408°
1971.730 15 1971.636 200 1971.287 4 1971.248 4 1970.573 80 1970.091 1			11021 9/2 00001 7/2			51171.9	18241 _{11/2} — 69408° ₁₁
1971.636 1971.287 4 1971.248 1970.573 1970.091			16125 66059°	1954.196	40		17697 69901°
1971.287 4 1971.248 4 1970.573 80 1970.091 1		to the second se	$16135_{7/2} - 66852^{\circ}_{7/2}$	1954.092	2	51174.7	$17627_{9/2} - 68801^{\circ}_{7/2}$
1971.248 4 1970.573 80 1970.091 1	4		$25033_{9/2} - 75762^{\circ}_{9/2}$	1953.531 1953.321	20 5	51189.4 51194.9	
1970.573 80 1970.091 1		00.23.0	2000 9/2 10.02 9/2	1700.021		0.1.7	
1970.091	4			1952.395	1	51219.1	$18211_{5/2} - 69431^{\circ}_{7/3}$
	80	50746.7	$12846_{9/2} - 63593^{\circ}_{9/2}$	1951.968	2	51230.3	
1969.791 40	1	50759.1	$39870_{9/2} - 90629^{\circ}_{9/2}$	1951.018	200 b l	51255.3	
	40	50766.8	$18211_{5/2} - 68978^{\circ}_{5/2}$	1950.864	1	51259.3	$16135_{7/2} - 67395^{\circ}_{5/3}$
1969.650 20	20	50770.4	$17534_{15/2} - 68305^{\circ}_{15/2}$	1949.759	100	51288.4	14859 _{11/2} — 66148° ₁₃
1969.468	10	50775.1	$18211_{5/2} - 68987^{\circ}_{7/2}$	1949.156	60	51304.3	$12846_{9/2} - 64150^{\circ}_{11}$
	60		3/2 3/2 3/2	1948.364	10	51325.1	$27138_{7/2} - 78463^{\circ}_{7/2}$
	40		$16135_{7/2} - 66943^{\circ}_{5/2}$				$17627_{9/2} - 68987_{7/2}^{\circ}$
				1947.036	10	51360.1	
	10 20		$24470_{7/2} - 75294^{\circ}_{7/2}$	1946.900 1946.830	$\begin{vmatrix} 1\\3 \end{vmatrix}$	51363.7 51365.6	$14558_{9/2} - 65922^{\circ}_{11}$

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

${\stackrel{\lambda_{\rm vac}}{{\rm A}}}$	Intensity	$\sigma \atop (cm^{-1})$	Classification ^a	$\mathop{\rm A}_{\rm vac}^{\rm A}$	Intensity	σ (cm^{-1})	Classification ^a
1946.417	80	51376.4	$14558_{\ 9/2}-\ 65935^{\circ}_{\ 7/2}$				$23532_{5/2} - 75560^{\circ}_{5/2}$
1945.646	2	51396.8	3/2	1921.828	2	52033.8	
1945.053	1	51412.5	$17113_{13/2} - 68525^{\circ}_{11/2}$	1921.763	50	52035.6	$19700_{11/2} - 71736^{\circ}_{11/2}$
943.835	8	51444.7	$18241_{11/2} - 69686^{\circ}_{9/2}$	1920.869	1	52059.8	15100 11/2 11100 11/2
1943.650	4	51449.6	$23844_{9/2} - 75294^{\circ}_{7/2}$	1919.639	1	52093.1	
1943.293	10	51459.0		1919.162	30	52106.1	$19872_{7/2} - 71978^{\circ}_{7/2}$
1943.248	30	51460.2	$18921_{15/2}$ $- 70381^{\circ}_{13/2}$	1918.562	100	52122.4	$19872_{7/2} - 71994^{\circ}_{5/2}$
941.939	2	51494.9	$21535_{9/2} - 73029^{\circ}_{9/2}$	1917.201	1	52159.4	
941.556	100	51505.1	$13352_{11/2} - 64857^{\circ}_{9/2}$	1916.741	4	52171.9	$31254_{7/2} - 83426^{\circ}_{5/2}$
941.250	2	51513.2	$13352_{11/2}$ — $64865^{\circ}_{11/2}$	1916.507	1	52178.3	
940.930	2	51521.7		1916.106	50	52189.2	$14859_{11/2} - 67049^{\circ}_{9/2}$
940.853	5	51523.7	$15525_{11/2}$ — $67049^{\circ}_{9/2}$	1915.296	1	52211.2	
940.770	2	51525.9		1914.681	2	52228.0	$27138_{7/2} - 79366^{\circ}_{5/2}$
939.299	100	51565.0		1913.964	70	52247.6	
939.161	10	51568.7		1913.622	1	52256.9	$27138_{7/2} - 79395^{\circ}_{7/2}$
1937.726	20	51606.9		1913.339	2	52264.6	
1937.127	10	51622.8	$18063_{9/2} - 69686^{\circ}_{9/2}$	1913.284	100 b l	52266.2	
936.659	40	51635.3	$15045_{5/2} - 66681^{\circ}_{5/2}$	1912.698	5	52282.2	
936.478	3	51640.1	$28720_{9/2} - 80360^{\circ}_{11/2}$	1912.651	20	52283.4	$19308_{11/2}$ $- 71592^{\circ}_{9/2}$
936.375	1	51642.9		1911.251	3	52321.8	
935.588	30	51663.9	$19872_{7/2} - 71536^{\circ}_{5/2}$	1910.242	2	52349.4	$15045_{5/2} - 67395^{\circ}_{5/2}$
935.290	1	51671.8	$38448_{9/2} - 90119^{\circ}_{11/2}$	1910.093	1	52353.5	
933.865	10	51709.9	$35801_{7/2} - 87511^{\circ}_{7/2}$	1909.895	3	52358.9	$23050_{3/2} - 75409^{\circ}_{3/2}$
933.775	100	51712.3	$19308_{11/2}$ — $71021^{\circ}_{9/2}$	1909.471	200	52370.5	$21238_{13/2}$ $- 73609^{\circ}_{11/2}$
933.491	1	51719.9	$19872_{7/2} - 71592^{\circ}_{9/2}$	1909.258	300	52376.4	$19360_{13/2}$ — $71736^{\circ}_{11/2}$
932.872	8	51736.5	18241 _{11/2} — 69978° _{11/2}	1907.956	4	52412.1	$25409_{7/2} - 77822^{\circ}_{5/2}$
932.181	5 b l	51755.0		1907.054	10	52436.9	
931.739	5	51766.8	$21611_{5/2} - 73378^{\circ}_{7/2}$	1906.750	10 b l	52445.3	
931.368	1	51776.8		1906.126	2	52462.4	$16516_{7/2} - 68978^{\circ}_{5/2}$
930.813	40	51791.6		1906.040	40	52464.8	$23175_{13/2} - 75640^{\circ}_{11/2}$
930.349	10	51804.1	$17627_{9/2} - 69431^{\circ}_{7/2}$	1905.819	20 h	52470.9	$16516_{7/2} - 68987^{\circ}_{7/2}$
930.001	3	51813.4		1905.688	10	52474.5	
929.920	20	51815.6	$16516_{7/2} - 68331^{\circ}_{7/2}$	1904.981	1	52494.0	$21611_{5/2} - 74105^{\circ}_{5/2}$
929.706	30	51821.4	$15045_{5/2} - 66867^{\circ}_{3/2}$	1904.862	3	52497.2	
928.246	7	51860.6		1904.625	1	52503.8	
1927.821	20	51872.0		1904.212	4	52515.2	
1927.774	20	51873.3	$15525_{11/2}$ — $67398^{\circ}_{9/2}$	1903.356	60	52538.8	$14859_{11/2}$ — $67398^{\circ}_{9/2}$ \sim
1927.678	4	51875.9	$14859_{\ 11/2} - 66735^{\circ}_{\ 13/2}$	1903.115	10 c l	52545.4	
1927.095	300	51891.6	$19700_{11/2}$ — $71592^{\circ}_{9/2}$	1903.083	10 c l	52546.3	$18990_{7/2} - 71536^{\circ}_{5/2}$
926.884	3	51897.3	$15045_{5/2} - 66943^{\circ}_{5/2}$	1902.215	2	52570.3	$13352_{11/2} - 65922^{\circ}_{11/2}$
925.579	.3 b l	51932.4		1901.979	4	52576.8	
925.184	10	51943.1	$27452_{5/2} - 79395^{\circ}_{7/2}$	1901.715	7	52584.1	
924.451	30	51962.9	$23651_{7/2} - 75614^{\circ}_{5/2}$	1900.811	5	52609.1	
923.365	300	51992.2	$23647_{13/2}$ $- 75640^{\circ}_{11/2}$	1900.561	1	52616.0	
923.154	2	51997.9		1899.627	1	52641.9	$24250_{3/2} - 76892^{\circ}_{3/2}$
922.689	200	52010.5	$12846_{9/2} - 64857^{\circ}_{9/2}$	1899.491	5	52645.7	
922.459	3	52016.7	$26446_{7/2} - 78463^{\circ}_{7/2}$	1898.200	80	52681.5	$14558_{9/2} - 67240^{\circ}_{7/2}$
922.394	1	52018.5	$12846_{9/2} - 64865^{\circ}_{11/2}$	1898.020	5	52686.5	$21418_{5/2} - 74105^{\circ}_{5/2}$
922.178	20	52024.3	$22080_{7/2} - 74105^{\circ}_{5/2}$				$34825_{7/2} - 87511^{\circ}_{7/2}$
922.047	10	52027.9	$16516_{7/2} - 68544^{\circ}_{9/2}$	1897.082	1	52712.5	$15525_{11/2} - 68238^{\circ}_{11/2}$

^a For doubly-classified lines, the wavelength is entered only once.

TABLE X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\lambda_{\mathrm{vac}}}{A}$	Intensity	σ (cm ⁻¹)	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{\mathrm{A}}$	Intensity	σ (cm ⁻¹)	Classification ^a
1896.430	6 c l	52730.6		1880.571	10	53175.3	
1896.409	$\begin{array}{c c} & 0 & l \\ 2 & c & l \end{array}$	52731.2		1879.845	4	53195.9	$35024_{7/2} - 88220^{\circ}_{9/2}$
1896.290	1	52734.6		1879.786	4	53197.5	$30505_{11/2} - 83703^{\circ}_{13/2}$
1895.474	2	52757.2		1879.673	1	53200.7	30303 11/2 03 103 13/2
1895.146	1	52766.4	$22527_{7/2} - 75294^{\circ}_{7/2}$	1879.571	$\begin{array}{c c} 2 & c & l \end{array}$	53203.6	
1894.672	2	52779.6	$18241_{11/2} - 71021^{\circ}_{9/2}$	1879.542	5	53204.4	
1894.520	1	52783.8	$15454_{13/2} - 68238^{\circ}_{11/2}$	1879.235	20	53213.1	$22080_{7/2} - 75294^{\circ}_{7/2}$
1894.358	3	52788.3	10,2	1878.823	10	53224.8	
1893.864	3	52802.1		1878.459	20	53235.1	
1893.751	1	52805.2		1877.694	10	53256.8	$20848_{5/2} - 74105^{\circ}_{5/2}$
1893.569	3	52810.3	$21294_{\ 7/2}\ -74105^{\circ}_{\ 5/2}$	1877.280	5	53268.5	17113 _{13/2} — 70381° _{13/2}
1893.334	1 h	52816.9		1876.933	100 b l	53278.4	
1893.181	10h	52821.2		1876.675	2	53285.7	$15045_{5/2} - 68331^{\circ}_{7/2}$
1892.506	60	52840.0	$14558_{9/2} - 67398^{\circ}_{9/2}$	1876.549	20	53289.3	$18211_{5/2} - 71501_{3/2}^{\circ}$
1892.266	1	52846.7	$17534_{15/2} - 70381^{\circ}_{13/2}$	1875.754	8	53311.9	$14558_{9/2} - 67870^{\circ}_{9/2}$
1892.183	5	52849.0	$15525_{11/2}$ — $68374^{\circ}_{9/2}$	1875.388	10	53322.3	$18063_{9/2} - 71385^{\circ}_{7/2}$
1892.050	4	52852.7	$21611_{5/2} - 74463^{\circ}_{3/2}$	1875.309	20	53324.6	$18211_{5/2} - 71536^{\circ}_{5/2}$
1891.609	2	52865.0	$17113_{13/2}$ — $69978^{\circ}_{11/2}$	1874.981	20	53333.9	
1890.948	5	52883.5		1874.079	60	53359.5	$23532_{5/2} - 76892^{\circ}_{3/2}$
1890.827	200	52886.9		1873.997	20	53361.9	
1890.665	2	52891.4		1873.914	5 b l	53364.2	
1889.832	2	52914.8	$16516_{7/2} - 69431^{\circ}_{7/2}$	1873.470	5	53376.9	***
1889.674	60	52919.2		1873.434	7	53377.9	14859 _{11/2} 68238° _{11/}
1888.294	30	52957.8	$18063_{9/2} - 71021^{\circ}_{9/2}$	1873.146	2	53386.1	1.31
1887.490	1	52980.4	$27380_{11/2} - 80360^{\circ}_{11/2}$	1872.737	200	53397.8	
1887.180	10	52989.1		1871.878	20	53422.3	4.
1886.792	4	53000.0	$15525_{11/2} - 68525^{\circ}_{11/2}$	1870.826	5	53452.3	1
1886.624	10	53004.7	$18990_{7/2} - 71994^{\circ}_{5/2}$	1870.354	1	53465.8	
1886.491	7	53008.5		1869.803	2	53481.6	2 4 -
1886.412	5	53010.7	$14859_{11/2} - 67870^{\circ}_{9/2}$	1868.246	1	53526.1	/ · · · · · · · · · · · · · · · · · · ·
1886.132	1	53018.6	$15525_{11/2}$ $-68544^{\circ}_{9/2}$	1867.982	5	53533.7	$22080_{7/2} - 75614^{\circ}_{5/2}$
1885.940	3	53024.0		1867.565	200	53545.7	$16135_{7/2} - 69681^{\circ}_{5/2}$
1885.869	4	53026.0	26005 701968	1867.224	5	53555.4	
1885.328 1885.015	3 5	53041.2 53050.0	$26095_{11/2} - 79136^{\circ}_{13/2}$	1866.957 1866.678	5 1	53563.1 53571.1	$24250_{3/2} - 77822^{\circ}_{5/2}$
							0,2
1884.653	3	53060.2		1866.179	30	53585.4	
1884.399	20	53067.3		1865.842	4	53595.1	
1884.152	10	53074.3	10046 (5000°	1865.698	5	53599.2	
1884.105	1	53075.6	$12846_{9/2} - 65922^{\circ}_{11/2}$	1865.530	10 c l	53604.1	
1883.789	3	53084.5		1865.503	10 c l	53604.8	
1883.700	50 c l	53087.0	$22527_{7/2} - 75614^{\circ}_{5/2}$	1865.232	20	53612.6	$15525_{11/2}$ $-69138^{\circ}_{9/2}$
1883.647	50 c l	53088.5	$12846_{9/2} - 65935^{\circ}_{7/2}$	1865.139	40	53615.3	$20848_{5/2} - 74463^{\circ}_{3/2}$
1883.315	2	53097.9	20505	1865.061	2	.53617.6	
1883.184 1883.007	50 1	53101.6 53106.5	$30505_{\ 11/2} -\ 83607^{\circ}_{\ 11/2}$	1864.141 1863.670	50 b l 20	53644.0 53657.6	$35291_{9/2} - 88948^{\circ}_{9/2}$
1000 020	9	52100.7		1962 202	20	53665 5	14859 _{11/2} — 68525° _{11/2}
1882.932	2	53108.7		1863.393	20	53665.5	14039 11/2 08525 11/
1882.843	3	53111.2		1863.347	5	53666.9	
1882.031	20 500	53134.1	$25979_{15/2} - 79136^{\circ}_{13/2}$	1863.289 1863.044	10	53668.5 53675.6	$24788_{9/2} - 78463^{\circ}_{7/2}$
1881.224	500 10	53156.9 53163.5	$16516_{7/2} - 69681^{\circ}_{5/2}$	1862.028	4h	53704.9	24100 9/2 10403 7/2

^a For doubly-classified lines, the wavelength is entered only once.

TABLE X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\boldsymbol{\lambda_{vac}}}{\mathbf{A}}$	Intensity	σ (cm ⁻¹)	Classification ^a	$egin{pmatrix} \lambda_{ m vac} \ A \end{bmatrix}$	Intensity	$\sigma_{\rm (cm^{-1})}$	Classification ^a
1061 467	60	F2701 1	10200 72020°	1042 574	4	E4949 E	
1861.467	60	53721.1	$19308_{11/2}$ $- 73029^{\circ}_{9/2}$	1843.574	4	54242.5	10260 72600°
861.040	10	53733.4		1843.356	10	54248.9	19360 _{13/2} — 73609° ₁
860.876	30	53738.1		1842.950	10	54260.8	$21148_{3/2} - 75409^{\circ}_{3}$
860.257	10	53756.0	$15045_{5/2} - 68801^{\circ}_{7/2}$	1842.789	200	54265.6	$21294_{7/2} - 75560^{\circ}_{5}$
1860.167	100	53758.6	$17627_{9/2} - 71385^{\circ}_{7/2}$	5	la.		26095 _{11/2} — 80360° ₁
			$21535_{9/2} - 75294^{\circ}_{7/2}$	1842.365	60	54278.1	14859 _{11/2} — 69138° ₉
1859.679	40h	53772.7	$14558_{9/2} - 68331_{7/2}^{\circ}$	1842.235	5	54281.9	
1859.328	5	53782.9	$18211_{5/2} - 71994^{\circ}_{5/2}$	1841.926	1	54291.0	$35828_{9/2} - 90119^{\circ}_{1}$
1859.270	5	53784.6		1841.729	2	54296.8	
1858.198	10	53815.6	$14558_{9/2} - 68374^{\circ}_{9/2}$	1841.514	6	54303.1	20160 _{3/2} - 74463°;
1857.791	5w	53827.4		1841.463	2	54304.6	
1857.615	5	53832.5		1841.311	2	54309.1	
			· .	1840.954	10 c l	54319.7	$21294_{7/2} - 75614^{\circ}$
1857.212	10	53844.1					21294 7/2 13014
1857.044	$\frac{1}{h}$	53849.0		1840.585	1 1	54330.6	
1856.931	1	53852.3		1840.136	3	54343.8	
1856.144	10	53875.1	$21418_{5/2} - 75294^{\circ}_{7/2}$	1839.547	2	54361.2	
1856.053	10	53877.8		1838.456	200	54393.5	$12846_{9/2} - 67240^{\circ}$
1855.878	10 c l	53882.8	$15525_{11/2} - 69408^{\circ}_{11/2}$	1838.198	50	54401.1	21238 _{13/2} — 75640°
1855.601	2	53890.9		1837.984	20	54407.4	, "
1855.511	10 h	53893.5		1837.352	3	54426.2	*
1855.117	3	53905.0	30505 _{11/2} — 84410° _{9/2}	1837.311	1	54427.4	
1855.004	30	53908.2	$19700_{11/2} - 73609^{\circ}_{11/2}$	1837.189	2	54431.0	
1854.181	5 c l	53932.2	131.00 11/2	1837.074	6	54434.4	
1853.958	10h	53938.6		1836.887	3	54439.9	
1853.754	1011	53944.6	$20160_{3/2} - 74105^{\circ}_{5/2}$	1836.705	3	54445.3	20848 5/2 - 75294
1853.326	4	53957.0	$25409_{7/2} - 79366^{\circ}_{5/2}$	1836.635	5	54447.4	
			2540 7/2 1550 5/2	1836.471	7	54452.3	15525 11/2 69978
1853.288	4	53958.2	1 - 1	1835.696	2	54475.2	15525 11/2 05510
1853.078	4	53964.3		ll .			
1852.481	2	53981.7		1835.657	1	54476.4	
1852.409	2h	53983.8		1835.219	1	54489.4	
1851.891	1	53998.8	$21294_{7/2} - 75294^{\circ}_{7/2}$	1834.398	8	54513.8	
1850.099	8	54051.2	$31254_{7/2} - 85306^{\circ}_{5/2}$	1833.240	100	54548.2	
1849.381	10	54072.1		1833.120	100	54551.8	
1849.277	2	54075.2		1832.466	2	54571.3	
1848.358	4	54102.1		1832.331	15	54575.3	$29835_{9/2} - 84410$
1848.161	2	54107.8		1831.264	4	54607.1	, ,
1847.484	10	54127.7		1831.212	8	54608.6	
1847.308	10 b l	54132.8		1830.872	50	54618.8	$23844_{9/2} - 78463$
1847.196	20 c l	54136.1		1830.727	1	54623.1	17113 _{13/2} — 71736
1847.167	2	54137.0		1830.593	100 h	54627.1	10,2
1847.014	10	54141.4		1830.311	20	54635.5	15045 7/2 - 69681
	20			1829.742	10h	54652.5	100 10 7/2 07001
1846.935		54143.8		1829.313	100h	54665.3	
1846.836	40	54146.6	W.				
1846.378 1846.187	20	54160.1 54165.7	, , , , , , , , , , , , , , , , , , ,	1828.849 1828.589	5 <i>b l</i> 1	54679.2 54687.0	
	1	E4174 0		1000 104	9	54609.7	78694° _{11/2} —133393
1845.896	1	54174.2		1828.196	$\frac{2}{2}$	54698.7	10094 11/2-153393
1844.951	2	54202.0		1828.045	2	54703.2	
1844.862	3	54204.6	7	1827.758	4	54711.8	
1844.590	1	54212.6		1826.966	10	54735.6	
1843.910	20	54232.6	$19872_{7/2} - 74105^{\circ}_{5/2}$	1825.989	2	54764.8	

 $^{^{\}rm a}\, {\rm For}$ doubly-classified lines, the wavelength is entered only once.

TABLE X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

7							4 / 4
$\overset{\lambda_{\mathrm{vac}}}{{\mathrm{A}}}$	Intensity	σ (cm ⁻¹)	Classification ^a	λ _{vac} Å	Intensity	σ (cm ⁻¹)	Classification ^a
1007 700	1	5.4770.0	7	1700 247	20	55,000,0	
1825.792	1	54770.8	10041 70000°	1798.347	20	55606.6	
1825.215	2	54788.1	$18241_{11/2}$ $73029^{\circ}_{9/2}$	1797.273	20	55639.8	12046 (0402°
1823.960	3	54825.8	25201 00110°	1797.085	20	55645.7	$12846_{\ 9/2} -\ 68492^{\circ}_{\ 7/2}$
1823.855	15	54828.9	$35291_{9/2} - 90119^{\circ}_{11/2}$	1797.011	1	55648.0	
1823.703	60	54833.5		1795.721	2	55687.9	
1823.561	30	54837.8	2 2	1795.662	10	55689.8	$28720_{9/2} - 84410^{\circ}_{9/2}$
1822.640	2	54865.5		1794.822	10	55715.8	$22747_{9/2} - 78463^{\circ}_{7/2}$
1822.514	20	54869.3	$16516_{7/2} - 71385^{\circ}_{7/2}$	1794.614	40 h	55722.3	
1821.782	4	54891.3		1794.164	1	55736.3	37
1821.451	8	54901.3	*	1793.973	40	55742.2	$19872_{7/2} - 75614^{\circ}_{5/2}$
1821.333	1	54904.8		1793.695	100	55750.8	
1820.860	50	54919.1		1793.502	40	55756.8	
1820.296	4	54936.1		1792.983	10	55773.0	
1819.595	30	54957.3	$26446_{7/2} - 81404^{\circ}_{5/2}$	1792.794	3	55778.8	
1819.292	15	54966.4	$18063_{9/2} - 73029^{\circ}_{9/2}$	1792.569	1	55785.9	$13352_{11/2}$ — $69138^{\circ}_{5/2}$
1819.259	10	54967.4		1792.101	1	55800.4	
1818.913	10	54977.9		1791.938	30	55805.5	
1818.031	10 b l	55004.6	Table 1	1791.690	80	55813.2	
1817.401	3	55023.6		1791.030	2	55826.2	
1817.344	7	55025.4		1790.071	2	55863.7	
1017 002	1	55025 1		1700 007		55065 I	
1817.023	1	55035.1	22647 79604°	1790.027	3	55865.1	
1816.643	400	55046.6	$23647_{13/2} - 78694^{\circ}_{11/2}$	1789.955	1 1	55867.3	
1816.484	2	55051.4		1789.656	5	55876.7	10079 75769°
1815.721 1815.025	30 4	55074.5 55095.7		1789.247 1789.129	$\begin{vmatrix} 1 \\ 1 \end{vmatrix}$	55889.4 55893.1	$19872_{7/2} - 75762^{\circ}_{9/2} 18211_{5/2} - 74105^{\circ}_{5/2}$
1015.025	4	33093.1		1709.129	1	55095.1	16211 5/2 - 74103 5/2
1814.295	40	55117.8	$14859_{11/2} - 69978^{\circ}_{11/2}$	1788.462	2	55914.0	$36640_{7/2} - 92554^{\circ}_{5/2}$
1812.375	20	55176.2		1787.770	3	55935.6	$22527_{7/2} - 78463^{\circ}_{7/2}$
1811.894	200w	55190.9		1787.635	1	55939.8	
1810.775	50	55225.0		1787.154	15	55954.9	$12846_{\ 9/2} -\ 68801^{\circ}_{\ 7/2}$
1810.611	3	55230.0		1786.964	4	55960.8	$23175_{13/2}$ $- 79136^{\circ}_{13/2}$
1809.556	4	55262.2	$23050_{3/2} - 78312^{\circ}_{1/2}$	1786.691	10 h	55969.4	
1808.516	15	55293.9	$22527_{7/2} - 77822^{\circ}_{5/2}$	1786.141	70	55986.6	
1808.106	30	55306.5		1785.885	10	55994.6	$25409_{7/2} - 81404^{\circ}_{5/2}$
1807.913	4	55312.4		1785.330	1	56012.0	.,-
1807.776	1	55316.6		1780.963	10 b l	56149.4	
1805.481	5	55386.9		1780.596	5	56161.0	14859 _{11/2} — 71021° _{9/2}
1804.775	40	55408.6		1780.210	10	56173.1	3/2
1804.354	10	55421.5	$19872_{7/2} - 75294^{\circ}_{7/2}$	1779.460	4	56196.8	
1803.399	2	55450.8	.,-	1779.025	2	56210.6	$21611_{5/2} - 77822^{\circ}_{5/2}$
1803.231	3 <i>b l</i>	55456.0		1778.732	1	56219.8	3/2
1803.100	3 <i>b l</i>	55460.0		1778.422	1	56229.6	
1802.430	20 b l	55480.6		1777.716	4	56251.9	$18211_{5/2} - 74463^{\circ}_{3/2}$
1802.292	2001	55484.9	$12846_{9/2} - 68331^{\circ}_{7/2}$	1777.452	2	56260.3	10211 5/2 17700 3/2
1802.186	5	55488.2	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1776.879	20	56278.4	
1801.964	1	55495.0	13/2	1776.515	15 h	56290.0	
1801.172	100	55519.4	23175 _{13/2} — 78694° _{11/2}	1774.491	5	56354.2	
1000 000	20		$38448_{9/2} - 93967^{\circ}_{7/2}$	1774.257	1 7	56361.6	
1800.902	20	55527.7	$12846_{9/2} - 68374^{\circ}_{9/2}$	1773.023	7	56400.8	0.0707
1800.839	10	55529.7		1772.390	1	56421.0	$38726_{7/2} - 95147^{\circ}_{9/2}$
1799.453	1	55572.4		1772.129	3	56429.3	

^a For doubly-classified lines, the wavelength is entered only once.

 $TABLE\ X.\quad \textit{Observed spectral lines of Pr\ III}\ in\ the\ vacuum\ ultra\ violet\ region-Continued$

$\overset{\lambda_{vac}}{A}$	Intensity	$\frac{\sigma}{(cm^{-1})}$	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{\mathring{\mathbf{A}}}$	Intensity	σ (cm ⁻¹)	Classification ^a
1771.958	4	56434.7		1740.056	1	57469.4	
1771.680	i	56443.6		1739.840	200	57476.6	
1771.545	15	56447.9		1738.971	30	57505.3	
1771.483	10	56449.9		1737.972	5h	57538.3	
1771.328	4	56454.8		1736.996	10	57570.6	
1769.398	100	56516.4	$23844_{\ 9/2} -\ 80360^{\circ}_{\ 11/2}$	1736.747	5	57578.9	
1769.064	20	56527.1	$21294_{7/2} - 77822^{\circ}_{5/2}$	1736.646	200	57582.2	. 1
1768.618	7	56541.3		1735.801	4	57610.3	2, 3
1768.479	10	56545.8		1735.757	1	57611.8	
1768.114	5	56557.4	4 4	1734.029	2	57669.2	$13352_{11/2}$ — $71021^{\circ}_{9/2}$
1766.432	3	56611.3	$22277_{3/2} - 78889^{\circ}_{3/2}$	1732.382	20	57724.0	25979 _{15/2} — 83703° _{13/2}
1765.543	2	56639.8		1731.526	2	57752.5	$23651_{7/2} - 81404^{\circ}_{5/2}$
1765.299	1	56647.6	$22747_{9/2} - 79395^{\circ}_{7/2}$	1731.442	2	57755.3	$21611_{5/2} - 79366^{\circ}_{5/2}$
1765.087	4	56654.4	$36642_{13/2} - 93296^{\circ}_{11/2}$	1729.702	3	57813.4	$23175_{13/2}$ — $80988^{\circ}_{13/2}$
1764.859	10 h	56661.7		1728.302	1	57860.3	$21535_{9/2} - 79395^{\circ}_{7/2}$
1763.122	20	56717.6		1727.281	1	57894.4	
1763.005	1	56721.3		1727.194	1	57897.4	$21238_{13/2}$ $- 79136_{13/2}$
1762.665	7	56732.3	$14859_{\ 11/2} - 71592^{\circ}_{\ 9/2}$	1725.553	3bl	57952.4	
1761.668	20	56764.4		1724.116	1	58000.7	
1761.052	2	56784.2		1723.641	10	58016.7	
1760.859	10	56790.5		1722.693	2	58048.6	
1760.518	10 h	56801.5		1722.011	15	58071.6	$21294_{7/2} - 79366^{\circ}_{5/2}$
1759.916	1	56820.9		1721.800	1	58078.8	
1759.318	30	56840.2		1721.473	1	58089.8	
1759.278	10 c l	56841.5	* 1	1721.102	5h	58102.3	
1758.351	5	56871.5		1720.034	2	58138.4	
1758.277	1	56873.9		1719.940	4	58141.6	
1758.196	7	56876.5	$14859_{\ 11/2} - 71736^{\circ}_{\ 11/2}$	1717.770	200	58215.0	$30733_{11/2}$ — $88948^{\circ}_{9/2}$
1755.522	20	56963.1	¥	1717.152	1	58236.0	
1755.445	4	56965.6	$31254_{7/2} - 88220^{\circ}_{9/2}$	1715.471	5	58293.0	
1754.934	10 h	56982.2		1713.147	4	58372.1	
1754.583	200	56993.6		1712.848	60 h	58382.3	$38448_{9/2} - 96830^{\circ}_{7/2}$
1753.297	10	57035.4		1712.381	1	58398.2	
1750.486	5 c l	57127.0		1712.058	1	58409.2	`
1750.462	5 c l	57127.8	$71978^{\circ}_{7/2}$ —129106 $_{9/2}$	1711.408	2h	58431.4	
1749.160	2	57170.3	$35384_{5/2} - 92554^{\circ}_{5/2}$	1710.139	2	58474.8	*
1748.330	5	57197.4		1709.377	5 h	58500.8	
1747.949	100	57209.9		1707.514	1	58564.7	$24461_{5/2} - 83025^{\circ}_{3/2}$
1746.225	1	57266.4		1706.743	10	58591.1	$19872_{7/2} - 78463^{\circ}_{7/2}$
1745.879	3	57277.7	$21611_{5/2} - 78889^{\circ}_{3/2}$	1705.705	50 <i>h</i>	58626.8	$28885_{9/2} - 87511^{\circ}_{7/2}$
1745.474	10 h	57291.0		1702.266	1	58745.2	$21418_{\ 5/2} -\ 80164^{\circ}_{\ 3/2}$
1745.329	2	57295.8		1700.952	20	58790.6	$28720_{9/2} - 87511^{\circ}_{7/2}$
1744.571	4	57320.7	20047 000000	1700.128	1	58819.1	$24788_{9/2} - 83607^{\circ}_{11/2}$
1743.957 1743.758	3	57340.9 57347.4	$23647_{13/2} - 80988^{\circ}_{13/2}$	1699.416 1698.689	$\begin{vmatrix} 3\\10 \end{vmatrix}$	58843.7 58868.9	
1743.377	400	57359.9	32760 _{13/2} — 90119° _{11/2}			59000 1	
1743.577			32100 13/2 90119 11/2	1697.558	3	58908.1 58050.5	
1742.574	$\frac{2}{10}$	57386.4 57402.9	$18211_{5/2} - 75614^{\circ}_{5/2}$	1696.079	15	58959.5	25400 - 94410°
1742.073	10	57 4 02.9 57 4 19.7	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1694.896 1694.547	100	59000.7 59012.8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

 $^{^{\}rm a}\, {\rm For}\ doubly\text{-}{\rm classified}$ lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\lambda_{\mathrm{vac}}}{\mathrm{A}}$	Intensity	σ (cm ⁻¹)	Classification ^a	$\mathop{\mathrm{A}}_{\mathrm{vac}}^{A}$	Intensity	$\sigma_{\rm (cm^{-1})}$	Classification ^a
1691.726	10	59111.2		1521.236	10	65736.0	
1689.800	2	59178.6		1520.128	1		12250 70126°
1687.085	1				1	65783.9	$13352_{11/2}$ — $79136^{\circ}_{13/2}$
		59273.8	20040 001648	1520.030	3	65788.2	
1685.905	1	59315.3	$20848_{5/2} - 80164^{\circ}_{3/2}$	1519.247	100	65822.1	
1685.033	2	59346.0	$35801_{7/2} - 95147^{\circ}_{9/2}$	1518.966	4 h	65834.2	
1684.583	1	59361.9		1518.655	2	65847.7	$12846_{9/2} - 78694^{\circ}_{11/2}$
1683.887	5	59386.4	$30733_{11/2} - 90119^{\circ}_{11/2}$	1518.560	2	65851.9	$15045_{5/2} - 80897^{\circ}_{3/2}$
1681.073	1 h	59485.8		1518.374	1	65859.9	
1680.841	8	59494.0	$19872_{7/2} - 79366^{\circ}_{5/2}$	1518.212	1	65867.0	
1679.872	1	59528.3	1,2	1518.142	40 h	65870.0	
1677.314	20 h	59619.1	*	1517.622	20 h	65892.6	
1676.900	30	59633.8	$71592^{\circ}_{9/2} - 131226_{9/2}$	1517.441	10	65900.4	$21611_{5/2} - 87511^{\circ}_{7/2}$
1676.363	3	59653.0	71392 9/2 131220 9/2	1517.341	100 h	65904.8	$21011_{5/2} - 37311_{7/2}$
1674.074	$\frac{3}{4h}$	59734.5		1516.753	5		65295° _{7/2} —131226 _{9/2}
1673.663	1	59749.2		1516.733	40w	65930.3 65939.9	05295 7/2 -151220 9/2
1.670.014		50775 0	10000	1514.045			
1672.914	4	59775.9	$19360_{13/2}$ — $79136^{\circ}_{13/2}$	1516.365	1	65947.2	21.525
1671.427	20	59829.1		1515.694	15	65976.4	$21535_{9/2} - 87511^{\circ}_{7/2}$
1667.796	4	59959.4	$23647_{13/2} - 83607^{\circ}_{11/2}$	1514.893	50 b l	66011.3	
1666.198	7	60016.9		1513.746	10 <i>h</i>	66061.3	
1666.118	1	60019.8		1513.602	5	66067.6	
1665.129	8	60055.4	$23647_{13/2} - 83703^{\circ}_{13/2}$	1513.530	5w	66070.7	18921 _{15/2} — 84992° _{15/2}
1663.639	1	60109.2	13/2	1512.678	1	66107.9	$26446_{7/2} - 92554^{\circ}_{5/2}$
1660.981	3	60205.4	$71021^{\circ}_{9/2} - 131226_{9/2}$	1512.632	1	66109.9	1,2
1657.206	2	60342.5	0/2	1512.206	100w	66128.6	14859 _{11/2} — 80988° _{13/3}
1654.182	3	60452.8	18241 ^{11/2} — 78694° _{11/2}	1511.988	10	66138.1	11005 11/2 00500 13/2
1653.351	2	60483.2		1511.274	4	66169.3	18241 _{11/2} — 84410° _{9/2}
1649.187	400w	60635.9		1510.693	10 <i>h</i>	66194.8	10241 11/2 04410 9/2
1648.067	3	60677.2	$18211_{5/2} - 78889^{\circ}_{3/2}$	1509.987	4	66225.7	
1645.043	1	60788.7	$10211 \frac{5}{2} = 70009 \frac{3}{2}$		50 <i>h</i>		
1630.147	$\frac{1}{5h}$	61344.2	$23647_{13/2} - 84992^{\circ}_{15/2}$	1509.565 1509.155	$\frac{30n}{2cl}$	66244.2 66262.2	$28885_{9/2} - 95147^{\circ}_{9/2}$
1627.434	200h	61446.4	$35384_{5/2} - 96830^{\circ}_{7/2}$	1508.867	7w	66274.9	$23844_{9/2} - 90119^{\circ}_{11/2}$
1624.969	1	61539.6	$35291_{9/2} - 96830^{\circ}_{7/2}$	1508.327	3	66298.6	
1622.622	1	61628.6	$19360_{13/2}$ — $80988^{\circ}_{13/2}$	1508.074	20h	66309.7	
1621.248	100	61680.9	$33466_{11/2}$ — $95147^{\circ}_{9/2}$	1506.863	3	66363.0	$27604_{9/2} - 93967^{\circ}_{7/2}$
1614.502	2	61938.6		1506.805	1	66365.6	$44903_{5/2} - 111268^{\circ}_{3/2}$
1611.809	100 c l	62042.1		1506.425	2	66382.3	
1604.766	1	62314.4		1505.774	3	66411.0	
1594.572	10	62712.7	$31254_{7/2} - 93967^{\circ}_{7/2}$	1505.654	300	66416.3	
1589.553	2	62910.8	1/2	1505.409	5	66427.1	$28720_{9/2} - 95147^{\circ}_{9/2}$
1580.105	3	63286.9	$29267_{5/2} - 92554^{\circ}_{5/2}$	1505.329	20 <i>h</i>	66430.7	20.20 9/2 9011. 9/2
1579.856	1	63296.9		1504.783	30	66454.8	$67049^{\circ}_{9/2} - 133503_{11/2}$
1574.825	1	63499.1		1504.761	400w	66455.7	0.019 9/2 100000 11/
1573.388	10 h	63557.1	2000502441°	1504.662	2	66460.1	69408° _{11/2} —135868 _{9/2}
1569.341			$28885_{9/2} - 92441^{\circ}_{7/2}$		400 b l	66471.8	
1509.541	5	63721.0 65309.5	$28720_{\ 9/2} -\ 92441^{\circ}_{\ 7/2}$	1504.398 1504.269	1	66477.5	23647 _{13/2} — 90119° _{11/}
1590 951	1	65265.0	10241 026078	1504.006	0	66405 6	46679 1191500
1529.851	1	65365.8	$18241_{11/2}$ — $83607^{\circ}_{11/2}$	1504.086	8	66485.6	46673 _{7/2} -113158° _{9/2}
1522.489	2h	65681.9		1503.607	20	66506.7	$25934_{5/2} - 92441^{\circ}_{7/2}$
1522.241	100h	65692.6	$27604_{9/2} - 93296^{\circ}_{11/2}$	1503.422	100 c l	66514.9	$27452_{5/2} - 93967^{\circ}_{7/2}$
			$22527_{7/2} - 88220^{\circ}_{9/2}$	1502.967	10	66535.1	1 2 4
1521.417	3	65728.2		1502.807	2	66542.1	

^a For doubly-classified lines, the wavelength is entraed only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

$\overset{\lambda_{\mathrm{vac}}}{\mathring{\mathbf{A}}}$	Intensity	$\sigma \atop (cm^{-1})$	Classification ^a	$egin{array}{c} \lambda_{ m vac} \ m \mathring{A} \end{array}$	Intensity	σ (cm ⁻¹)	Classification ^a
1502.688	10	66547.4	62558° _{11/2} —129106 _{9/2}	1487.561	15	67224.1	
1502.435	3	66558.6	02000 11/2 120100 9/2	1487.137	100 h	67243.3	
1502.435	10	66564.4		1486.827	1	67257.3	
1502.505	10	66592.3	*	1486.630	20h	67266.2	*
1501.054	20	66619.8	$25934_{5/2} - 92554^{\circ}_{5/2}$	1486.538	5	67270.4	
1500.901	3w	66626.6		1485.425	200	67320.8	
1500.675	10	66636.7		1484.932	20	67343.2	$68525^{\circ}_{11/2}$ $-135868_{9/2}$
1500.445	20 h	66646.9		1484.661	50	67355.4	$66148^{\circ}_{13/2}$ – $133503_{11/2}$
1500.080	50	66663.1	$44679_{7/2} -111342^{\circ}_{7/2}$	1484.298	300w	67371.9	$22747_{9/2} - 90119^{\circ}_{11/2}$
1499.756	50w	66677.5	$23442_{11/2} - 90119^{\circ}_{11/2}$	1484.211	3	67375.9	
1499.586	3 h	66685.1	$21535_{9/2} - 88220^{\circ}_{9/2}$	1484.046	3	67383.4	63816° _{11/2} —131200 _{11/2}
1499.112	2	66706.2		1483.825	7	67393.4	
1498.566	4	66730.5	$69138^{\circ}_{9/2} - 135868_{9/2}$	1483.598	10	67403.7	
1498.426	1	66736.7		1483.508	5	67407.8	$25033_{9/2} - 92441^{\circ}_{7/2}$
1497.724	1	66768.0	66735° _{13/2} —133503 _{11/2}	1483.470	8	67409.5	63816° _{11/2} —131226 _{9/2}
1497.352	3	66784.6	$23844_{9/2} - 90629^{\circ}_{9/2}$	1483.400	10	67412.7	
1496.880	7	66805.6		1482.662	3	67446.2	
1496.831	8	66807.8		1482.585	10	67449.8	
1496.247	20	66833.9		1482.548	1	67451.4	
1495.999	200	66845.0		1482.417	20	67457.4	17534 _{15/2} — 84992° _{15/2}
1495.547	30	66865.2	62240° _{11/2} —129106 _{9/2}	1482.127	10	67470.6	65922° _{11/2} —133393 _{13/2}
1495.506	7	66867.0		1481.704	3	67489.9	
1495.220	200	66879.8		1481.609	1	67494.2	68374° _{9/2} —135868 _{9/2}
1495.047	2h	66887.5		1481.475	7	67500.3	$61605^{\circ}_{7/2}$ $-129106_{9/2}$
1494.944	20h	66892.1		1481.193	5	67513.1	
1494.747	10	66901.0	68544° _{9/2} -135445 _{7/2}	1481.123	5	67516.3	24.44
1494.200	40w	66925.4	$21294_{7/2} - 88220^{\circ}_{9/2}$	1481.035	40	67520.3	$26446_{7/2} - 93967^{\circ}_{7/2}$
1493.724	4cl	66946.8		1480.953	3	67524.1	25/24 251450
1493.694	10 c l	66948.1	(04000 105445	1480.527	2	67543.5	$27604_{9/2} - 95147^{\circ}_{9/2}$
1493.590	5	66952.8	$68492^{\circ}_{7/2}$ $-135445_{7/2}$	1480.093	10 h	67563.3	
1492.951	4	66981.4	64915° 191900	1479.953	10	67569.7	
1492.874	60	66984.9	64215° _{13/2} —131200 _{11/2}	1479.887	40	67572.7	67070° 125445
1492.352	100w	67008.3	$13352_{11/2} - 80360^{\circ}_{11/2}$	1479.849	2	67574.5	67870° _{9/2} —135445 _{7/2}
1491.830 1491.713	$\frac{3}{10h}$	67031.8 67037.0	$25409_{\ 7/2} -\ 92441^{\circ}_{\ 7/2}$	1479.695 1479.549	$\begin{vmatrix} 20 \\ 10 b l \end{vmatrix}$	67581.5 67588.2	$65922^{\circ}_{11/2}$ $-133503_{11/2}$
	1		(4150° 12100(
1490.867	7	67075.1	$64150^{\circ}_{11/2}$ $-131226_{9/2}$	1479.300	2	67599.5	(25020 121200
1490.494	50	67091.8	$66301^{\circ}_{15/2}$ – $133393_{13/2}$	1479.136	10	67607.0	63593° _{9/2} —131200 _{11/2}
1490.431	2	67094.7	60991° 195445	1479.083	20	67609.4	
$1490.014 \\ 1489.937$	$ \begin{array}{c c} 3h \\ 50h \end{array} $	67113.5 67116.9	$68331^{\circ}_{7/2}$ $-135445_{7/2}$	1478.974 1478.835	$\begin{bmatrix} 2 \\ 5 \end{bmatrix}$	67614.4 67620.8	
1489.689	3	67128.1		1478.618	3	67630.7	68238° _{11/2} —135868 _{9/2}
1489.567	200	67133.6	25400 02554°	1478.572	8	67632.8	$63593^{\circ}_{9/2} - 131226_{9/2}$
1489.319	40	67144.8	$25409_{7/2} - 92554^{\circ}_{5/2}$	1478.527	20	67634.9	10079 075110
$1489.187 \\ 1489.073$	10h	67150.7 67155.9		1478.436 1478.324	10 20	67639.0 67644.2	$19872_{7/2} - 87511^{\circ}_{7/2}$
1499 094	100 h	67150 0		1478.253	10	67647.4	
1488.984	1001	67159.9		F 7 8 795 7 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5			$24788_{9/2} - 92441^{\circ}_{7/2}$
1488.202	20	67195.2	26005 02206°	1478.120	100	67653.5	24100 9/2 - 92441 7/2
1488.071	30 20	67201.1	$26095_{11/2} - 93296^{\circ}_{11/2}$	1478.048	20	67656.8	
1487.843	20	67211.4		1477.977	20 b l	67660.0	

 $^{^{\}rm a}$ For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

	1						
$\overset{\boldsymbol{\lambda_{\mathrm{vac}}}}{\overset{\boldsymbol{A}}{\boldsymbol{A}}}$	Intensity	σ (cm^{-1})	Classification ^a	$egin{array}{c} \lambda_{ m vac} \ A \end{array}$	Intensity	σ (cm ⁻¹)	Classification ^a
1477.550		(7(70.0		1466,000		60107.0	
1477.559	6	67679.2		1466.320	1	68197.9	
1477.506	3	67681.6		1466.011	1	68212.3	
1477.109	15	67699.8		1465.984	1	68213.6	
1477.046	7	67702.7		1465.899	2	68217.5	
			45044 119556°				15454 02702°
1476.843	30	67712.0	$45844_{3/2} - 113556^{\circ}_{5/2}$	1465.216	2	68249.3	15454 _{13/2} — 83703° _{13/2}
1476.566	2	67724.7		1465.124	200	68253.6	
1476.516	10	67727.0		1465.021	200	68258.4	
1476.274	200	67738.1		1464.853	3	68266.2	* * * * * * * * * * * * * * * * * * * *
1475.801							
	4	67759.8		1464.742	5 b l	68271.4	
1475.700	10	67764.4		1464.502	60w	68282.6	
1475.562	10	67770.8		1464.400	1	68287.3	
1475.508	20h	67773.3		1464.013	40	68305.4	
1475.411	200	67777.7		1463.825	100	68314.2	
							,
1474.094	50	67838.3		1463.756	10	68317.4	,
1474.013	100	67842.0		1463.554	400	68326.8	
1473.818	200w	67851.0		1463.332	200	68337.2	
1473.720	4h	67855.5		1463.233	400	68341.8	
1473.364	2	67871.9		1462.700	30	68366.7	
			22747 00620°				
1473.155	2	67881.5	$22747_{9/2} - 90629^{\circ}_{9/2}$	1462.585	20	68372.1	
1472.995	1	67888.9		1462.155	50	68392.2	
1472.456	1	67913.7		1462.019	1	68398.6	
1472.332	20	67919.5		1461.616	100 h	68417.4	
1472.142	1	67928.2	2 2	1461.504		68422.7	
			서 그 :		1		
1472.102	2	67930.1		1461.405	4	68427.3	
1471.895	3	67939.6		1461.218	2	68436.0	
1471.767	30	67945.5	$28885_{9/2} - 96830^{\circ}_{7/2}$	1460.632	2	68463.5	
1471.518	3	67957.0		1460.440	2	68472.5	
1471.255	5	67969.2		1460.223	ī	68482.7	
1470.908	3	67985.2		1460.050	40	68490.8	1
1470.805	80	67990.0		1459.674	40	68508.4	$24788_{9/2} - 93296^{\circ}_{11/2}$
1470.324	10	68012.2		1459.405	3	68521.1	
1470.261	20 b l	68015.1		1459.339	100	68524.2	
1470.045	3w	68025.1		1459.257	2h	68528.0	$64865^{\circ}_{11/2}$ $-133393_{13/2}$
	2	68032.4	$25934_{5/2} - 93967^{\circ}_{7/2}$				04003 11/2 133393 13/2
1469.887			$23934 \frac{5}{2} = 93907 \frac{7}{2}$	1459.033	1	68538.5	
1469.649	2	68043.4		1458.771	8	68550.8	
1469.511	7	68049.8	$67395^{\circ}_{5/2}$ $-135445_{7/2}$	1458.701	2	68554.1	
1469.369	3	68056.4		1458.614	30h	68558.2	
1468.902	60	68078.1		1458.202	10	68577.6	
The strategies of the strategi	10		$24470_{7/2} - 92554^{\circ}_{5/2}$				
1468.779		68083.8		1458.130	100	68581.0	660500 305445
1468.573	5w	68093.3	$24461_{5/2} - 92554^{\circ}_{5/2}$	1457.894	2	68592.1	$66852^{\circ}_{7/2}$ $-135445_{7/2}$
1468.399	200	68101.4	$22527_{7/2} - 90629^{\circ}_{9/2}$	1457.784	10	68597.3	$23844_{9/2} - 92441^{\circ}_{7/2}$
1468.227	20	68109.3	$28720_{9/2} - 96830^{\circ}_{7/2}$	1457.512	30	68610.1	11-
1467.698	100 h	68133.9	0,2	1457.433	4h	68613.8	
	3	68136.3					
1467.646 1467.595	10	68138.7		1457.357 1457.257	$\begin{bmatrix} 3h \\ 5 \end{bmatrix}$	68617.4 68622.1	
1101.050	10	00100.1		1701.201	,	00022.1	
1467.409	4	68147.3		1456.949	40	68636.6	
1467.247	3	68154.8		1456.787	1	68644.2	
1467.153	7	68159.2		1456.738	î	68646.5	$64857^{\circ}_{9/2} - 133503_{11/2}$
							3 100 i 9/2 100000 11/2
1467.081	$\frac{10h}{2}$	68162.6		1456.574	2	68654.2	06446 051450
1466.971	2	68167.7		1455.583	30	68701.0	$26446_{7/2} - 95147^{\circ}_{9/2}$

 $^{^{\}rm a}$ For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

$\overset{\lambda_{vac}}{A}$	Intensity	σ (cm ⁻¹)	Classification ^a	$egin{array}{c} \lambda_{ m vac} \ m \mathring{A} \end{array}$	Intensity	σ (cm ⁻¹)	Classification ^a
1454.957	400 b l	68730.6	4	1440.844	1 h	69403.8	*
1454.832	4	68736.4	, '	1440.733	10 <i>h</i>	69409.1	
1454.775	5	68739.2		1440.234	5	69433.2	
1454.602	5	68747.3	$46673_{7/2}$ $-115420^{\circ}_{7/2}$	1439.922	30	69448.2	19062 97511°
1454.002	5	00747.3	$14859_{11/2} - 83607^{\circ}_{11/2}$	1439.540	100	69466.6	$18063_{9/2} - 87511^{\circ}_{7/2}$
1454.265	20	68763.2		1439.420	10 h	69472.4	
1454.029	40	68774.4		1438.925	2	69496.3	$24470_{7/2} - 93967^{\circ}_{7/2}$
1453.934	5	68778.9		1438.766	3	69504.0	$23050_{3/2} - 92554^{\circ}_{5/2}$
1453.705	7	68789.8	$16516_{7/2} - 85306^{\circ}_{5/2}$	1438.719	5	69506.3	$24461_{5/2} - 93967^{\circ}_{7/2}$
1453.541	15	68797.5		1438.532	20 h	69515.3	,,2
1453.405	30	68803.9		1438.037	50 h	69539.2	
1453.094	20 h	68818.7		1437.871	1	69547.3	
1453.014	100 h	68822.5		1437.405	7	69569.8	
1452.887	40	68828.5		1435.977	10	69639.0	
1452.569	1	68843.6	$14859_{\ 11/2} -\ 83703^{\circ}_{\ 13/2}$	1434.845	40	69693.9	$45805_{9/2} - 115499^{\circ}_{9/2}$
1452.478	1	68847.8		1434.629	40 h	69704.4	
1452.352	400	68853.8		1434.540	5 h	69708.8	
1452.005	8 h	68870.3		1434.187	20h	69725.9	
1451.783	100	68880.8	$21238_{13/2} - 90119^{\circ}_{11/2}$	1434.090	10 h	69730.6	
1451.358	300 h	68901.0		1433.936	20	69738.1	$25409_{7/2} - 95147^{\circ}_{9/2}$
1451.193	30	68908.8	$23532_{5/2} - 92441^{\circ}_{7/2}$	1432.971	5 h	69785.1	
1450.960	4h	68919.9		1432.015	5 h	69831.7	
1450.500	2	68941.7	²	1431.711	5w	69846.5	
1450.403	4	68946.4		1431.554	3	69854.1	$23442_{11/2} - 93296^{\circ}_{11/2}$
1450.241	10 h	68954.0		1431.244	20	69869.3	$61357^{\circ}_{9/2}$ $-131226_{9/2}$
1448.814	5	69022.0	$23532_{5/2} - 92554^{\circ}_{5/2}$	1431.103	40	69876.2	
1448.524	10 h	69035.8		1431.014	100	69880.5	
1448.168	100	69052.8	$26095_{11/2} - 95147^{\circ}_{9/2}$	1430.930	3	69884.6	$17627_{9/2} - 87511^{\circ}_{7/2}$
1447.963	4	69062.5		1430.543	5	69903.5	1
1447.616	100	69079.1	**	1430.329	20	69914.0	$22527_{7/2} - 92441^{\circ}_{7/2}$
1447.301	3	69094.1	$21535_{9/2} - 90629^{\circ}_{9/2}$	1430.158	300	69922.3	
1446.361	1	69139.0	$48401_{3/2} - 117540^{\circ}_{3/2}$	1429.627	1	69948.3	
1445.822	50 h	69164.8	-,-	1428.703	3	69993.6	$45807_{5/2} - 115800^{\circ}_{5/2}$
1445.659	4	69172.6		1428.018	40	70027.1	$22527_{7/2} - 92554^{\circ}_{5/2}$
1445.517	300	69179.4	$24788_{9/2} - 93967^{\circ}_{7/2}$	1427.709	20	70042.3	1/2
1445.279	2	69190.8		1427.561	3	70049.5	
1445.033	3h	69202.6		1427.014	100	70076.4	
1444.551	50 h	69225.7		1426.067	100	70122.9	$23844_{9/2} - 93967^{\circ}_{7/2}$
1444.331	2	69236.2		1424.775	2	70186.5	3/2
1444.106	20	69247.0		1424.001	1	70224.7	
1443.659	2h	69268.4	$64235^{\circ}_{~9/2}$ $-133503_{~11/2}$	1423.653	5	70241.8	
1443.470	400	69277.5	11/2	1423.393	3	70254.7	
1443.005	1	69299.8	$18211_{5/2} - 87511^{\circ}_{7/2}$	1423.187	4 h	70264.8	
1442.865	$\frac{1}{3h}$	69306.6	0,2	1423.114	2h	70268.4	*
1442.750	5 h	69312.1	, A	1422.943	2	70276.9	$22277_{3/2} - 92554^{\circ}_{5/2}$
1442.290	10	69334.2	$21294_{7/2} - 90629^{\circ}_{9/2}$	1422.718	10	70288.0	
1442.085	7	69344.0	.,,_	1422.551	10 h	70296.2	
1441.730	7	69361.1		1422.079	3 h	70319.6	
1441.388	20	69377.6	$27452_{5/2} - 96830^{\circ}_{7/2}$	1421.745	10	70336.1	
1440.948	20 h	69398.8		1421.636	20	70341.5	

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

$\overset{\lambda_{vac}}{A}$	Intensity	σ (cm ⁻¹)	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{A}$	Intensity	σ (cm ⁻¹)	Classification ^a
1421.479	1	70349.3		1406.681	15	71089.3	
1421.262	100	70360.0	$24788_{9/2} - 95147^{\circ}_{9/2}$	1406.071	15	71120.2	44670 -115900°
1420.795	15	70383.1	$26446_{7/2} - 96830^{\circ}_{7/2}$	1405.544	50		44679 _{7/2} -115800° _{5/}
1420.733	5		20440 7/2 - 90030 7/2	1405.434		71146.8	$21294_{7/2} - 92441^{\circ}_{7/2}$
		70406.0	10700 00110°		2	71152.4	62240° _{11/2} —133393 ₁₃
1420.071	50 h	70419.0	19700 _{11/2} — 90119° _{11/2}	1405.100	1,	71169.3	
1420.021	10 c l	70421.5		1404.974	30	71175.7	
1418.966	7	70473.8	$22080_{7/2} - 92554^{\circ}_{5/2}$	1404.747	300	71187.2	
1418.477	2	70498.1		1404.102	20	71219.9	$22747_{9/2} - 93967^{\circ}_{7/2}$
1417.458	1	70548.8	$22747_{9/2} - 93296^{\circ}_{11/2}$	1403.981	300	71226.0	
1417.081	20	70567.6		1403.868	4	71231.8	
1416.779	20	70582.6		1403.598	60	71245.5	
1416.165	5	70613.2		1403.310	100	71243.3	$21294_{7/2} - 92554^{\circ}_{5/2}$
1415.874	1	70627.8	$64817^{\circ}_{5/2}$ $-135445_{7/2}$	1403.171	100		$21294_{7/2} - 92334_{5/2}$
1415.756	300		04017 5/2 -133443 7/2			71267.2	
		70633.6		1402.907	40	71280.6	10005 1111010
1414.393	3	70701.7		1402.743	20	71288.9	$40205_{3/2} -111494^{\circ}_{5/2}$
1414.230	2	70709.8		1402.599	3	71296.2	
1414.137	50	70714.5	$62678^{\circ}_{13/2} - 133393_{13/2}$	1402.458	8	71303.4	$23844_{9/2} - 95147^{\circ}_{9/2}$
1413.766	3	70733.1	10/2	1402.122	8	71320.5	$19308_{11/2} - 90629^{\circ}_{9/2}$
1413.674	10	70737.7		1402.047	100 c l	71324.3	19308 11/2 90029 9/
1413.359	5	70753.4		1402.030	30 c l		
1410.009		10133.4		1402.030	30 C t	71325.2	
1413.235	3 h	70759.6	$19360_{\ 13/2} -\ 90119^{\circ}_{\ 11/2}$	1401.774	3	71338.2	
1412.825	400	70780.2		1401.405	4	71357.0	
1412.655	5 h	70788.7		1401.176	100	71368.6	
1412.492	3	70796.9		1400.611	20 h	71397.4	
1412.297	20	70806.6	$60419^{\circ}_{11/2} - 131226_{9/2}$	1400.434	7	71406.4	$21148_{3/2} - 92554^{\circ}_{5/3}$
1412.087	10	70817.2		1400.359	7 h	71410.3	
1411.924	20	70825.3	$62678^{\circ}_{13/2}$ $-133503_{11/2}$	1400.160	3	71420.4	$25409_{7/2} - 96830^{\circ}_{7/2}$
1411.819	20	70830.6	$21611_{5/2} - 92441^{\circ}_{7/2}$	1399.141	5	71472.4	$39870_{9/2} -111342^{\circ}_{7/2}$
1411.732	100 h	70835.0	21011 5/2 92441 7/2	1398.824		71488.6	39070 9/2 -111342 7/
			,		40		
1411.399	10 c l	70851.7		1398.695	5	71495.2	
1411.372	3 c l	70853.0		1398.619	40	71499.1	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
1411.184	2	70862.5		1397.919	2	71534.9	
1410.745	10	70884.5	$50647_{11/2}$ — $121532^{\circ}_{11/2}$	1397.770	4	71542.5	9:
1410.651	100	70889.3	$64979^{\circ}_{7/2}$ $-135868_{9/2}$	1397.421	100 h	71560.4	
1410.528	10 b l	70895.4	$25934_{5/2} - 96830^{\circ}_{7/2}$	1397.344	20	71564.3	
1410.304	60	70906.7	$21535_{9/2} - 92441^{\circ}_{7/2}$	1397.227	5	71570.3	
1409.801	100 h	70932.0	$58174^{\circ}_{9/2} - 129106_{9/2}$	1396.842	7	71590.0	
1409.708	5	70936.7	9/2 12/10/9/2	1396.444	50	71610.5	
1409.700	3	70945.4	62558° _{11/2} —133503 _{11/2}	1396.219	20	71610.3	
1409.479	20	70948.2	$58158^{\circ}_{7/2}$ $-129106_{9/2}$	1395.722	20	71647.5	
1400.544	0	70005 0	16516 055110				
1408.544	3	70995.3	$16516_{7/2} - 87511^{\circ}_{7/2}$	1395.658	5	71650.8	
1408.221	10	71011.6	$64857^{\circ}_{9/2}$ $-135868_{9/2}$	1395.383	8	71664.9	7
1407.904	2	71027.6		1395.316	. 3	71668.4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1407.773	20	71034.2	$60166^{\circ}_{9/2}$ $-131200_{11/2}$	1395.196	4h	71674.5	
1407.574	3	71044.2	$64401^{\circ}_{5/2}$ $-135445_{7/2}$	1394.784	10	71695.7	45844 _{3/2} -117540° ₃
1407.485	30 h	71048.7		1394.718	20 h	71699.1	
1407.352	6	71055.4		1394.585	60	71705.9	$20848_{5/2} - 92554^{\circ}_{5}$
1407.283	10 c l	71058.9	$13352_{11/2} - 84410^{\circ}_{9/2}$	1071.000	00	11100.7	$23442_{11/2} - 95147^{\circ}_{9/2}$
1407.260	10 c l	71060.1	$60166^{\circ}_{9/2}$ $-131226_{9/2}$	1394.540	2	71708.2	20772 11/2 95147 9/
- 101.200	1000	11000.1	JULUU 9/2 101220 9/2	エリノエ・リオリ	4	111100.4	

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

$\overset{\boldsymbol{\lambda_{\mathrm{vac}}}}{\mathbf{A}}$	Intensity	$\sigma \ (\mathrm{cm^{-1}})$	Classification ^a	$egin{array}{c} \lambda_{ m yac} \ A \end{array}$	Intensity	σ (cm ⁻¹)	Classification ^a
1394.323	20	71719.4		1370.129	2	72005 0	92044 06020°
1393.964	20	71737.9		1368.661	2	72985.8 73064.1	$23844_{9/2} - 96830^{\circ}_{7/2}$
1393.905	4	71740.9		1367.730	100 h		
1393.526	2	71760.4		1366.761	5 3	73113.8	
1393.452	100	71764.2		1366.522	3	73165.7 73178.5	$23651_{7/2} - 96830^{\circ}_{7/2}$
1392.825	100	71796.5	$25033_{\ 9/2} -\ 96830^{\circ}_{\ 7/2}$	1366.392	200	73185.4	
1392.651	3	71805.5		1364.645	1	73279.1	
1392.367	1	71820.1		1364.382	2	73293.2	
1390.762	3	71903.0	,	1364.303	1	73297.5	$39725_{15/2}-113023^{\circ}_{17/2}$
1390.367	100	71923.4		1363.020	2	73366.5	0312013/2 110020 11/2
1390.301	2	71926.9		1362.453	40 h	73397.0	
1390.089	5	71937.8		1362.371	20 h	73401.4	$44679_{7/2} - 118081^{\circ}_{9/2}$
1389.786	7	71953.5		1362.113	1	73415.4	$44903_{5/2} - 118318^{\circ}_{7/2}$
1389.588	100 h	71963.8		1361.813	2	73431.5	1,2
1389.240	7w	71981.8	,	1359.082	3 h	73579.1	
1388.403	2	72025.2		1359.003	30 h	73583.4	
1388.073	1	72042.3	$24788_{9/2} - 96830^{\circ}_{7/2}$	1358.233	2	73625.1	
1388.004	1	72045.9		1356.483	200 h	73720.0	
1387.775	40	72057.8	$21238_{13/2} - 93296^{\circ}_{11/2}$	1356.355	2h	73727.0	$40098_{5/2} - 113825^{\circ}_{3/2}$
1387.268	4	72084.1	$16135_{7/2} - 88220^{\circ}_{9/2}$	1355.383	1	73779.9	
1387.136	2	72091.0		1355.214	3	73789.1	44679 _{7/2} —118468° _{9/2}
1386.163	3	72141.6	$44903_{5/2}$ $-117044^{\circ}_{7/2}$	1354.815	2	73810.8	
1385.459	5 h	72178.2		1353.997	2	73855.4	
1384.669	3	72219.4		1353.601	10 h	73877.0	
1383.796	10	72265.0		1353.151	3	73901.6	
1383.656	300 h	72272.3		1352.987	2	73910.5	39870 _{9/2} —113780° _{9/2}
1383.608	2	72274.8	$45805_{9/2} - 118081^{\circ}_{9/2}$	1352.697	600	73926.4	
1382.351	2	72340.5		1352.511	300	73936.5	$19360_{13/2}$ — $93296^{\circ}_{11/2}$
1382.193	2	72348.8		1350.905	1	74024.4	
1382.045	1	72356.5	$45844_{\ 3/2} -118201^{\circ}_{\ 3/2}$	1350.326	10 h	74056.2	
1381.886	2	72364.9	$44679_{\ 7/2}\ -117044^{\circ}_{\ 7/2}$	1350.171	20	74064.7	
1381.816	4	72368.5		1349.740	1	74088.3	61357° _{9/2} —135445 _{7/2}
1381.446	100	72387.9	18241 _{11/2} — 90629° _{9/2}	1349.618	7	74095.0	$19872_{7/2} - 93967^{\circ}_{7/2}$
1381.209 1380.107	10 40 h	72400.3 72458.2	$22747_{9/2} - 95147^{\circ}_{9/2}$	1349.334 1349.059	7 5	74110.6 74125.7	38785 _{15/2} —112896° _{15/2}
	40 <i>n</i>		,				
1379.958	3	72466.0	$45805_{9/2} - 118271^{\circ}_{11/2}$	1347.513	10	74210.8	36670 _{11/2} —110881° _{11/2}
1378.385	1	72548.7	$38785_{15/2}$ — $111335^{\circ}_{15/2}$	1347.328	5	74221.0	
1377.992	15	72569.4	$19872_{7/2} - 92441^{\circ}_{7/2}$	1347.162	30	74230.1	$18211_{5/2} - 92441^{\circ}_{7/2}$
1377.425	20	72599.2		1345.174	100 h	74339.8	$39485_{1/2} - 113825^{\circ}_{3/2}$
1376.770	15	72633.8	$38701_{13/2}$ — $111335^{\circ}_{15/2}$	1345.087	200w	74344.6	
1376.032	8	72672.7	$21294_{7/2} - 93967^{\circ}_{7/2}$	1344.704	5	74365.8	
1375.992	4	72674.8		1344.323	10	74386.9	
1375.847	1	72682.5	$19872_{7/2} - 92554^{\circ}_{5/2}$	1342.855	10	74468.2	36642 _{13/2} —1111110° _{13/2}
1374.618 1374.199	$\begin{bmatrix} 20h \\ 2 \end{bmatrix}$	72747.5 72769.7		1342.259 1338.810	100	74501.3 74693.2	36642 _{13/2} —111335° _{15/2}
			44000				13/2 111000 15/2
1373.939	10	72783.4	$44903_{5/2} - 117686^{\circ}_{5/2}$	1338.568	2 h	74706.7	
1372.124	3 h	72879.7		1337.468	40 h	74768.1	00501
$1371.420 \\ 1371.220$	$\begin{bmatrix} 100h \\ 2h \end{bmatrix}$	72917.1 72927.8		1335.134 1334.983	100	74898.8 74907.3	38701 _{13/2} —113600° _{13/2}

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region – Continued

$\overset{\mathbf{\lambda_{vac}}}{\mathbf{A}}$	Intensity	σ (cm ⁻¹)	Classification ^a	$egin{array}{c} \lambda_{ m vac} \ A \end{array}$	Intensity	σ (cm^{-1})	Classification ^a
1333.802	20 h	74973.6		1294.456	2	77252.5	
1332.359	1	75054.8	$18241_{11/2} - 93296^{\circ}_{11/2}$	1294.103	3	77273.6	26640 112014°
1331.490	1	75103.8	$15241_{11/2} - 93290_{11/2}$ $15525_{11/2} - 90629_{9/2}^{\circ}$	1294.103	10	77277.2	36640 _{7/2} -113914° _{5/2}
1330.985	60	75132.3	38701 _{13/2} —113833° _{15/2}	1293.079	5	77334.8	$13352_{11/2} - 90629^{\circ}_{9/2}$
1329.459	1	75218.6	30701 13/2 113033 15/2	1292.456	$\frac{3}{3h}$	77372.1	40205 _{3/2} -117540° _{3/2}
1328.452	30	75275.6	38549 _{1/2} -113825° _{3/2}	1292.062	1	77395.7	$15045_{5/2} - 92441^{\circ}_{7/2}$
1328.207	5	75289.5	$45805_{9/2} - 121095^{\circ}_{11/2}$	1291.104	20	77453.1	38785 _{15/2} —116238° _{15/2}
1325.155	4	75462.9	$41026_{17/2}$ $-116489^{\circ}_{17/2}$				39870 _{9/2} -117323° _{11/2}
1324.595	50 h	75494.8	11,2	1289.817	1	77530.4	3/3/3/3/2 11/323 11/2
1322.376	1	75621.4		1288.999	2	77579.6	$37919_{7/2} - 115499^{\circ}_{9/2}$
1321.520	5	75670.4	39732 _{11/2} —115403° _{11/2}	1287.736	2 h	77655.7	
1319.844	1	75766.5	$39732_{11/2}$ $-115499^{\circ}_{9/2}$	1286.935	300	77704.0	$38785_{15/2} - 116489^{\circ}_{17/2}$
1319.796	1	75769.3	$14859_{11/2} - 90629_{9/2}^{\circ}$	1286.530	40h	77728.5	13/2 220 201 11/2
1316.719	3	75946.4	$39725_{15/2} - 115672^{\circ}_{15/2}$	1286.233	1	77746.4	
1316.264	1	75972.6	$36670_{\ 11/2} - 112643^{\circ}_{\ 11/2}$	1284.023	10	77880.2	$37919_{7/2} -115800^{\circ}_{5/2}$
1315.596	1	76011.2	38785 _{15/2} —114797° _{13/2}	1278.394	3h	78223.1	
1314.573	2	76070.3	$14558_{9/2} - 90629^{\circ}_{9/2}$	1277.726	2	78264.0	
1314.136	20	76095.6	$38701_{13/2} - 114797^{\circ}_{13/2}$	1277.553	50 h	78274.6	
1313.582	10	76127.7	$36642_{13/2} - 112769^{\circ}_{13/2}$	1277.286	30	78291.0	
1313.538	2	76130.3	$35137_{3/2} - 111268^{\circ}_{3/2}$	1276.937	1	78312.4	
1313.376	5 h	76139.6		1276.817	2 h	78319.8	
1312.336	7	76199.0	$39732_{11/2}$ — $115933^{\circ}_{11/2}$	1276.612	2h	78332.3	
1310.972	1 h	76279.3	$37011_{5/2} - 113291^{\circ}_{7/2}$	1276.327	1	78349.8	$38694_{5/2} - 117044^{\circ}_{7/2}$
1310.898	2h	76283.6		1275.701	1	78388.3	
1310.307	2	76318.0	$35024_{\ 7/2} -111342^{\circ}_{\ 7/2}$	1274.924	20	78436.0	
1310.001	1	76335.8		1273.361	5	78532.3	$35024_{7/2} - 113556^{\circ}_{5/2}$
1309.831	2h	76345.7		1272.901	20	78560.7	$25244^{\circ}_{15/2} - 103805_{13/2}$
1308.577	2	76418.9	$16135_{7/2} - 92554^{\circ}_{5/2}$	1272.820	1	78565.7	$39120_{3/2} - 117686^{\circ}_{5/2}$
1308.234	2	76438.9	$39870_{9/2} - 116309^{\circ}_{11/2}$	1272.690	3	78573.7	$23091^{\circ}_{3/2} - 101665_{5/2}$
1307.215	20 h	76498.5		1271.934	10 h	78620.4	
1306.420	1	76545.1	$37011_{5/2} - 113556^{\circ}_{5/2}$	1271.829	1	78626.9	
1305.892	1	76576.0	$39732_{11/2}$ — $116309^{\circ}_{11/2}$	1269.499	1	78771.2	$34520_{5/2} - 113291^{\circ}_{7/2}$
1305.771	1	76583.1	$39870_{9/2} - 116453^{\circ}_{9/2}$	1269.345	1	78780.8	$36640_{7/2} - 115420^{\circ}_{7/2}$
1305.623	1	76591.8		1269.232	2	78787.8	37011 _{5/2} —115800° _{5/2}
1303.501	2	76716.5	$37197_{3/2} - 113914^{\circ}_{5/2}$	1268.819	2	78813.4	
1302.961	3	76748.3	$34520_{\ 5/2}\ -111268^{\circ}_{\ 3/2}$	1268.084	1	78859.1	36640 _{7/2} -115499° _{9/2}
1302.884	3h	76752.8		1267.783	40	78877.8	39732 _{11/2} —118610° _{13/2}
1302.696	10	76763.9	$39725_{15/2}$ — $116489^{\circ}_{17/2}$	1267.235	2h	78912.0	
1300.617	50	76886.6	$38785_{15/2}$ $-115672^{\circ}_{15/2}$	1266.730	2h	78943.4	
1300.285	3	76906.2	$18241_{11/2} - 95147^{\circ}_{9/2}$	1265.676	20	79009.2	$39870_{\ 9/2}\ -118879^{\circ}_{\ 11/2}$
1299.811	30 h	76934.3		1265.347	5	79029.7	36640 _{7/2} -115670° _{7/2}
1299.407	10	76958.2	36642 _{13/2} —113600° _{13/2}				$36642_{13/2} - 115672^{\circ}_{15/2}$
1299.193	2	76970.9	38701 _{13/2} —115672° _{15/2}	1264.221	10	79100.1	
1298.693	40	77000.5		1263.489	20	79145.9	39732 _{11/2} —118879° _{11/2}
1298.630	100	77004.2		1263.274	20	79159.4	36640 _{7/2} -115800° _{5/2}
1298.410	2	77017.3		1263.160	1	79166.5	
1298.139	10 h	77033.4		1261.871	20	79247.4	$39024_{\ 9/2} -118271^{\circ}_{\ 11/2}$
1297.828	3	77051.8	$38448_{\ 9/2}\ -115499^{\circ}_{\ 9/2}$	1260.991	20	79302.7	
1295.473	30	77191.9	$36642_{13/2}$ – $113833^{\circ}_{15/2}$	1259.747	4	79381.0	36640 _{7/2} -116021° _{7/2}
1294.860	2	77228.4	Comment of the control of the contro	1258.859	4 <i>h</i>	79437.0	

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

$\overset{\boldsymbol{\lambda_{vac}}}{\mathbf{A}}$	Intensity	$\sigma \ (\mathrm{cm}^{-1})$	Classification ^a	$egin{array}{c} \lambda_{ m yac} \ A \end{array}$	Intensity	σ (cm^{-1})	Classification ^a
1258.754	1	79443.6		1917 644	40	09195 0	
1258.700	2	79447.0	24357° _{11/2} —103805 _{13/2}	1217.644	40	82125.8	20505 119642°
1257.936	1	79495.3	$35828_{9/2} -115324^{\circ}_{9/2}$	1217.473	3	82137.3	30505 _{11/2} —112643° _{11/2}
1257.835	10h	79501.7	33626 9/2 -113324 9/2	1217.169	4	82157.9	$29835_{9/2} -111993^{\circ}_{9/2}$
1256.362	20	79594.9	$12846_{9/2} - 92441^{\circ}_{7/2}$	1217.063 1215.996	$\frac{1}{2}$	82165.0 82237.1	36642 _{13/2} —118879° _{11/2}
1255.468	1	79651.6	$38549_{1/2} - 118201^{\circ}_{3/2}$	1214.562	1	82334.2	
1255.162	3	79671.0	$35828_{9/2} - 115499^{\circ}_{9/2}$	1212.271	i	82489.8	$35828_{9/2} - 118318^{\circ}_{7/2}$
1254.915	5	79686.7	0,2	1212.053	2	82504.6	33323 9/2 113313 1/2
1252.937	7	79812.5	36640 _{7/2} -116453° _{9/2}	1211.998	1	82508.4	$39024_{9/2} - 121532^{\circ}_{11/2}$
			$48401_{3/2} - 128214^{\circ}_{3/2}$	1211.894	60	82515.5	3/2 11/2
1250.337	20	79978.4		12]1.111	3	82568.8	
1250.190	10	79987.8		1210.532	3	82608.3	
1249.025	3	80062.4	$23245^{\circ}_{5/2}$ $-103308_{7/2}$	1210.158	4	82633.8	
1246.860	5h	80201.5		1210.078	20	82639.3	
1245.521	5	80287.7	14859 _{11/2} — 95147° _{9/2}	1209.191	2	82699.9	
1244.669	2	80342.6	37197 _{3/2} -117540° _{3/2}	1208.938	2 h	82717.2	
1242.667	1	80472.1		1208.755	2	82729.8	27604 _{9/2} -110333° _{7/2}
1241.027	5h	80578.4					$38701_{13/2}$ – $121431^{\circ}_{13/2}$
1239.467	7	80679.8	24886° _{7/2} —105566 _{9/2}	1208.272	2	82762.8	$45805_{9/2} - 128568^{\circ}_{9/2}$
1238.007	4	80775.0	$35024_{7/2} - 115800^{\circ}_{5/2}$	1208.013	40 b l	82780.6	
1237.976	2	80777.0	,	1205.675	2 h	82941.1	
1236.596	1	80867.2		1205.511	20 h	82952.4	
1235.607	20 h	80931.9		1204.999	20 b l	82987.6	
1235.369	1	80947.5	26650 1176470	1204.511	4 h	83021.2	25020 1100508
1234.649	.1	80994.7	$36652_{5/2} - 117647^{\circ}_{7/2}$	1204.078	50	83051.1	$35828_{\ 9/2}\ -118879^{\circ}_{\ 11/2}$
1234.534	3	81002.2		1204.000	4	83056.5	$35024_{7/2} - 118081^{\circ}_{9/2}$
1234.351	1	81014.2		1203.946	2h	83060.2	
1234.150	3	81027.4		1203.448	2	83094.6	$30505_{11/2}-113600^{\circ}_{13/2}$
1233.869	3	81045.9	$29835_{9/2} - 110881^{\circ}_{11/2}$	1203.266	1	83107.1	
			36640 _{7/2} -117686° _{5/2}	1203.106	10 h	83118.2	
1233.573	1	81065.3	29267 _{5/2} —110333° _{7/2}	1203.054	2 h	83121.8	
1233.242	1	81087.1	29835 _{9/2} —110922° _{9/2}	1202.997	1	83125.7	
1231.958	1	81171.6		1202.889	1	83133.2	
1229.989	3h	81301.5		1202.515	2	83159.0	
1229.728	20	81318.8		1202.463	5 b l	83162.6	
1228.610	10 c l	81392.8	39725 _{15/2} —1211119° _{15/2}	1202.389	4	83167.8	25391° _{13/2} —108559 _{11/2}
1228.067	2	81428.8	35024 _{7/2} -116453° _{9/2}	1201.999	1	83194.8	27138 _{7/2} -110333° _{7/2}
1224.015	5	81698.3	39732 _{11/2} —121431° _{13/2}	1200.879	1	83272.3	28720 _{9/2} -111993° _{9/2}
1223.251	1	81749.4		1200.565	3	83294.1	$35024_{7/2} - 118318^{\circ}_{7/2}$
1223.055	1	81762.5		1200.254	5	83315.7	
1222.497	10	81799.8	39732 _{11/2} —121532° _{11/2}	1200.203	5 b l	83319.2	20005
1222.214	2	81818.7	$35828_{9/2} - 117647^{\circ}_{7/2}$	1200.140	8	83323.6	$29835_{9/2} -113158^{\circ}_{9/2}$
1222.173	1	81821.5	36670 110610°	1200.067	5 h	83328.7	
1220.398 1220.279	1 4	81940.5 81948.5	$36670_{\ 11/2}-118610^{\circ}_{\ 13/2}$	1198.482 1198.399	$\frac{2h}{40}$	83438.9 83444.7	35024 _{7/2} -118468° _{9/2}
1219.975	2	81968.9	36642—119610°				0,2
1219.500	1	82000.8	36642 _{13/2} —118610° _{13/2}	1197.869	3	83481.6	
			29267 _{5/2} -111268° _{3/2}	1197.651	2	83496.8	25000 1100018
	20	82[12[1.5	35024 11 /0/1/1				
1219.208 1218.533	20 2	82020.5 82065.9	$35024_{7/2} - 117044^{\circ}_{7/2}$	1197.589 1197.505	50 30	83501.1 83507.0	$\begin{array}{c} 27380_{\ 11/2}110881^{\circ}_{\ 11/2} \\ 29263_{\ 13/2}112769^{\circ}_{\ 13/2} \end{array}$

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\lambda_{\mathrm{vac}}}{A}$	Intensity	σ (cm ⁻¹)	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{{\mathrm{A}}}$	Intensity	σ (cm^{-1})	Classification ^a
1196.893	10	83549.7	$44903_{\ 5/2}-128453^{\circ}_{\ 7/2}$	1161.532	7	86093.2	$24788_{\ 9/2}\ -110881^{\circ}_{\ 11/2}$
1196.513	1	83576.2	77703 5/2 120433 7/2	1161.460	8	86098.5	$29835_{9/2} - 115933^{\circ}_{11/2}$
1195.692	4	83633.6	$29263_{13/2} - 112896^{\circ}_{15/2}$	1160.892	2	86140.7	29263 _{13/2} —115403° _{11/2}
1194.310	20	83730.4	$27380_{11/2}^{13/2} - 1111110^{\circ}_{13/2}$	1160.821	3	86145.9	$29263_{13/2}$ $-115408^{\circ}_{13/2}$ $29263_{13/2}$ $-115408^{\circ}_{13/2}$
1192.794	3	83836.8	21000 11/2 111110 13/2	1160.321	10	86153.6	$27138_{7/2} -113291^{\circ}_{7/2}$
1192.472	1	83859.4		1160.409	4	86176.5	27604 _{9/2} -113780° _{9/2}
1192.047	15	83889.3	$44679_{7/2} - 128568^{\circ}_{9/2}$	1159.818	20	86220.4	$27380_{11/2} - 113600^{\circ}_{13/3}$
1191.806	100	83906.3		1159.497	10	86244.3	
1190.132	10	84024.3	$29267_{5/2} - 113291^{\circ}_{7/2}$	1158.871	1	86290.9	5.7.7.4
1190.043	100	84030.6		1158.222	5 h	86339.2	
1189.183	20	84091.3	÷ .	1157.964	2	86358.5	$35024_{7/2}$ $-121382^{\circ}_{9/2}$
1188.622	3	84131.0		1157.912	40	86362.3	
1187.589	15	84204.2	$27138_{7/2} - 111342^{\circ}_{7/2}$	1157.279	20	86409.6	29263 _{13/2} —115672° _{15/5}
1187.470	4	84212.6	,	1156.410	15	86474.5	$29835_{9/2} - 116309^{\circ}_{11/2}$
1187.418	1	84216.3		1155.871	3	86514.8	
1187.176	2	84233.5		1155.747	40	86524.1	
1185.662	1	84341.1		1155.635	2	86532.5	$29267_{5/2} - 115800^{\circ}_{5/2}$
1185.135	2	84378.6		1154.705	1	86602.2	
1184.806	1	84402.0		1154.526	1	86615.6	
1183.796	1	84474.0		1154.091	1	86648.3	
1183.751	1	84477.2	$36642_{\ 13/2} - 121119^{\circ}_{\ 15/2}$	1153.796	5	86670.4	29263 _{13/2} —115933° _{11/}
1183.029	1	84528.8		1152.347	10	86779.4	$28720_{\ 9/2}\ -115499^{\circ}_{\ 9/2}$
1182.794	20	84545.6	$31254_{7/2} - 115800^{\circ}_{5/2}$	1151.922	2	86811.4	
1182.655	15	84555.5		1151.863	3	86815.9	
1182.425	6 h	84572.0		1151.718	5	86826.8	$31254_{7/2} - 118081^{\circ}_{9/2}$
1182.002	3 h	84602.2		1151.530	10	86841.0	
1181.852	2	84612.	$27380_{\ 11/2}$ — $111993^{\circ}_{\ 9/2}$	1151.474	10	86845.2	$26446_{7/2} - 113291^{\circ}_{7/2}$
1181.804	1	84616.4		1150.956	2	86884.3	$14187^{\circ}_{5/2}$ $-101071_{5/2}$
1180.016	80	84744.6		1150.518	20	86917.4	$25979_{15/2}$ — $112896^{\circ}_{15/2}$
1179.786	4	84761.1		1149.956	30	86959.8	$24309_{3/2} - 111268^{\circ}_{3/2}$
1179.739	4	84764.5		1149.740	20	86976.2	$29263_{13/2}$ – $116238^{\circ}_{15/2}$
1178.552	3	84849.9		1149.180	5	87018.6	$24250_{3/2} - 111268^{\circ}_{3/2}$
1178.140	40	84879.6	20004 1100050	1148.979	10	87033.8	$24461_{\ 5/2}\ -111494^{\circ}_{\ 5/2}$
1178.012 1177.911	5 5 <i>c l</i>	84888.8 84896.1	$28936_{3/2} - 113825^{\circ}_{3/2} \ 26446_{7/2} - 111342^{\circ}_{7/2}$	1148.836 1148.493	$\frac{100}{20h}$	87044.6 87070.6	
1177 006	20 - 1	04907.0	20505 115402°	1140 126	-	07007.7	
1177.886	$\begin{bmatrix} 20 \ c \ l \end{bmatrix}$	84897.9 84994.4	$30505_{11/2}$ — $115403^{\circ}_{11/2}$ $30505_{11/2}$ — $115499^{\circ}_{9/2}$	1148.136	5	87097.7	94700 111002°
1176.548				1146.717	1	87205.5	$24788_{9/2} -111993^{\circ}_{9/2}$
1175.638	10	85060.2	$28720_{\ 9/2} -113780^{\circ}_{\ 9/2}$	1146.659	1	87209.9	$29835_{9/2} -117044^{\circ}_{7/2}$
1175.458	$\frac{1}{1}$	85073.2		1146.600	1	87214.4	$31254_{7/2} - 118468^{\circ}_{9/2}$
1175.410	1	85076.7		1146.346	4	87233.7	23647 _{13/2} —110881° _{11/}
1175.191	10	85092.6		1146.060	1	87255.5	16089° _{13/2} —103344 _{11/}
1172.829	30	85263.9		1145.869	4	87270.0	30505 _{11/2} —117775° _{13/}
1171.087	4	85390.8		1145.456	10	87301.5	$28720_{\ 9/2}\ -116021^{\circ}_{\ 7/2}$
1170.564 1169.104	10 10	85428.9 85535.6		1145.216 1144.726	1 10	87319.8 87357.2	$25934_{\ 5/2}\ -113291^{\circ}_{\ 7/2}$
1166.804	10	85704.2	35828 _{9/2} -121532° _{11/2}	1144 000	1	97411 0	
1165.446	3	85804.1	$30505_{11/2}^{9/2} - 121332_{11/2}^{11/2}$ $30505_{11/2} - 116309^{\circ}_{11/2}$	1144.009	1 1	87411.9	27290 114707°
1163.446	1	85862.0	$24470_{7/2} - 110333^{\circ}_{7/2}$	1143.937	4	87417.4	$27380_{11/2}$ — $114797^{\circ}_{13/2}$
1104.009		The transfer of the second sec	24410 7/2 -110333 7/2	1143.836	2	87425.1	
1163.805	4	85925.0		1143.342	50	87462.9	$23647_{13/2}$ $-1111110^{\circ}_{13/2}$

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\mathop{A}\limits_{\mathbf{A}}^{\mathbf{vac}}$	Intensity	$\sigma \atop (cm^{-1})$	Classification ^a	A yac	Intensity	σ (cm ⁻¹)	Classification ^a
1143.020	2	87487.5	29835 _{9/2} -117323° _{11/2}	1130.153	3	88483.6	
1142.900	20	87496.7	2 3 3 3 7 2 2 2 3 3 3 1 7 2	1129.886	3	88504.5	25409 _{7/2} -113914° _{5/}
1142.788	10	87505.3	$26095_{11/2} - 113600^{\circ}_{13/2}$	1129.785	10	88512.4	29263 _{13/2} —117775° ₁₃
	20	87512.8	20070 11/2 110000 13/2		1	88569.7	27452 _{5/2} -116021° _{7/}
1142.690				1129.054			
142.012	20	87564.8	· v	1128.731	1	88595.1	22747 _{9/2} —111342° _{7/}
1141.868	2	87575.8	30505 _{11/2} —118081° _{9/2}	1127.367	40	88702.3	26095 _{11/2} —114797° ₁₃
1141.795	20	87581.4		1127.107	4	88722.7	21611 _{5/2} -110333° ₇
1141.697	40	87588.9	$28720_{9/2} - 116309^{\circ}_{11/2}$	1127.030	2	88728.8	39485 _{1/2} -128214° ₃
1141.465	4	87606.7		1126.802	5	88746.7	25033 _{9/2} -113780° ₉
1141.419	1	87610.2		1126.623	2	88760.8	
1141.262	3	87622.3	25934 _{5/2} -113556° _{5/2}	1196 999	3	88787.7	
	2		23934 5/2 113330 5/2	1126.282		88799.8	29263 _{13/2} —118063° ₁
1141.157	1	87630.4	99647 111995°	1126.128	300 h		22527 _{7/2} -111342° ₇
1140.413	200	87687.5	23647 _{13/2} —111335° _{15/2}	1125.935	4	88815.1	
1140.174	30	87705.9	23175 _{13/2} —110881° _{11/2}	1125.895	5	88818.2	25979 _{15/2} —114797° ₁
1139.821	10	87733.1	28720 _{9/2} —116453° _{9/2}	1125.725	20	88831.6	
1139.688	10	87743.3		1125.596	20	88841.8	22080 _{7/2} -110922°s
1139.245	1	87777.4	$29267_{5/2} - 117044^{\circ}_{7/2}$	1125.442	5	88854.0	28720 _{9/2} -117574°
1139.090	3	87789.4		1125.355	1	88860.8	
1138.958	3	87799.6	$27604_{9/2} - 115403^{\circ}_{11/2}$	1124.668	30	88915.1	21418 _{5/2} -110333° ₂
1138.822	2	87810.0	$23532_{5/2} -111342^{\circ}_{7/2}$	1124.366	1	88939.0	0,2
1138.712	80	87818.5		1124.014	1	88966.9	22527 _{7/2} -111494°
1138.231	2	87855. 6	24788 9/2 -112643° _{11/2}	1123.920	15	88974.3	26446 _{7/2} -115420°
			1,0		1	88991.1	.,-
1137.886	30	87882.3	$25409_{7/2} - 113291^{\circ}_{7/2}$	1123.708			22277 _{3/2} -111268°
1137.809 1137.714	50 100	87888.2 87895.6	27604 _{9/2} -115499° _{9/2}	1123.647 1123.103	3 2	88995.9 89039.0	21294 _{7/2} -110333°
1101.111	100	0.050.0	21001 9/2 110199 9/2	1120:100		0,00,00	21231 1/2 110000 1
1137.197	20	87935.5	23175 _{13/2} —1111110° _{13/2}	1123.041	1	89043.9	29835 _{9/2} -118879°
1136.852	3	87962.2	$23532_{5/2} - 111494^{\circ}_{5/2}$	1122.803	3	89062.8	
1136.709	50	87973.3		1122.386	7	89095.9	24461 _{5/2} -113556°
1136.628	8	87979.5	$25934_{5/2} - 113914^{\circ}_{5/2}$	1122.005	40	89126.2	
1136.551	1	87985.5	29263 _{13/2} —117248° _{13/2}	1121.452	3	89170.1	
1136.484	4	87990.7	17642° _{15/2} —105632 _{13/2}	1121.115	5	89196.9	
	4		17042 15/2—103032 13/2		3		26095 _{11/2} —115324°
1135.927	20	88033.8	17400° 105450	1120.707		89229.4	20093 11/2-113324
1135.835	1	88041.0	17409° _{11/2} —105450 _{11/2}	1120.577	2	89239.7	22647 1120069
1135.654	1	88055.0		1120.463	1	89248.8	23647 13/2-112896
1135.268	10	88084.9		1120.300	4	89261.8	22080 _{7/2} -111342°
1135.004	300	88105.4	30505 _{11/2} —118610° _{13/2}	1120.257	1	89265.2	28936 _{3/2} -118201°
1134.751	8	88125.1	25033 _{9/2} -113158° _{9/2}	1119.698	2	89309.8	24470 _{7/2} -113780°
1134.462	4	88147.5	$25409_{7/2} - 113556^{\circ}_{5/2}$	1119.636	30	89314.7	23844 9/2 -113158
1134.298	50	88160.2	23175 _{13/2} —111335° _{15/2}	1117.000		0,011	27138 _{7/2} -116453°
1133.483	30	88223.6	20110 13/2 111000 15/2	1119.555	1	89321.2	2.100 1/2 110100
1100 050	20	00010.7		1110 450	10	00000	00440 330550
1133.272	20	88240.1	2024	1119.470	10	89328.0	23442 11/2-112769
1132.851	40	88272.9	$29267_{5/2} - 117540^{\circ}_{3/2}$	1119.241	40	89346.3	21535 9/2 -110881
1131.973	1	88341.3	23651 _{7/2} -111993° _{9/2}	1119.153	40	89353.3	26446 _{7/2} -115800°
1131.719	2	88361.2	27138 _{7/2} -115499° _{9/2}	1119.054	100 h	89361.2	21505
1131.558	10	88373.7	30505 _{11/2} —118879° _{11/2}	1118.723	4	89387.6	21535 _{9/2} -110922°
1131.283	8	88395.2	22527 _{7/2} -110922° _{9/2}	1118.508	30	89404.8	26095 11/2-115499
1130.988	15	88418.3	29267 _{5/2} -117686° _{5/2}	1118.395	15	89413.8	$22080_{7/2} - 111494^{\circ}$
1130.753	2	88436.6	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1118.027	8	89443.3	24470 _{7/2} -113914°
1130.654	1	88444.4		1117.977	20	89447.3	23844 9/2 -113291
	3	and the second second second	$23050_{3/2} - 111494^{\circ}_{5/2}$	1117.904	5		24461 _{5/2} -113914
1130.363	J 3	88467.2		1117,904	J	89453.1	2 Troi 5/2 -113914

^a For doubly-classified lines, the wavelength is entered only once.

TABLE X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\boldsymbol{\lambda_{\mathrm{vac}}}}{\boldsymbol{\Lambda}}$	Intensity	σ (cm ⁻¹)	Classification a	$\overset{\lambda_{\mathrm{vac}}}{{\mathrm{A}}}$	Intensity	σ (cm^{-1})	Classification ^a
1117.803	10	89461.2		1107.998	40	90252.9	
1117.500	6	89485.5	$20848_{5/2} - 110333^{\circ}_{7/2} \ 25934_{5/2} - 115420^{\circ}_{7/2}$	1107.911	80	90260.0	25979 _{15/2} —116238° ₁₅ 25409 _{7/2} —115670° _{7/}
1117.230	3	89507.1	$23651_{7/2} -113158^{\circ}_{9/2}$	1107.881	20 c l	90262.4	23651 _{7/2} -113914° ₅
1116.681	30	89551.1	$28720_{9/2}^{-1} -118271^{\circ}_{11/2}^{-1}$	1107.536	100	90290.5	25033 _{9/2} -115324° _{9/2}
1116.516	3	89564.3		1107.096	20	90326.4	
1116.382	30	89575.1	$24250_{3/2} - 113825^{\circ}_{3/2} \ 26446_{7/2} - 116021^{\circ}_{7/2}$	1106.948 1106.755	$\begin{vmatrix} 2\\3 \end{vmatrix}$	90338.5 90354.2	23442 _{11/2} —113780° ₉
1116 264	3	89584.5	20440 7/2 110021 7/2	1106.753	80	90369.6	25033 _{9/2} -115403° ₁
1116.264 1116.139	50	89594.6	23175 _{13/2} —112769° _{13/2}	1106.423	20	90381.4	23532 _{5/2} -113914° ₅
1115 705	15	90697.9	21204 —110022°	1106 241	10 c l	90388.0	
1115.725	15	89627.8	$21294_{7/2} - 110922^{\circ}_{9/2}$	1106.341 1106.311	30	90390.5	25409 _{7/2} -115800° ₅
1115.571	30	89640.2	23651 _{7/2} -113291° _{7/2}		3	90395.3	27380 _{11/2} —117775° ₁
1115.429	10	89651.6	91611 111960°	1106.252	4	90393.3	22747 _{9/2} —113158°s
115.353 114.912	60	89657.7 89693.2	$\begin{array}{c} 21611_{\ 5/2} - 111268^{\circ}_{\ 3/2} \\ 25979_{\ 15/2} - 115672^{\circ}_{\ 15/2} \end{array}$	1106.060 1105.962	200	90411.0	22141 9/2 -113130
1114 501	20	90710.9	,	1105 754	6	90436.0	
1114.581	30	89719.8	21611 _{5/2} -111342° _{7/2}	1105.754	$\begin{vmatrix} 6\\2 \end{vmatrix}$	90457.5	21535 _{9/2} -111993°s
1114.436	1	89731.5	$21011_{5/2} - 111342_{7/2} 28720_{9/2} - 118468^{\circ}_{9/2}$	1105.492		90466.1	$25033_{9/2} -111993_{9/2}$ $25033_{9/2} -115499_{9/2}^{\circ}$
1114.228	20	89748.2		1105.386	80	90480.2	25055 9/2 115455
1113.753 1113.489	10	89786.5 89807.8	$23844_{\ 9/2} -113630^{\circ}_{\ 7/2} \ 21535_{\ 9/2} -111342^{\circ}_{\ 7/2}$	1105.214 1104.843	20 2000	90510.6	25979 _{15/2} —116489°
1110.065	10	90950 1	91410111960°	1104 791	10	90520.6	
1112.965	10	89850.1	$21418_{\ 5/2}\ -111268^{\circ}_{\ 3/2}$	1104.721 1104.525	10 40	90536.7	24788 _{9/2} -115324°
1112.582	10	89881.0	21611111404°		4	90547.8	27138 _{7/2} -117686°
1112.549	5	89883.7	$21611_{5/2} - 111494^{\circ}_{5/2}$	1104.389		90565.5	20315 _{9/2} -110881°
1112.400 1112.268	$\begin{vmatrix} 1\\30 \end{vmatrix}$	89895.7 89906.4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1104.173 1103.780	$\begin{vmatrix} 2\\20 \end{vmatrix}$	90597.8	26446 _{7/2} -117044°
1110 160	10	90015.0	25409 _{7/2} -115324° _{9/2}	1103.660	40	90607.6	
1112.162	10	89915.0		1103.605	10	90612.1	25409 _{7/2} -116021°
1112.050	5	89924.0	$21418_{5/2} - 111342^{\circ}_{7/2}$	1103.553	20 h	90616.4	20107 7/2 110021
1111.902	10	89936.0	$23844_{9/2} - 113780^{\circ}_{9/2}$	1103.354	5	90632.7	24788 _{9/2} -115420°
1111.768 1111.694	100	89946.8 89952.8	23647 _{13/2} —113600° _{13/2}	1103.334	8	90646.6	20848 _{5/2} -111494°
1111 520	20	89965.4		1103.150	15	90649.5	37919 7/2 -128568
1111.539	10	89970.5	$27604_{\ 9/2} - 117574^{\circ}_{\ 11/2}$	1103.130	400	90659.0	23175 _{13/2} —113833°
1111.475	3	89978.8		1102.938	1	90666.9	27604 _{9/2} -118271°
1111.373	50	89994.9	$23651_{7/2} -113630^{\circ}_{7/2} \ 28885_{9/2} -118879^{\circ}_{11/2}$	1102.556	20	90698.3	$21294_{7/2} -111993^{\circ}$
1111.174 1111.117	1	89999.5	20003 9/2 11007 9 11/2	1102.392	200	90711.8	24788 _{9/2} —115499°
1111 025	1	90006.2	26446 _{7/2} -116453° _{9/2}	1101.939	20	90749.1	27452 5/2 -118201
1111.035 1110.898	1	90017.3	$20315_{9/2} -110333^{\circ}_{7/2}$	1101.757	100	90764.1	22527 _{7/2} -113291
	1	90036.9	20313 9/2 110333 7/2	1101.660	1 1	90772.1	22321 7/2 113271
1110.656 1110.520	200	90047.9	$21294_{7/2} - 111342^{\circ}_{7/2}$	1101.542	1	90781.8	
1110.320	30	90076.1	$21418_{5/2} -111494^{\circ}_{5/2}$	1101.542	40	90853.5	24470 7/2 -115324
1110 000	1.	90083.4		1100.546	1	90864.0	23050 3/2 -113914
1110.082	1 5			1100.540	1	90004.0	
1109.801	5 15	90106.2 90128.8	$23651_{7/2} - 113780^{\circ}_{9/2}$	1100 515	9	00966-6	27604 _{9/2} -118468° 27452 _{5/2} -118318°
1109.523				1100.515	2	90866.6	
1109.156 1109.011	200	90158.6 90170.4	28720 _{9/2} —118879° _{11/2}	1100.389 1099.894	4 4	90877.0 90917.8	30505 11/2-121382
1100 070	10	00191.9		1000 002	200	00025 4	30505 101401
1108.879	10	90181.2	22647 1120220	1099.803	200	90925.4	30505 11/2-121431
1108.817	500	90186.2	23647 _{13/2} —113833° _{15/2}	1099.596	4	90942.5	27138 7/2 -118081
1108.709	20	90195.0 90200.0	$27452_{5/2} - 117647^{\circ}_{7/2} \ 21294_{7/2} - 111494^{\circ}_{5/2}$	1099.505 1099.389	20 7	90950.0 90959.6	24470 _{7/2} -115420 24461 _{5/2} -115420
1108.648							

 $^{^{\}rm a}$ For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\lambda_{vac}}{\mathring{A}}$	Intensity	σ (cm ⁻¹)	Classification ^a	λ _{vac} Å	Intensity	σ (cm ⁻¹)	Classification ^a
1098.981	3	90993.4		1091.293	2	91634.4	25409 _{7/2} -117044° _{7/2}
1098.735	1	91013.8	$21755_{11/2} - 112769^{\circ}_{13/2}$	1031.230	_	71001.1	26446 _{7/2} -118081° _{9/2}
1098.573	40	91027.2	$20315_{9/2} -111342^{\circ}_{7/2}$	1091.097	1	91650.9	20440 7/2 110001 9/2
1070.010	TO .	71021.2	$30505_{11/2}^{9/2} -121532^{\circ}_{11/2}$		2		$23844_{9/2} - 115499^{\circ}_{9/2}$
1098.506	4	91032.7	$22747_{9/2} -113780^{\circ}_{9/2}$	1091.047 1090.876	$\frac{2}{2}$	91655.1 91669.4	25044 9/2 -115499 9/2
				1050.010		21002.1	
1098.296	40	91050.1	$19872_{7/2}$ $-110922^{\circ}_{9/2}$	1090.839	2	91672.6	23651 _{7/2} -115324° _{9/2}
1098.243	20	91054.5		1090.739	5	91681.0	$21611_{5/2} - 113291^{\circ}_{7/2}$
1098.164	2	91061.1		1090.626	50	91690.5	
1097.967	1	91077.4	$22080_{7/2} - 113158^{\circ}_{9/2}$	1090.536	200	91698.0	29835 _{9/2} -121532° _{11/}
1097.595	100	91108.3	$20160_{3/2} - 111268^{\circ}_{3/2}$	1090.366	10	91712.3	25934 _{5/2} -117647° _{7/2}
1007 149	50	01145 4	24700 115022°				26640 1202528
1097.148	50	91145.4	24788 _{9/2} -115933° _{11/2}	1000 000	1.5	01.740.6	$36640_{7/2} - 128352^{\circ}_{9/2}$
1096.955	1 1	91161.4	10700 110001°	1090.006	15	91742.6	10060 1111108
1096.731	20	91180.1	19700 _{11/2} —110881° _{11/2}	1089.921	1	91749.8	19360 _{13/2} —1111110° _{13/}
1004 045	101	01010 0	27138 _{7/2} -118318° _{7/2}	1089.844	4	91756.2	$21535_{9/2} - 113291^{\circ}_{7/2}$
1096.367	10 <i>h</i>	91210.3	22080 _{7/2} —113291° _{7/2}	,			23647 _{13/2} —115403° _{11/2}
1096.121	100	91230.8	27380 _{11/2} —118610° _{13/2}	1089.571	20	91779.2	· · · · · · · · · · · · · · · · · · ·
1096.080	50 b l	91234.2	24788 _{9/2} -116021° _{7/2}	1089.464	15	91788.2	
1095.856	30	91252.9	$22527_{7/2} -113780^{\circ}_{9/2}$	1089.312	8	91801.1	19308 _{11/2} —1111110° _{13/}
1095.766	100	91260.4	$29835_{9/2} - 121095^{\circ}_{11/2}$	1009.512	0	91001.1	
1095.587	60	91275.3	$25033_{9/2} - 121093_{11/2}$ $25033_{9/2} - 116309^{\circ}_{11/2}$	1000 167	1	01012.2	36652 _{5/2} -128453° _{7/2}
1093.307		91273.3	25055 9/2 11050 7 11/2	1089.167	1	91813.3	$36640_{7/2} - 128453^{\circ}_{7/2}$
		,	$27604_{\ 9/2} - 118879^{\circ}_{\ 11/2}$	1088.933	30	91833.0	22080 _{7/2} -113914° _{5/2}
1095.513	30	91281.4		1088.879	3	91837.6	
1095.403	15	91290.6	₽	1088.659	500	91856.1	29263 _{13/2} —121119° _{15/}
1094.928	80	91330.2	27138 _{7/2} -118468° _{9/2}	1088.572	20	91863.5	$21294_{7/2} - 113158^{\circ}_{9/2}$
1094.878	30	91334.4	$20160_{3/2} - 111494^{\circ}_{5/2}$	1088.353	10	91881.9	23442 _{11/2} —115324° _{9/2}
1094.832	1	91338.2	24461 _{5/2} -115800° _{5/2}	1088.284	10	91887.8	23532 _{5/2} -115420° _{7/2}
1094.767	15	91343.6	$18990_{7/2} - 110333^{\circ}_{7/2}$	1088.125	70	91901.2	25552 5/2 115420 7/2
1094.637	1	91354.5	23442 _{11/2} —114797° _{13/2}				26640129569°
1094.486	30	91367.1	23772 11/2 11777 13/2	1087.804	100	91928.3	36640 _{7/2} -128568° _{9/2}
			22527 _{7/2} -113914° _{5/2}	1087.601	4	91945.5	$21611_{5/2} - 113556^{\circ}_{5/2}$
1094.255	80	91386.4	22321 7/2 -113914 5/2	1087.563	1	91948.7	
1094.058	3	91402.8	$21755_{11/2}$ – $113158^{\circ}_{9/2}$	1087.465	2	91957.0	
1093.870	10	91418.5		1087.418	2	91961.0	23442 _{11/2} —115403° ₁₁
1093.601	1	91441.0	$37011_{5/2} - 128453^{\circ}_{7/2}$	1087.362	1	91965.7	23442 _{11/2} —115408° ₁₃
1093.521	80	91447.7	0,2	1087.252	4	91974.0	19360 _{13/2} —111335° ₁₅
1093.253	80	91470.1	$19872_{7/2}$ $-111342^{\circ}_{7/2}$	1087.164	4	91982.4	24470 _{7/2} -116453° _{9/2}
1000 105	60	01455 0	22000 1105560	100= 000		03003.0	
1093.185	60	91475.8	$22080_{7/2} - 113556^{\circ}_{5/2}$	1087.063	1 1	91991.0	21224 31225
1092.910	20	91498.8	27380 _{11/2} —118879° _{11/2}	1086.993	5	91996.9	21294 _{7/2} —113291° _{7/2}
1092.529	2	91530.8	21238 $_{13/2}$ —112769 $^{\circ}_{13/2}$	1086.700	40	92021.7	26446 _{7/2} -118468° _{9/2}
1092.481	6	91534.8	$36683_{1/2} - 128214^{\circ}_{3/2}$	1086.598 1086.538	$\begin{vmatrix} 10 \\ 1 \end{vmatrix}$	92030.4 92035.4	
1092.401		91334.0		1060.556	1	92033.4	
1092.325	20 c l	91547.8	$22277_{3/2} - 113825^{\circ}_{3/2}$	1086.388	2	92048.1	
			29835 _{9/2} —121382° _{9/2}	1086.321	3	92053.8	18241 _{11/2} —110295° ₁₁
1092.301	20 c l	91549.9	$22080_{7/2} - 113630^{\circ}_{7/2}$	1086.280	2	92057.3	23442 _{11/2} —115499° _{9/5}
		1 11	$24250_{3/2} - 115800^{\circ}_{5/2}$	1085.915	40	92088.2	23844 _{9/2} -115933° ₁₁
1092.032	2	91572.4	$19308_{\ 11/2}\!\!-\!\!110881^{\circ}_{\ 11/2}$	1085.828	20	92095.6	21535 _{9/2} —113630° _{7/}
1091.983	3	91576.5	$23844_{9/2} - 115420^{\circ}_{7/2}$	1085.531	20	92120.8	19872 _{7/2} —111993° _{9/}
1091.676	1	91602.3	200 7 9/2 110 720 7/2				.,-
1091.575	30	91612.4		1085.435	1	92129.0	21535 _{9/2} -113664° ₁₁
1091.333	70			1085.380	1	92133.6	
1091.477	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	91619.0 91622.9		1085.283	2	92141.9	

 $[\]ensuremath{^{a}}\xspace$ For doubly-classified lines, the wavelength is entered only once.

TABLE X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\lambda_{\mathrm{vac}}}{{\mathrm{A}}}$	Intensity	$\sigma \atop (cm^{-1})$	Classification ^a	$\stackrel{\lambda_{ m vac}}{A}$	Intensity	σ (cm^{-1})	Classification ^a
9		001564		1070.010	10	02477.0	21140 110025°
1085.112	8	92156.4		1079.013	10	92677.3	$21148_{3/2} - 113825^{\circ}_{3/2}$
1084.976	15	92167.9	$29263_{13/2}$ $-121431^{\circ}_{13/2}$	1078.672	1	92706.6	$17627_{9/2} - 110333^{\circ}_{7/2}$
1084.873	10	92176.7	$23844_{\ 9/2} -116021^{\circ}_{\ 7/2}$	1078.516	2	92720.0	
	~		$26095_{11/2}$ $-118271^{\circ}_{11/2}$	1077.972	2	92766.8	
1084.417	500	92215.4	$41026_{17/2}$ — $133242^{\circ}_{19/2}$	1077.851	1	92777.2	
1084.262	8 <i>b l</i>	92228.6	23175 _{13/2} —115403° _{11/2}	1077.782	40	92783.1	
1084.204	7	92233.6	$23175_{13/2} - 115408^{\circ}_{13/2}$	1077.742	4	92786.6	$24788_{9/2} - 117574^{\circ}_{11/2}$
1084.157	20	92237.6	$25409_{7/2} - 117647^{\circ}_{7/2}$	1077.623	2	92796.8	$22527_{7/2} - 115324^{\circ}_{9/2}$
1084.071	1	92244.9	$21535_{9/2} - 113780^{\circ}_{9/2}$	1077.571	30	92801.3	$23651_{7/2} - 116453^{\circ}_{9/2}$
1083.936	20	92256.4	$24470_{7/2}^{\circ} -116727^{\circ}_{5/2}$	1077.451	10	92811.6	$28720_{9/2} - 121532^{\circ}_{11/2}$
			$24788_{\ 9/2} -117044^{\circ}_{\ 7/2}$	1077.382	20	92817.6	$18063_{\ 9/2} - 110881^{\circ}_{\ 11/2}$
1083.876	40	92261.5	$21294_{7/2} - 113556^{\circ}_{5/2}$	1076.902	40	92856.0	$18063_{~9/2}$ $-110922^{\circ}_{~9/2}$
1083.815	10	92266.7	$23532_{5/2} - 115800^{\circ}_{5/2}$				$24788_{\ 9/2} -117647^{\circ}_{\ 7/2}$
*			$25934_{\ 5/2} -118201^{\circ}_{\ 3/2}$	1076.831	3	92865.1	
1083.747	20	92272.4		1076.790	10	92868.6	$18241_{\ 11/2}$ — $1111110^{\circ}_{\ 13/2}$
1083.697	2	92276.7	$25409_{\ 7/2}\ -117686^{\circ}_{\ 5/2}$	1076.708	2	92875.7	
1083.548	5	92289.4	$18241_{11/2} - 110530^{\circ}_{13/2}$	1076.325	30	92908.7	$25409_{7/2} - 118318^{\circ}_{7/2}$
			$25033_{\ 9/2} -117323^{\circ}_{\ 11/2}$	1076.137	5	92925.0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
1083.393	10	92302.6	$21611_{5/2}^{5/2} - 113914_{5/2}^{\circ}$	1075.961	100	92940.2	
1083.348	20	92306.4	0,2	1075.707	2	92962.1	
1083.285	1	92311.8		1075.586	10 c l	92972.6	22527 _{7/2} -115499° _{9/2}
1083.001	10	92336.0	$21294_{7/2} - 113630^{\circ}_{7/2}$	1075.565	50 c l	92974.4	22021 7/2 110155 9/2
1082.881	40	92346.2	$41026_{17/2}$ $-133373^{\circ}_{17/2}$	1075.532	10 c l	92977.2	$20848_{5/2} - 113825^{\circ}_{3/2}$
1082.824	8	92351.1	11020 17/2 100010 17/2	1075.448	1	92984.5	200 10 5/2 110020 3/2
1082.704	50	92361.4	$21238_{\ 13/2}\!\!-\!\!113600^{\circ}_{\ 13/2}$	1075.147	1	93010.5	23442 _{11/2} —116453° _{9/2}
1082.445	8	92383.4	$25934_{\ 5/2}\ -118318^{\circ}_{\ 7/2}$	1074.855	100	02025 0	
1082.443	20				100	93035.8	95033 110001° -
		92413.7	18921 _{15/2} —111335° _{15/2}	1074.726	5	93047.0	$25033_{9/2} - 118081^{\circ}_{9/2}$
1082.045	10	92417.6	$24309_{3/2} - 116727^{\circ}_{5/2}$	1074.669	40	93051.9	25400 1104600
1081.807	3	92437.9	20040 112901°	1074.590	7	93058.8	$25409_{7/2} - 118468^{\circ}_{9/2}$
1081.746	10	92443.1	$20848_{\ 5/2}\ -113291^{\circ}_{\ 7/2}$	1074.515	100	93065.2	$20848_{5/2} - 113914^{\circ}_{5/2}$
1081.574	3	92457.8	-	1074.474	5	93068.8	$19700_{11/2} - 112769^{\circ}_{13/2}$
1081.356	20	92476.5	$24250_{\ 3/2} -116727^{\circ}_{\ 5/2}$	1074.353	7	93079.3	$24461_{5/2} -117540^{\circ}_{3/2}$
1081.252	5	92485.4	$21294_{7/2} - 113780^{\circ}_{9/2}$	1074.171	5	93095.0	3/2 11/0/0 3/2
1081.210	5	92489.0	$23532_{5/2}^{5/2} -116021_{7/2}^{\circ}$	1074.041	5	93106.3	
1080.898	100	92515.7	26095 _{11/2} —118610° _{13/2}	1073.901	200	93118.4	27380 _{11/2} —120498° _{13/2}
1080.797	6	92524.3	35828 —128352°	1073.801	1	93127.1	, and the second
1000 550		00545.0	$35828_{~9/2}$ $-128352^{\circ}_{~9/2}$	1000 663	100		
1080.553	300	92545.2	25020 120201°	1073.661	100	93139.3	
1080.459		92553.3	$35828_{9/2} - 128381^{\circ}_{11/2}$	1073.340	20	93167.1	
1080.187	50	92576.6	22747 _{9/2} -115324° _{9/2}	1073.308	3	93169.9	99747 115099°
1080.110	20	92583.2	$24461_{\ 5/2}\ -117044^{\circ}_{\ 7/2}$	1073.126	200	93185.7	22747 _{9/2} -115933° _{11/2}
1080.019	2	92591.0		1072.600	30	93231.4	24309 _{3/2} -117540° _{3/2}
1079.947	3	92597.1		1072.529	100	93237.6	$25033_{9/2} - 118271^{\circ}_{11/2}$
1079.921	10	92599.4		1072.466	20	93243.0	$22080_{7/2} - 115324^{\circ}_{9/2}$
1079.727	10	92616.0		1072.425	5	93246.6	$19649_{17/2}$ – $112896^{\circ}_{15/2}$
1079.698	10	92618.5		1072.342	20	93253.8	$17627_{\ 9/2}\ -110881^{\circ}_{\ 11/2}$
1079.452	100	92639.6	18241 _{11/2} —110881° _{11/2}	1072.237	8	93263.0	
1079.268	60	92655.4	$22747_{9/2} - 115403^{\circ}_{11/2}$	1072.108	50 c l	93274.2	$22747_{9/2} - 116021^{\circ}_{7/2}$
1079.204	1	92660.9	23647 _{13/2} —116309° _{11/2}	1072.076	10 c l	93277.0	$35291_{9/2}^{9/2} -128568_{9/2}^{\circ}$
1079.078	50 c l	92671.7	$25409_{7/2} - 118081^{\circ}_{9/2}$	1072.009	100	93282.8	5/2 120000 9/2
1079.058	50 c l	92673.4	$22747_{9/2} -115420^{\circ}_{7/2}$	1071.968	10	93286.4	$19872_{7/2} - 113158^{\circ}_{9/2}$
	-300		22.1. 9/2 110 120 7/2	1011.700	10	70200.T	170.2 7/2 110100 9/2

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

$egin{array}{c} \lambda_{ m vac} \ A \end{array}$	Intensity	σ (cm^{-1})	Classification ^a	Å Å	Intensity	σ (cm^{-1})	Classification ^a
1071.865	200	93295.3	17627 _{9/2} -110922° _{9/2}	1065.331	40	93867.5	21535 _{9/2} -115403° _{11/2} ×
1071.487	100	93328.2	$35024_{7/2} - 128352^{\circ}_{9/2}$	1065.224	2	93877.0	21000 9/2 110 100 11/2
1071.422	300	93333.9	$19308_{11/2}$ $-112643^{\circ}_{11/2}$	1065.128	20	93885.4	$21535_{9/2} - 115420^{\circ}_{7/2}$
1071.334	50	93341.6	17000 11/2 112010 11/2	1064.971	40	93899.3	19700 _{11/2} —113600° _{13/2}
1071.213	100	93352.1		1064.874	10	93907.8	$19872_{7/2} -113780^{\circ}_{9/2}$
1070.750	3	93392.5	23651 _{7/2} -117044° _{7/2}	1064.795	50	93914.8	
1070.617	7	93404.1	1,2	1064.640	20 c l	93928.5	$27604_{9/2} - 121532^{\circ}_{11/2}$
1070.554	80	93409.6	$19360_{\ 13/2}$ – $112769^{\circ}_{\ 13/2}$	1064.585	100	93933.3	$34520_{5/2} - 128453^{\circ}_{7/2} \ \ \times$
1070.461	60	93417.7	$17113_{13/2} - 110530^{\circ}_{13/2}$	1064.499	40	93940.9	$22080_{7/2} - 116021^{\circ}_{7/2}$
1070.336	10	93428.6	$35024_{~7/2}~-28453^{\circ}_{~7/2}$	1064.390	100	93950.5	24250 _{3/2} -118201° _{3/2}
1070.246	100	93436.5		1064.289	50	93959.4	
1069.881	500	93468.3	$39725_{15/2}$ – $133194^{\circ}_{17/2}$	1064.127	10 c l	93973.7	
1069.768	20	93478.2	$23844_{9/2} - 117323^{\circ}_{11/2}$	1064.102	5 c l	93976.0	
1069.710	40	93483.3	$24788_{\ 9/2}\ -118271^{\circ}_{\ 11/2}$	1063.926	20	93991.5	
1069.622	100	93491.0	$27604_{9/2} - 121095^{\circ}_{11/2}$	1063.858	60	93997.5	17113 _{13/2} —1111110° _{13/2}
1069.520	1	93499.9		,			24470 _{7/2} -118468° _{9/2}
1069.385	60	93511.7	$23532_{5/2} - 117044^{\circ}_{7/2}$	1063.746	10	94007.4	$23532_{5/2} - 117540^{\circ}_{3/2}$
1069.265	5	93522.2	$22277_{3/2} - 115800^{\circ}_{5/2}$	1063.653	20	94015.6	$34198_{1/2} - 128214^{\circ}_{3/2}$
1069.108	20	93535.9	$19360_{13/2}$ — $112896^{\circ}_{15/2}$	1063.362	20	94041.4	$19872_{7/2} - 113914^{\circ}_{5/2}$
1068.852	500 c l	93558.3	21238 $_{13/2}$ —114797 $^{\circ}_{13/2}$	1063.255	100	94050.8	27380 _{11/2} —121431° _{13/2}
1068.820	5 c l	93561.1	$22747_{9/2} - 116309^{\circ}_{11/2}$	1063.163	70	94059.0	$21611_{5/2} - 115670^{\circ}_{7/2}$
1068.761	10 h	93566.3		1063.104	50	94064.2	
1068.641	80	93576.8		1062.911	10	94081.2	
1068.397	200	93598.2		1062.819	5	94089.4	
1068.270	2	93609.3		1062.673	100	94102.3	18921 _{15/2} —113023° _{17/2}
1068.014	10	93631.7		1062.392	50 c l	94127.2	23647 _{13/2} —117775° _{13/2}
1067.950	300	93637.3		1062.356	50 c l	94130.4	
1067.910	5cl	93640.8		1062.095	80	94153.5	$23532_{5/2} - 117686^{\circ}_{5/2}$
1067.848	10 h	93646.3		1061.975	40	94164.2	21238 _{13/2} —115403° _{11/2}
1067.779	20	93652.3	21755 _{11/2} —115408° _{13/2}	1061.909	20 c l	94170.0	21238 _{13/2} —115408° _{13/2}
1067.503	50	93676.6	$23050_{3/2} - 116727^{\circ}_{5/2}$	1061.887	10 c l	94172.0	
1067.416	40	93684.2	$19872_{7/2} - 113556^{\circ}_{5/2}$	1061.830	4	94177.0	$21755_{11/2}$ — $115933^{\circ}_{11/2}$
1067.167	10	93706.0	22747 _{9/2} -116453° _{9/2}	1061.695	10	94189.0	$21611_{5/2} - 115800^{\circ}_{5/2}$
1067.117	200	93710.4		1061.599	500	94197.5	16135 _{7/2} —110333° _{7/2}
1067.068	20	93714.7	27380 _{11/2} —121095° _{11/2}	1061.519	5	94204.6	$21294_{7/2} - 115499^{\circ}_{9/2}$
1067.000	10	93720.7		1061.328	200	94221.6	17113 _{13/2} —111335° _{15/2}
1066.896	200	93729.8	$23844_{9/2} - 117574^{\circ}_{11/2}$	1061.162	30 c l	94236.3	$23844_{9/2} - 118081^{\circ}_{9/2}$
1066.570	20	93758.5	$19872_{7/2} - 113630^{\circ}_{7/2}$	1061.120	30 c l	94240.0	$19360_{13/2}$ — $113600^{\circ}_{13/2}$
1066.520	2	93762.9		1061.072	5cl	94244.3	$27138_{7/2} - 121382^{\circ}_{9/2}$
1066.465	3	93767.7	17113 _{13/2} —110881° _{11/2}	1061.051	5 c l	94246.2	
1066.345	100	93778.3	27604 _{9/2} -121382° _{9/2}	1060.993	100	94251.3	21418 _{5/2} -115670° _{7/2}
1066.223	20	93789.0	21535 _{9/2} -115324° _{9/2}	1060.857	100	94263.4	. *
1066.177	3	93793.0		1060.734	20	94274.3	
1066.089	20 c l	93800.8	$17534_{15/2}$ — $111335^{\circ}_{15/2}$	1060.546	200	94291.0	19308 _{11/2} —113600° _{13/2}
1066.034	500	93805.6	23442 _{11/2} —117248° _{13/2}	1060.486	10	94296.4	$22747_{\ 9/2} -117044^{\circ}_{\ 7/2}$
1065.791	30	93827.0		1060.250	30	94317.4	
1065.625	10	93841.6		1060.160	40	94325.4	
1065.586	10	93845.1	$25033_{9/2} - 118879^{\circ}_{11/2}$	1060.077	20	94332.8	23442 _{11/2} —117775° _{13/2}
1065.524	80	93850.5		1059.926	10	94346.2	
1065.464	20	93855.8		1059.822	20	94355.5	$19308_{11/2} - 113664^{\circ}_{11/2}$

^a For doubly-classified lines, the wavelength is entered only once.

TABLE X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

${\stackrel{\lambda_{ m vac}}{ m A}}$	Intensity	σ (cm^{-1})	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{\mathrm{A}}$	Intensity	σ (cm^{-1})	Classification ^a
1059.714	10	04265 1		1052 177	1	0.4050.0	
		94365.1	22000 1164520	1053.177	1	94950.8	
1059.631	100 c l	94372.5	$22080_{7/2} - 116453^{\circ}_{9/2}$	1053.105	1	94957.3	
1059.587	100 c l	94376.4		1053.021	100	94964.9	
1059.410	50	94392.2		1052.860	100 c l	94979.4	
1059.281	400 c l	94403.7	26095 _{11/2} —120498° _{13/2}	1052.815	40	94983.4	
1059.250	100 c l	94406.4	16516 _{7/2} -110922° _{9/2}	1052.633	1000	94999.9	21238 _{13/2} —116238°
1059.157	200	94414.7		1052.571	100	95005.5	15525 _{11/2} —110530°
1059.022	60	94426.8	$23844_{9/2} - 118271^{\circ}_{11/2}$	1052.456	3	95015.8	17627 _{9/2} -112643°
1058.948	10	94433.3	$21238_{13/2} - 115672^{\circ}_{15/2}$	1052.262	3	95033.4	11021 9/2 112049
1058.769	60	94449.3	$22277_{3/2}^{-1} -116727_{5/2}^{\circ}$	1052.202	5 c l	95038.8	
1058.510	100	94472.4		1052.133	5 c l	95045.0	
1058.393	3	94482.9		1051.929	30		
1058.348			91525 —116091°			95063.4	21220 116200
	3	94486.9	21535 _{9/2} -116021° _{7/2}	1051.851	5	95070.5	21238 _{13/2} —116309°
1058.150	4	94504.6	21294 _{7/2} -115800° _{5/2}	1051.792	200	95075.8	19649 _{17/2} —114725°
1058.018	20	94516.4	$22527_{7/2} -117044^{\circ}_{7/2}$	1051.732	40	95081.2	
1057.903	5 c l	94526.6		1051.568	200	95096.1	19700 _{11/2} —114797°
1057.885	10 c l	94528.2	$18241_{\ 11/2}$ — $112769^{\circ}_{\ 13/2}$	1051.423	30	95109.2	
1057.783	100	94537.3		1051.347	5	95116.1	21611 _{5/2} -116727°
057.721	100	94542.9		1051.313	20	95119.2	22527 _{7/2} -117647°
057.490	10 c l	94563.5		1051.093	10	95139.1	1/2
057.456	20	94566.6	18990 _{7/2} -113556° _{5/2}	1050.961	5	95151.0	23050 3/2 -118201
			38785 _{15/2} —133352° _{15/2}	1050.881	10	95158.2	21294 _{7/2} -116453°
.057.310	400	94579.6	$18063_{9/2} - 112643_{11/2}^{\circ}$	1000.001	10	93130.2	
057.228	200	94587.0	38785 _{15/2} —133373° _{17/2}	1050 770	1	05160.2	22527 _{7/2} —117686°
057.228	40	94600.2	23175 _{13/2} —117775° _{13/2}	$1050.770 \\ 1050.652$	$\begin{vmatrix} 1 \\ 7 \end{vmatrix}$	95168.3 95179.0	23442 11/2—118610
056 015	10	04692.0	99647 119971°	1050 505			
1056.815	10	94623.9	23647 _{13/2} —118271° _{11/2}	1050.595	3	95184.2	20315 9/2 -115499
0.50			$23844_{9/2} - 118468^{\circ}_{9/2}$	1050.433	20	95198.8	
1056.619	8	94641.5		1050.323	100	95208.8	
056.518	100	94650.5	$38701_{13/2}$ $-133352^{\circ}_{15/2}$	1050.107	70	95228.4	18063 _{9/2} -113291°
056.314	20	94668.8	$23532_{5/2} - 118201^{\circ}_{3/2}$	1050.056	20	95233.0	0,2
056.211	50	94678.0		1049.914	1	95245.9	
056.030	80	94694.3	$21238_{13/2}$ – $115933^{\circ}_{11/2}$	1049.546	20	95279.3	
055.857	20	94709.8	13/2 110/00 11/2	1049.456	100	95287.5	15045110222
055.668	20	94726.8	$21294_{7/2} - 116021^{\circ}_{7/2}$	1049.450	100	93201.3	15045 5/2 -110333
055.297	20	94760.0	21274 7/2 110021 7/2	1049.228	20	95308.2	26095 _{11/2} —121382° 21418 _{5/2} —116727
055 149	200	04770.0	21525 1162000	1040.004			
055.143	300	94773.9	21535 _{9/2} —116309° _{11/2}	1049.086	2000	95321.1	19649 17/2—114970
055.072	30	94780.3		1048.951	5	95333.3	22747 _{9/2} -118081
054.613	50	94821.5	$20848_{5/2} - 115670^{\circ}_{7/2}$	1048.923	15	95335.9	26095 11/2-121431
054.558	50 c l	94826.5	16516 _{7/2} —111342° _{7/2}	1048.703	100 c l	95355.9	15525 11/2-110881
054.525	80 c l	94829.4	23442 _{11/2} —118271° _{11/2}	1048.672	20 c l	95358.7	16135 7/2 -111494
054.441	60	94837.0					18241 11/2-113600
054.388	5	94841.7		1048.643	200 c l	95361.3	17534 _{15/2} —112896°
054.263	7	94853.0		1048.413	3	95382.2	11004 15/2 112000
053.876	400	94887.8	23175 _{13/2} —118063° _{15/2}	1048.318	4	95390.9	
053.584	6	94914.1	13/2 110000 13/2	1048.255	40	95396.6	15525 11/2-110922
053.542	3	94917.9	18241 _{11/2} —113158° _{9/2}	1049 199	7	05409.7	99977 117606
330.012		7 7 7 1 1 . 7	$\begin{array}{c} 16241_{11/2} - 113136_{9/2} \\ 21535_{9/2} - 116453_{9/2}^{\circ} \end{array}$	1048.122	7	95408.7	22277 3/2 -117686
052 419	1	04020 6	21333 9/2 -110433 9/2	1047.966	3	95422.9	18241 11/2—113664
053.412	1	94929.6	26446 121222	1047.924	8	95426.8	15454 _{13/2} —110881°
053.344	40	94935.8	$26446_{7/2} - 121382^{\circ}_{9/2}$	1047.811	100	95437.1	19360 _{13/2} —114797°
053.260	2	94943.3					23442 _{11/2} —118879°

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\boldsymbol{\lambda_{vac}}}{\mathbf{A}}$	Intensity	σ (cm ⁻¹)	Classification ^a	$\overset{\boldsymbol{\lambda_{vac}}}{\overset{\boldsymbol{A}}{\boldsymbol{A}}}$	Intensity	σ, (cm ⁻¹)	Classification ^a
1047.752	1	95442.4		1041.872	100	95981.1	
1047.625	10	95454.0		1041.740	100	95993.2	20215 116200°
1047.375	10 c l	95476.8	16516 _{7/2} —111993° _{9/2}				$20315_{9/2} - 116309^{\circ}_{11}$
1047.373	10 c l		10310 7/2 111333 9/2	1041.625	100	96003.8	17627 _{9/2} -113630° _{7/2}
		95478.9	17524112022°	1041.563	20	96009.6	21238 _{13/2} —117248° ₁₃
1047.244	3000	95488.7	17534 _{15/2} —113023° _{17/2}	1041.459	400	96019.1	21755 _{11/2} —117775° _{13,}
1047.105	3	95501.4		1041.260	200	96037.5	17627 _{9/2} -113664° ₁₁
1047.048	1	95506.6	,	1041.205	20	96042.6	19360 _{13/2} —115403° ₁₁
1046.941	3	95516.4		1041.145	100	96048.1	19360 _{13/2} —115408° ₁₃
1046.779	300	95531.1		1041.002	60	96061.3	$25033_{9/2} - 121095^{\circ}_{11}$
1046.700	20	95538.4		1040.849	10	96075.4	21611 _{5/2} -117686° _{5/2}
1046.594	1	95548.0	19872 _{7/2} —115420° _{7/2}	1040.646	50	96094.2	19308 _{11/2} —115403° ₁₁
1046.543	1	95552.7		1040.591	100	96099.2	19308 _{11/2} —115408° ₁₃
1046.195	500	95584.5	$15525_{11/2}$ — $111110^{\circ}_{13/2}$	1040.437	6	96113.5	11/2
1046.113	10	95592.0		1040.387	3	96118.1	
1046.014	30	95601.0	18063 _{9/2} —113664° _{11/2}	1040.247	20	96131.0	22747 _{9/2} -118879° ₁₁
1045.900	10	95611.4		1040.180	100	96137.2	20315 _{9/2} -116453° _{9/3}
1045.858	100	95615.3		1040.139	50	96141.0	20313 9/2 110433 9/2
1045.765	5	95623.8	$19700_{11/2} - 115324^{\circ}_{9/2}$	1040.082	5		
1045.707	20	95629.1	19100 11/2 113024 9/2	1040.051	5	96146.3	10079 116091°
1045.707	10 b l	95647.0		1040.031	10	96149.1 96159.1	19872 _{7/2} -116021° _{7/}
1045 445	20. 1	05.650.0		1000 770	.	0.51=4.4	
1045.447	20 c l	9565Q.9	15454 1111108	1039.778	50	96174.4	
1045.411	300 c l	95656.2	15454 _{13/2} —1111110° _{13/2}	1039.380	10	96211.2	
1045.248	8	95671.1	$14859_{\ 11/2}$ $-110530^{\circ}_{\ 13/2}$	1039.253	60 c l	96223.0	$15045_{5/2} - 111268^{\circ}_{3/2}$
1045.181	1	95677.2		1039.200	50 c l	96227.9	$21418_{5/2} - 117647^{\circ}_{7/}$
1045.049	1	95689.3		1039.156	100 c l	96231.9	19700 _{11/2} —115933° ₁₁
1044.993	4	95694.4	/	1039.033	5	96243.3	
1044.909	30	95702.1	$18211_{5/2}$ $-113914^{\circ}_{5/2}$	1038.962	10	96249.9	14859 _{11/2} —1111110° ₁₃
		= ,,	$19700_{11/2}$ $-115403^{\circ}_{11/2}$	1038.773	3	96267.4	$21418_{5/2} - 117686^{\circ}_{5/2}$
1044.851	10	95707.4	$19700_{11/2} - 115408^{\circ}_{13/2}$	1038.451	10	96297.3	$15045_{5/2} - 111342^{\circ}_{7/2}$
1044.608	30	95729.7	,	1038.356	7	96306.1	3,2
1044.239	50	95763.5		1038.293	1000	96311.9	19360 _{13/2} —115672° ₁₅
1044.203	50	95766.8		1038.186	400	96321.8	14558 _{9/2} -110881° ₁₁
1044.117	3	95774.7	$14558_{\ 9/2}\ -110333^{\circ}_{\ 7/2}$	1038.066	40	96333.0	11000 9/2 110001 1
1044.029	500	95782.8	$17113_{13/2}$ $-112896^{\circ}_{15/2}$	1037.862	5	96351.9	21294 _{7/2} -117647° _{7/}
1043.970	3	95788.2	$21535_{9/2} - 117323^{\circ}_{11/2}$	1037.738	50 c l	96363.4	14558 _{9/2} -110922° _{9/}
1042.052	50	05700.0	10700 115400°	1027 702	50 /	060667	
1043.853	50	95798.9	19700 _{11/2} —115499° _{9/2}	1037.703	50 c l	96366.7	
1043.797	500	95804.1	18921 _{15/2} —114725° _{17/2}	1037.584	20	96377.7	
1043.639	10	95818.6	$21755_{11/2}$ – $117574^{\circ}_{11/2}$	1037.479	5	96387.5	22080 _{7/2} -118468° _{9/}
1043.501	50	95831.2		1037.432	2	96391.9	21148 _{3/2} -117540° _{3/}
1043.294	5	95850.2					21294 _{7/2} -117686° _{5/2}
1043.223	200	95856.8	16135 _{7/2} -111993° _{9/2}	1037.390	30	96395.8	
1043.110	10	95867.2		1037.232	10	96410.4	$31803_{1/2} - 128214^{\circ}_{3/2}$
1042.964	1000	95880.6	$15454_{13/2}$ – $111335^{\circ}_{15/2}$	1036.823	15	96448.5	
1042.819	10	95893.9		1036.749	5	96455.4	
1042.651	7	95909.4		1036.623	10	96467.1	15525 _{11/2} —111993° _{9/}
1042.478	100	95925.3	$32288_{~3/2} - 128214^{\circ}_{~3/2}$	1036.410	60	96486.9	17113 _{13/2} —113600° ₁₃
1042.476	2	95925.3	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1000.410	00	20400.9	18921 _{15/2} —115408° ₁₃
			22321 7/2 -110400 9/2	1036 174	40 a 1	06509.0	10921 15/2-115408 13
1042.250	20	95946.3		1036.174	40 c l	96508.9	
1042.031	3	95966.4	25400 121222	1036.151	40 c l	96511.0	
1041.963	60	95972.7	$25409_{7/2} - 121382^{\circ}_{9/2}$	1035.765	8 b l	96547.0	

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

$\overset{f{\lambda_{yac}}}{ ext{A}}$	Intensity	σ (cm ⁻¹)	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{\mathrm{A}}$	Intensity	σ (cm^{-1})	Classification ^a
1035.675	30	96555.4	18241 _{11/2} —114797° _{13/2}	1029.711	200	97114.6	16516 _{7/2} -113630° _{7/2}
1035.554	10	96566.7	$20160_{3/2} - 116727^{\circ}_{5/2}$	1029.631	50	97122.2	.,2
1035.386	20	96582.3	0,2	1029.393	5	97144.6	19308 _{11/2} —116453° _{9/2}
1035.312	10	96589.2	$19649_{17/2} - 116238_{15/2}^{\circ}$	1029.284	10h	97154.9	19500 11/2 110 100 9/2
1035.260	10	96594.1	$24788_{9/2} - 121382^{\circ}_{9/2}$	1029.212	100	97161.7	18241 _{11/2} —115403° _{11/}
				1027.212	100	7,101.1	10211 11/2 210100 11/.
1035.111	50	96607.0	19700 _{11/2} —116309° _{11/2}	1029.158	30	97166.8	18241 _{11/2} —115408° _{13/}
1035.063	2	96612.5		1029.032	2000	97178.7	13352 _{11/2} —110530° _{13/}
1034.937	3	96624.2	19308 _{11/2} —115933° _{11/2}	1028.901	100	97191.1	17534 _{15/2} —114725° _{17/}
1034.826	5	96634.6		1028.711	8 h	97209.0	18211 _{5/2} -115420° _{7/2}
1034.804	30	96636.6		1028.277	10	97250.1	
1034.338	100	96680.2	18990 _{7/2} —115670° _{7/2}	1000 164	20 - 1	07960.0	18063 _{9/2} -115324° _{9/2}
1034.336	7	96701.1	10990 7/2 -113070 7/2	1028.164	20 c l	97260.8	10003 9/2 -113324 9/2
1034.114	20 c l	96707.6	91611119910°	1028.029	2	97273.5	10001 116020°
1034.043			$21611_{\ 5/2}\ -118318^{\circ}_{\ 7/2}$	1027.569	100 b l	97317.1	18921 _{15/2} —116238° ₁₅
	10 c l	96710.7		1027.488	10 h	97324.7	
1033.827	10	96728.0		1027.226	40	97349.6	
1033.787	5	96731.7		1027.146	3	97357.1	$18063_{9/2} - 115420^{\circ}_{7/2}$
1033.738	20	96736.3	$21535_{9/2} - 118271^{\circ}_{11/2}$	1026.922	2	97378.4	
1033.680	20	96741.7	-,-	1026.706	1	97398.9	
1033.652	10	96744.4	$24788_{9/2} - 121532^{\circ}_{11/2}$	1026.477	20	97420.6	$16135_{7/2} - 113556^{\circ}_{5/3}$
1033.582	100	96750.9	18921 _{15/2} —115672° _{15/2}	1026.415	1	97426.5	,,2
1033.424	5	96765.7		1006 000		07494 9	14550 1110020
1033.329	30	96774.6		1026.333	2	97434.3	14558 _{9/2} -111993° _{9/2}
			01505 1100100	1026.251	100	97442.0	15454 _{13/2} —112896° ₁₅
1033.238	50 c l	96783.1	$21535_{9/2} - 118318^{\circ}_{7/2}$	1026.183	500	97448.5	12846 _{9/2} -110295° ₁₁
1033.207	20 c l	96786.0	$21294_{7/2} - 118081^{\circ}_{9/2}$	1026.030	100 c l	97463.0	18990 _{7/2} -116453° _{9/}
1033.070	15	96798.9	$20848_{\ 5/2} -117647^{\circ}_{\ 7/2}$	1025.999	10 c l	97466.0	
1032.977	2	96807.6		1025.945	4	97471.1	23647 _{13/2} —1211119° ₁₅
1032.798	70	96824.4	$21238_{13/2}$ $-118063^{\circ}_{15/2}$	1025.694	40 h	97495.0	$16135_{7/2} - 113630^{\circ}_{7/2}$
1032.496	2	96852.7		1025.243	10	97537.8	23844 _{9/2} -121382° _{9/}
1032.450	200	96857.0		1025.144	50	97547.3	19700 _{11/2} —117248° ₁₃
1032.299	10	96871.2		1024.944	10 h	97566.3	
1032.221	7	96878.5	19360 _{13/2} —116238° _{15/2}	1004 711	107	07500.5	18211 _{5/2} -115800° _{5/5}
1032.147	2	96885.4	13000 13/2 110250 15/2	1024.711	10h	97588.5	
1032.083	400	96891.4		1024.358	8	97622.1	19700 _{11/2} —117323° ₁₁
1031.870	10	96911.4	$24470_{7/2} - 121382^{\circ}_{9/2}$	1024.308	1	97626.9	
1031.635	20	96933.5	$21535_{9/2} -118468^{\circ}_{9/2}$	1024.210	5	97636.2	16125 —112790°
			21000 9/2 110100 9/2	1024.123	1	97644.5	16135 _{7/2} -113780° _{9/}
1031.536	300	96942.8	$13352_{11/2}$ — $110295^{\circ}_{11/2}$	1024.036	10	97652.8	23442 _{11/2} —121095° ₁₁
1031.435	5	96952.3		1023.976	20	97658.5	
1031.360	3	96959.4	* :	1023.670	5 c l	97687.7	$23844_{9/2} - 121532^{\circ}_{11}$
1031.297	2	96965.3		1023.573	30	97697.0	$17627_{9/2} - 115324^{\circ}_{9}$
1031.171	20	96977.1		1023.268	100	97726.1	5,2
1030.944	5	96998.5		1023.223	10	97730.4	23651 _{7/2} -121382° _{9/}
1030.851	300	97007.2	$20315_{9/2} - 117323^{\circ}_{11/2}$	1023.223	200	97757.9	
1030.687	50	97022.7	$16135_{7/2} -113158^{\circ}_{9/2}$	1022.900			13352 _{11/2} —1111110° ₁₃
1030.600	5	97030.8	10100 7/2 110100 9/2	1022.756	10 <i>c l</i> 50	97761.3	10070 1176470
1030.500	20	97040.3	16516 _{7/2} -113556° _{5/2}	1022.750	2	97775.0 97793.8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
1020 220	20	07057.4	-,				
1030.329	20	97056.4	23442 _{11/2} —120498° _{13/2}	1022.395	2	97809.6	$18211_{5/2} - 116021^{\circ}_{7/2}$
1030.193	40	97069.2		1022.301	4	97818.5	
1030.125	3	97075.6		1022.146	4	97833.4	
1030.047	20	97082.9	18241 _{11/2} —115324° _{9/2}	1022.077	4	97840.0	
1029.785	20	97107.6		1021.865	5h		

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\boldsymbol{\lambda_{\mathrm{vac}}}}{\boldsymbol{A}}$	Intensity	$\sigma \ (m cm^{-1})$	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{\mathrm{A}}$	Intensity	σ (cm^{-1})	Classification ^a
1021.764	1	97867.0	18063 _{9/2} -115933° _{11/2}	1013.841	4	98634.8	22747 _{9/2} -121382° _{9/2}
1021.726	30	97873.6	17534 _{15/2} —115408° _{13/2}	1013.780	30	98640.7	$13352_{11/2} - 111993^{\circ}_{9/2}$
102120	00	71010.0	$19700_{11/2} - 117574^{\circ}_{11/2}$	1013.462	100	98671.7	13332 11/2 111793 9/2
1021.664	7	97879.5	19700 11/2 117974 11/2 .	1013.354	5	98682.2	$17627_{9/2} - 116309^{\circ}_{11/2}$
1021.578	15	97887.8	19360 _{13/2} —117248° _{13/2}	1013.142	80	98702.8	19360 _{13/2} —118063° _{15/2}
			10,2			70.02.0	13/2 110000 13/2
1021.352	1000	97909.4	$14859_{\ 11/2} - 112769^{\circ}_{\ 13/2}$	1012.832	5	98733.1	$14558_{9/2} - 113291^{\circ}_{7/2}$
1021.150	20	97928.8					$29835_{9/2} - 128568^{\circ}_{9/2}$
1021.039	7	97939.4	19308 _{11/2} —117248° _{13/2}	1012.760	1	98740.1	$14859_{11/2} - 113600^{\circ}_{13/2}$
1020.990	50	97944.2	$23175_{13/2}$ $-121119^{\circ}_{15/2}$	1012.300	2	98784.9	$22747_{9/2} - 121532^{\circ}_{11/2}$
1020.609	10	97980.7		1012.101	400	98804.4	$14859_{\ 11/2}$ — $113664^{\circ}_{\ 11/2}$
1000 050	_	00015.0		1011 000			10011
1020.252	5	98015.0		1011.809	50	98832.9	$18211_{5/2} - 117044^{\circ}_{7/2}$
1020.189	5	98021.0	12044 1100018	1011.307	10	98881.9	
1020.052	40	98034.2	$12846_{9/2} - 110881^{\circ}_{11/2}$	1011.012	60	98910.8	
1019.982	2	98040.9	$20160_{\ 3/2}\ -118201^{\circ}_{\ 3/2}$	1010.914	10	98920.4	14859 _{11/2} —113780° _{9/2}
1019.890	10	98049.8		1010.560	50	98955.0	17534 _{15/2} —116489° _{17/2}
1019.699	1	98068.2	18241 _{11/2} —116309° _{11/2}	1010.282	20	98982.3	
1019.631	60	98074.7	15525 _{11/2} —113600° _{13/2}	1010.153	20	98994.9	
1017.001	00	70014.1	$19700_{11/2}$ $-117775^{\circ}_{13/2}$	1010.034	20	99006.6	19941117949°
1019.534	60	98084.0	$14558_{9/2} -112643^{\circ}_{11/2}$	1010.034			18241 _{11/2} —117248° _{13/2}
1019.334	1	98089.8	23442 _{11/2} —121532° _{11/2}	1009.730	1	99034.4	
1019.474	1	90009.0	23442 11/2-121332 11/2	1009.570	1	99052.1	
1019.311	100	98105.5		1009.029	1	99105.2	14558 _{9/2} -113664° _{11/2}
1019.207	2	98115.5		1008.938	1	99114.1	3/2
1018.968	200	98138.5	$15525_{11/2} - 113664^{\circ}_{11/2}$	1008.742	15	99133.4	
1018.890	3	98146.0	$15454_{13/2} - 113600^{\circ}_{13/2}$	1008.612	500	99146.2	$12846_{9/2} - 111993^{\circ}_{9/2}$
1018.544	1	98179.4	10,1	1008.536	3	99153.6	$16516_{7/2} - 115670^{\circ}_{7/2}$
1010 050	_	00105.0					
1018.373	5	98195.8		1008.285	2	99178.3	$19700_{11/2}$ — $118879^{\circ}_{11/2}$
1018.242	100	98208.5	19872 _{7/2} -118081° _{9/2}	1008.220	20 h	99184.7	
1017.853	2	98246.0	$15045_{5/2}$ $-113291^{\circ}_{7/2}$	1007.847	40	99221.4	$14558_{9/2} - 113780^{\circ}_{9/2}$
1017 516	10	00070 ($18063_{9/2} - 116309^{\circ}_{11/2}$	1007.459	40	99259.6	18063 _{9/2} —117323° _{11/2}
1017.516	10	98278.6					$21238_{13/2}$ $-120498^{\circ}_{13/2}$
1017.396	5 c l	98290.1	17113 _{13/2} —115403° _{11/2}	1007.392	1	99266.2	
1017.345	50 c l	98295.1	17113 _{13/2} -115408° _{13/2}	1007.336	7	99271.7	15525 _{11/2} —114797° _{13/2}
1017.310	20 c l	98298.4	$14859_{11/2} - 113158^{\circ}_{9/2}$	1007.088	i	99296.2	13323 11/2 114797 13/2
1017.231	5	98306.1	$17627_{9/2} -115933^{\circ}_{11/2}$	1006.829	3	99321.7	
1016.991	10	98329.3	11021 9/2 110700 11/2	1006.681	5	99336.3	
						33330.0	
1016.714	5	98356.1		1006.383	3	99365.7	
1016.471	200	98379.6	$15454_{13/2}$ – $113833^{\circ}_{15/2}$	1006.221	3	99381.7	
1015.785	20	98446.0	$19872_{7/2} - 118318^{\circ}_{7/2}$	1005.857	10	99417.7	$13352_{11/2}$ $-112769^{\circ}_{13/2}$
1015.730	10	98451.4					$17627_{9/2} - 117044^{\circ}_{7/2}$
1015.699	2	98454.4		1005.676	5	99435.6	$18211_{5/2} - 117647^{\circ}_{7/2}$
1015 460	_	00476.7		1005 504	,	00444.7	
1015.469	5	98476.7		1005.584	1	99444.7	
1015.340	1	98489.2		1005.280	3	99474.8	
1015.274	30	98495.6		1004.912	30	99511.2	10000
1015.170	8	98505.7	20025 1202520	1004.533	2	99548.8	$1398^{\circ}_{11/2}$ – $100947_{9/2}$
1015.046	3	98517.7	29835 _{9/2} -128352° _{9/2}	1004.259	1	99575.9	
1014.815	3	98540.1		1003.399	8	99661.2	
1014.750	10	98546.4	29835 _{9/2} -128381° _{11/2}	1003.258	10	99675.2	
1014.622	30	98558.9	17113 _{13/2} —125672° _{15/2}	1003.238			
1014.022	10 c l	98596.9	$17113_{13/2} - 113072_{15/2}$ $19872_{7/2} - 118468^{\circ}_{9/2}$	1002.876	1 1	99713.2 99728.3	
1011.201	1000	70070.7	17012 7/2 110400 9/2	1004.724	1	997/8 3	

 $^{^{\}rm a}$ For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region—Continued

$\stackrel{\lambda_{ m vac}}{\Lambda}$	Intensity	σ (cm^{-1})	Classification ^a	$\overset{\lambda_{\mathrm{vac}}}{\mathring{\Lambda}}$	Intensity	σ (cm^{-1})	Classification ^a
1001.528	4	99847.4		979.694	2	102072.7	
1001.224 1001.197	50 c l 20 c l	99877.7 99880.4		979.218	1	102122.3	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
1000.630	80	99937.0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	978.001 977.928	4 7	102249.4 102257.0	15525 _{11/2} —117775° _{13/2} 18241 _{11/2} —120498° _{13/2}
1000.525	7	99947.5	$17627_{9/2} - 117574^{\circ}_{11/2}$	976.676	10	102388.1	14859 _{11/2} —117248° _{13/2}
1000.351	3	99964.9		974.231	2	102645.1	1170000
1000.023 999.499	5 30	99997.7 100050.1	$21535_{\ 9/2}\ -121532^{\circ}_{\ 11/2}$	973.100	$\begin{array}{c} 3 \\ 1 \end{array}$	102764.4	$14558_{9/2} - 117323^{\circ}_{11/2}$
999.118	3	100030.1	$21294_{7/2}$ $-121382^{\circ}_{9/2}$	972.263 972.148	2	102852.8 102865.0	
			2893° _{13/2} —102981 _{13/2}	971.675	10	102915.1	14859 _{11/2} —117775° _{13/2}
998.931	10	100107.0	$18211_{\ 5/2}\ -118318^{\circ}_{\ 7/2}$	971.358	1	102948.6	31-5-10
998.827 997.048	$\frac{1}{10}$	100117.4		970.727	5	103015.6	$14558_{9/2} - 117574^{\circ}_{11/2}$
996.885	10	100296.1 100312.5	$12846_{\ 9/2} - 113158^{\circ}_{\ 9/2}$	970.065 969.090	10 20	103085.9 103189.6	18241 _{11/2} —121431° _{13/2}
996.425	5	100358.8	$13352_{11/2}$ $-113664^{\circ}_{11/2}$	968.140 966.531	$\frac{2}{2}$	103290.8 103462.8	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
996.321	10	100369.3	18241 _{11/2} —118610° _{13/2}	965.313	10	103593.3	24788 _{9/2} -128381° _{11/2}
995.957	2	100405.9	$18063_{9/2} - 118468_{9/2}^{\circ}$	964.531	1	103677.3	21100 3/2
995.571	2	100444.9	$12846_{\ 9/2}\ -113291^{\circ}_{\ 7/2}$	963.849	10	103750.7	14859 _{11/2} —118610° _{13/2}
995.520	5 h	100450.0	14050	954.857	8	104727.7	$12846_{\ 9/2} - 117574^{\circ}_{\ 11/2}$
995.377 994.598	3 70	100464.4	14859 _{11/2} —115324° _{9/2}	936.296	5	106803.8	, =
994.545	6	100543.1 100548.5	14859 _{11/2} —115403° _{11/2} 14859 _{11/2} —115408° _{13/2}	935.046 934.970	3 5	106946.6 106955.3	
994.380	3	100565.2	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	934.074	2	107057.9	21294 _{7/2} —128352° _{9/2}
994.123	1	100591.2	16135 _{7/2} -116727° _{5/2}	932.196	3	107273.6	21294 _{7/2} -128568° _{9/2}
004.075		1005000	2893° _{13/2} —103484 _{15/2}	931.153	40	107393.7	25979 _{15/2} —133373° _{17/2}
994.075	2	100596.0	4453° _{15/2} —105049 _{15/2}	920.003	1.	108695.3	
993.795 993.642	100	100624.4 100639.9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	914.635 913.825	60	109333.2 109430.1	
993.600	1	100644.1	17627 _{9/2} -118271° _{11/2}	912.340	1	109608.3	
993.422	4	100662.2	$17113_{13/2} - 117775^{\circ}_{13/2}$	909.894	4	109902.9	
992.169	5	100789.3	$0^{\circ}_{9/2}$ $-100788_{7/2}$	907.103	1	110241.1	$18211_{5/2} - 128453^{\circ}_{7/2}$
992.085 990.750	30 5	100797.8 100933.6	$19700_{11/2}$ $-120498^{\circ}_{13/2}$ $12846_{9/2}$ $-113780^{\circ}_{9/2}$	904.386 903.766	2 2	110572.2 110648.1	
			12010 9/2 110100 9/2				
989.627 989.381	$\frac{2}{20}$	101048.2 101073.3	14859 _{11/2} —115933° _{11/2}	902.999	3	110742.1	**
988.353	20	101073.3	14009 11/2 -110900 11/2	896.172 894.647	$\frac{1}{3}$	111585.7 111775.9	
988.001	60	101214.5	$27138_{7/2} - 128352^{\circ}_{9/2}$	890.276	1	112324.7	
987.960	3	101218.7	$1398^{\circ}_{11/2} - 102617_{11/2}$	889.296	2	112448.5	
987.344	4	101281.8	27100	888.257	1	112580.0	
987.023	2	101314.8	27138 _{7/2} -128453° _{7/2}	887.360	4	112693.8	
985.880 985.120	2 3	101432.2 101510.5	$1398^{\circ}_{11/2} - 102830_{9/2} \ 19872_{7/2} - 121382^{\circ}_{9/2}$	886.233 885.575	2 2	112837.1 112921.0	
983.927	3	101633.6	19072 7/2 -121302 9/2	885.279	20	112921.0	
983.461	8	101681.7	19700 _{11/2} —121382° _{9/2}	884.158	40	113102.0	
982.796	4	101750.5	$14558_{\ 9/2}\ -116309^{\circ}_{\ 11/2}$	883.838	3	113142.9	
982.709	20	101759.5	19360 _{13/2} —121119° _{15/2}	882.990	3	113251.6	
982.340	1	101797.8	$15525_{11/2}$ $-117323^{\circ}_{11/2}$	882.336	1	113335.5	

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

880.303 879.840 879.841 878.749 878.215 876.355 876.305 875.339 874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069 870.893	10 2 10 1 10 2 1 1 1 2 1 1 1 1 1 1 1 1 1	113597.2 113657.0 113708.6 113798.1 113867.3 114109.0 114115.5 114241.4 114327.5 114353.5 114393.8 114397.2 114409.8 114449.3 114604.1	14859 _{11/2} —128568° _{9/2}	856.826 856.740 856.285 856.192 855.808 855.718 855.422 855.038 854.692 854.254 853.782 853.413	1 2 h 1 20 3 20 1 1 1 1	116709.8 116721.5 116783.5 116796.2 116848.6 116860.9 116901.4 116953.9 117001.2 117061.2	
879.840 879.441 878.749 878.215 876.355 876.305 875.339 874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	2 10 1 10 2 1 1 2 1 1 1 1 1 1 1 1 1 1 3 0	113657.0 113708.6 113798.1 113867.3 114109.0 114115.5 114241.4 114327.5 114353.5 114393.8 114397.2 114409.8 114449.3 114604.1	14859 _{11/2} —128568° _{9/2}	856.740 856.285 856.192 855.808 855.718 855.422 855.038 854.692 854.254	2 h 1 20 3 20 1 1 1 2	116721.5 116783.5 116796.2 116848.6 116860.9 116901.4 116953.9 117001.2 117061.2	
879.441 878.749 878.215 876.355 876.305 875.339 874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	10 1 10 2 1 1 2 1 1 1 1 1 1 1 1 1 30 1	113708.6 113798.1 113867.3 114109.0 114115.5 114241.4 114327.5 114353.5 114393.8 114397.2 114409.8 11449.3 114604.1	14859 _{11/2} —128568° _{9/2}	856.285 856.192 855.808 855.718 855.422 855.038 854.692 854.254	1 20 3 20 1 1 1 1	116783.5 116796.2 116848.6 116860.9 116901.4 116953.9 117001.2 117061.2	
878.749 878.215 876.355 876.305 875.339 874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	1 10 2 1 1 2 1 1 1 1 1 1 1 1 1 30 1	113798.1 113867.3 114109.0 114115.5 114241.4 114327.5 114353.5 114393.8 114397.2 114409.8 114449.3 114604.1	14059 11/2 120500 9/2	856.192 855.808 855.718 855.422 855.038 854.692 854.254	20 3 20 1 1 1 1 2	116796.2 116848.6 116860.9 116901.4 116953.9 117001.2 117061.2	
878.215 876.355 876.305 875.339 874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	10 2 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	113867.3 114109.0 114115.5 114241.4 114327.5 114353.5 114393.8 114397.2 114409.8 114449.3 114604.1		855.808 855.718 855.422 855.038 854.692 854.254 853.782	3 20 1 1 1 1 2	116848.6 116860.9 116901.4 116953.9 117001.2 117061.2	
876.305 875.339 874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	1 1 2 1 1 1 1 1 1 1 30 1	114115.5 114241.4 114327.5 114353.5 114393.8 114397.2 114409.8 114449.3 114604.1		855.422 855.038 854.692 854.254 853.782	1 1 1 1	116901.4 116953.9 117001.2 117061.2	
876.305 875.339 874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	1 1 2 1 1 1 1 1 1 1 30 1	114115.5 114241.4 114327.5 114353.5 114393.8 114397.2 114409.8 114449.3 114604.1		855.422 855.038 854.692 854.254 853.782	1 1 1 1	116901.4 116953.9 117001.2 117061.2	
875.339 874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	1 2 1 1 1 1 1 1 1 30 1	114241.4 114327.5 114353.5 114393.8 114397.2 114409.8 114449.3 114604.1		855.038 854.692 854.254 853.782	1 1 1	116953.9 117001.2 117061.2	
874.680 874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	2 1 1 1 1 1 1 1 30 1	114327.5 114353.5 114393.8 114397.2 114409.8 114449.3 114604.1		854.692 854.254 853.782	1 1 2	117001.2 117061.2	
874.481 874.173 874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	1 1 1 1 1 1 30 1	114353.5 114393.8 114397.2 114409.8 114449.3 114604.1		854.254 853.782	1 2	117061.2	
874.147 874.051 873.749 872.569 872.104 871.932 871.699 871.069	1 1 1 1 30 1	114397.2 114409.8 114449.3 114604.1				117125 9	
874.051 873.749 872.569 872.104 871.932 871.699 871.069	1 1 1 30 1	114409.8 114449.3 114604.1					
873.749 872.569 872.104 871.932 871.699 871.069	1 1 30 1	114449.3 114604.1			10	117176.6	
872.569 872.104 871.932 871.699 871.069	1 30 1	114604.1		853.318	2	117189.6	
872.104 871.932 871.699 871.069	30 1			853.229	4	117201.8	
871.932 871.699 871.069	1			853.120	i	117216.8	
871.699 871.069		114665.2		853.054	1	117225.9	
871.069		114687.8		852.968	i	117237.7	
	3	114718.5		851.867	2	117389.2	
870.893	2	114801.5		851.524	2	117436.5	
	1	114824.7		851.438	3	117448.4	
869.598	1	114995.7		851.361	8	117459.0	
868.558	10	115133.4		851.301	200	117467.3	
868.490	1	115142.4		851.168	15	117485.6	
868.414	1	115152.4		850.903	5	117522.2	-
866.285	4	115435.4		850.331	5	117601.3	
864.910	1	115619.0		850.156	10 b l	117625.5	
864.582	1	115662.8		850.061	1	117638.6	
864.320	1	115697.9		850.011	1	117645.5	
863.941	8	115748.6		849.895	20	117661.6	
863.349	1	115828.0		849.803	20	117674.3	
863.131	3h	115857.3		848.718	1	117824.8	
862.823	2	115898.6		848.657	10	117833.2	
862.427	2	115951.8		848.440	1	117863.4	
862.227	1	115978.7		847.729	1	117962.2	
861.535	2	116071.9		847.474	3	117997.7	
861.498	1	116076.9		846.565	2	118124.4	
861.307	1	116102.6		846.209	2	118174.1	1
860.721	2	116181.7		845.710	7	118243.8	
860.522	2	116208.5	-	845.231	10	118310.8	
860.313	3	116236.8		845.066	5	118334.0	
859.956	2	116285.0		844.788	3	118372.9	
859.730	3	116315.6	,	844.395	100	118428.0	
859.541	1	116341.2		843.998	2	118483.7 .	
859.299 859.102	1 7	116373.9 116400.6		843.887 843.542	10 40 b l	118499.3 118547.7	
857.723	8	116587.8		843.338	200	118576.4	
857.614	1	116602.6		843.312	10 c l	118580.1	
857.348	5	116638.8		842.497	40	118694.8	
857.210 857.091	1 1	116657.5 116673.7		842.384 842.130	1	118710.7	

^a For doubly-classified lines, the wavelength is entered only once.

Table X. Observed spectral lines of Pr III in the vacuum ultra violet region - Continued

$\overset{\lambda_{\mathrm{vac}}}{\mathrm{A}}$	Intensity	σ (cm^{-1})	Classification ^a	$egin{pmatrix} \lambda_{ m vac} \ A \end{matrix}$	Intensity	σ (cm ⁻¹)	Classification ^a
841.990	3	118766.2		832.631	2	120101.2	
841.779	1	118796.0		832.164	1	120168.6	
841.628	20 b l	118817.3		832.013	1	120190.4	
841.426	8	118845.9		831.919	3	120204.0	N
841.015	4	118903.9		831.846	10	120214.6	
840.890	30 c l	118921.6		831.265	200	120298.4	
840.871	10~c~l	118924.3		831.136	1	120317.2	
840.459	6	118982.6		830.927	2	120347.5	
840.282	8	119007.7		830.386	1	120425.9	
840.057	60	119039.5		830.061	2	120473.1	
839.995	60	119048.3		829.325	3	120580.0	
839.619	1	119101.6		828.364	50	120719.9	
839.529	1	119114.4		828.169	1	120748.3	
839.474	2	119122.2		828.134	1	120753.4	,
839.358	30 h	119138.7		827.345	1	120868.6	
838.933	30	119199.0		825.989	30	121067.0	
838.809	1	119216.6		825.404	7	121152.8	
837.712	2	119372.8		824.880	3	121229.8	
837.223	3	119442.5		824.542	1	121279.4	
836.744	8	119510.9		823.117	1	121489.4	
836.295	1	119575.0		822.725	2	121547.3	
835.843	15 <i>b l</i>	119639.7		822.467	15	121585.4	
834.617	1	119815.4		821.942	10	121663.1	
833.478	10	119979.2					
833.190	10	120020.6					

 $^{{}^{\}frac{\epsilon}{a}}$ For doubly-classified lines, the wavelength is entered only once.

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